

# DANBURY BRANCH IMPROVEMENT PROGRAM TASK 5

## ENVIRONMENTAL TECHNICAL MEMORANDUM IMPACTS ANALYSIS

STATE PROJECT 302-008



### SECTION 3: AIR QUALITY

APRIL 2011

## **SECTION 3. AIR QUALITY**

### **METHODOLOGY**

Air quality impacts are determined at both the regional and local levels. The determination of regional air quality impacts requires a rigorous modeling exercise, conducted by metropolitan planning organizations (MPOs) and/or state departments of transportation. For the Danbury Branch Improvement Program, the MPOs – the South Western Regional Planning Agency (SWRPA) and the Housatonic Valley Council of Elected Officials (HVCEO) – work in coordination with the Connecticut Department of Transportation (CTDOT) to conduct a conformity determination of their long- (20+ years) and near-term (within five years) transportation plans. This process involves modeling travel demand across the entire regional transportation system, considering the possible implementation of planned transportation initiatives, and applying vehicle trips, vehicle miles of travel, and associated emissions to the network. Air quality “conformity” is demonstrated when the forecasted emissions of the existing and planned road and transit networks of a transportation plan do not cause exceedances of air quality standards.

Local impact analysis takes place at the project level and focuses on carbon monoxide (CO) impacts on local air quality from the project. In order to assess CO impacts on local air quality from the Danbury Branch Improvement Program, a modeling analysis was conducted to calculate CO concentrations under Existing, No Build, Build, and Mitigated Build conditions at sensitive receptor locations in the vicinity of the intersections most likely to be impacted by the build alternative. The Build scenario represents the study area’s transportation system in the 2030 horizon year with the addition of traffic generated by the Danbury Branch Improvement Program. The Mitigated Build scenario has the same traffic conditions as the Build scenario but assumes that intersection improvements (mitigation) to reduce congestion have been made.

The modeling analysis determined whether the changes in vehicular traffic conditions on local roadways would create violations of federal CO standards. The analysis was conducted using the EPA MOBILE6.2 emissions factor model and the CALQVIEW2 (Windows version of CAL3QHC Version 2) model.

### **IMPACTS**

#### **Regional Impacts – Transportation Conformity**

SWRPA and HVCEO coordinate with the CTDOT to conduct a conformity determination of their State and Regional Transportation Plans (long-term) and Transportation Improvement Programs (TIP) (near-term). In Connecticut, the regional planning agencies (RPAs) prepare the Regional Transportation Plans and TIPs for their region. CTDOT prepares the statewide Master Transportation Plan and Statewide Transportation Improvement Program (STIP), which incorporates the MPOs’ current TIPs. The Master Plan and Regional Transportation Plan identifies long-range (20+ years) transportation needs in the region. The STIP and TIP lay out the priority projects to be funded within the next five years and the allocated budget amount. The conformity analysis must demonstrate that the existing and planned road and transit network

emissions are forecasted to be less than the amount allowed in the volatile organic compounds (VOC), nitrogen oxides (NO<sub>x</sub>), and CO emissions budgets established by the Connecticut Department of Environmental Protection (DEP) for transportation sources. The emissions budgets are set at levels that will maintain the National Ambient Air Quality Standards (NAAQS) for each pollutant. Therefore, transportation-related emissions must be less than or equal to these emissions budgets.

#### *Project Level Conformity Determination*

Federal regulations concerning the conformity of transportation projects developed, funded, or approved by the United States Department of Transportation and by MPOs are contained in 40 CFR 93. The Danbury Branch Improvement Program is included in the MPOs' current Regional Transportation Plans but is not included in their Transportation Improvement Programs (TIP).

In accordance with 40 CFR 93.115(a), the applicable criteria and procedures for determining the conformity of a project, which is not from conforming Transportation Plans and TIPs are listed in 40 CFR 93.109(b). Each of the following criteria has been satisfied, as follows:

- **Transportation Control Measures (TCMs)** – This project must not and does not interfere with the implementation of any TCMs in the current DEP State Implementation Plan (SIP), as there are none.

**Currently Conforming Regional Transportation Plan and TIP**– There must be a currently conforming Regional Transportation Plan and currently conforming TIP in the project area at the time of project approval. The MPOs current 2007 Transportation Plans and the 2010-2013 Statewide Transportation Improvement Program (STIP), which incorporates the MPOs' current TIPs, were determined to be in conformity by FHWA and FTA on November 13, 2009.

**CO, PM<sub>10</sub> and PM<sub>2.5</sub> Hot Spots** – The project must not cause or contribute to any new localized CO, particulate matter between 2.5 and 10 microns in diameter (PM<sub>10</sub>) and/or particulate matter less than 2.5 microns in diameter (PM<sub>2.5</sub>) violations or increase the frequency or severity of any existing CO, PM<sub>10</sub> and/or PM<sub>2.5</sub> violations in CO, PM<sub>10</sub> and/or PM<sub>2.5</sub> nonattainment and maintenance areas.

This project will not cause or contribute to any new violations or increase the frequency or severity of any existing CO violations in CO non-attainment or maintenance areas as evidenced by the results of the CO hot spot analysis contained herein. This project is not located in a PM<sub>10</sub> non-attainment or maintenance area, therefore a PM<sub>10</sub> hot spot analysis was not required.

The Danbury Branch Improvement Program is located in a PM<sub>2.5</sub> non-attainment area. This project could potentially be a project of local air quality concern as determined by 40 CFR 93.123 (b) (1). The potential for PM<sub>2.5</sub> hot-spots in the Build Alternatives could theoretically be higher or lower than that for the No Build Alternative, depending on the fuel source selected.

- **PM<sub>10</sub> and PM<sub>2.5</sub> control measures** – The project must comply with PM<sub>10</sub> and PM<sub>2.5</sub> control measures in the SIP. There are no PM<sub>10</sub> or PM<sub>2.5</sub> control measures in the current SIP, so this criterion is met.
- **Emissions Budget or Emissions Reduction** – This project has been demonstrated to be consistent with the motor vehicle emissions budgets in the SIP as evidenced by CTDOT's Ozone Air Quality Conformity Determination dated February 2006.

In summary, the Danbury Branch Improvement Program has been determined to be in conformity with the Clean Air Act, as amended, pursuant to all applicable U.S. Environmental Protection Agency (EPA) regulations.

### **Local Impacts – Microscale Analysis**

The following local impact microscale analysis is a CO modeling exercise that measures air quality impacts around signalized vehicular intersections near the existing and planned new rail stations in the corridor. The air quality impacts are estimated based on the Danbury Branch Improvement Program's vehicular traffic analysis, which accounts for changing traffic patterns and volumes over time, increased rail service, and additional station parking for the Build and No Build scenarios.

All of the study alternatives were modeled, including the No Build and TSM scenarios. The CO modeling analysis determined that none of the alternatives would create violations of federal CO standards at localized areas (where CO hotspots frequently occur). The analysis was conducted using the EPA MOBILE6.2 emissions factor model and the CALQVIEW2 (Windows version of CAL3QHC Version 2) model.

The corridor-wide traffic analysis identified four signalized intersections that could be potentially impacted by congestion from vehicular traffic such that local air quality conditions could be affected. The congestion was predicted by studies of future (year 2030) traffic volumes and level of service (operation) and is associated with traffic to and from the passenger stations. The four signalized intersections and the alternatives they are associated with are the following:

- Grist Mill Road (Route 7) / Glover Avenue [Alternatives C and E -- station improvements at existing Merritt 7 Station in Norwalk]
- Grist Mill Road (Route 7) / Main Avenue [Alternatives C and E -- station improvements at existing Merritt 7 Station in Norwalk]
- Federal Road (Route 202) / Station Road-Whisconier Road (Route 25) [Alternative D -- new station in Brookfield]
- Route 7 / Bridge Street (Route 202) [Alternative D -- new station in New Milford]

The Route 7/Bridge Street (Route 202) intersection, the Federal Road (Route 202)/Station Road-Whisconier Road (Route 25) intersection, and the Grist Mill Road (Route 7)/Main Avenue intersection are predicted to have the worst levels of service in the year 2030 PM Build scenario. The Route 7/Bridge Street (Route 202) intersection and the Grist Mill Road (Route 7)/Glover Avenue intersections are predicted to have the highest traffic volumes in this scenario.

As part of the air quality analysis, capacity and queuing analyses were utilized to determine air quality impacts for the following peak periods in the years indicated. The AM and PM peak periods tend to have the highest traffic volumes and worst level-of-service.

- 2010 morning (AM) and afternoon (PM) Existing scenarios
- 2030 AM and PM No-Build scenarios
- 2030 AM and PM Build scenarios
- 2030 AM and PM Mitigated Build scenarios.

CALQVIEW2 is a line source dispersion model that applies the Gaussian dispersion theory to traffic inputs and meteorological conditions to predict CO concentrations from vehicles on the roadway. Air quality impacts from mobile sources are modeled by analyzing queue links and free flow links. Queue links simulate vehicles idling at the stop bar of an intersection. Free-flow links simulate vehicles traveling through an intersection. Receptor locations are selected based on where people may be located who may be exposed to the CO produced by vehicles in the area (e.g., sidewalks, outdoor eating establishments). The CALQVIEW2 meteorological and background parameters used in the model are listed in Table 1.

**Table 1: CALQVIEW2 Parameters**

| <b>Parameter</b>                | <b>Value</b>                |
|---------------------------------|-----------------------------|
| Averaging time                  | 60 mins                     |
| Surface roughness length        | 175 cm                      |
| Settling velocity               | 0                           |
| Deposition velocity             | 0                           |
| Scale conversion factor         | 0.3048 (units in ft)        |
| Output                          | 1 (in ft)                   |
| Wind speed                      | 1 m/s                       |
| Wind direction                  | 0                           |
| Stability class                 | 4 (D) – Urban               |
| Mixing height                   | 1000 m                      |
| 1-hour background concentration | 4.3 parts per million (ppm) |
| Multiple wind directions        | Yes – 10 degree increments  |
| Receptor height                 | 6.0 ft                      |
| Signal times                    | Varies (traffic analysis)   |
| Traffic volumes                 | Varies (traffic analysis)   |

Mobile source CO emission factors were modeled using MOBILE6.2. These input files and associated output files are included in Appendix A (MOBILE 6.2 Input and Output Files).

Results from the model represent the one-hour average CO concentrations at each receptor due to the modeled traffic, and include a background concentration of 4.3 parts per million (ppm). To determine the eight-hour average concentration at each receptor, the one-hour dispersion result from the model was multiplied by the persistence factor of 0.7. The 2010 AM Existing and PM Existing, 2030 AM No-Build and PM No-Build, 2030 AM Build and PM Build, and 2030 AM Mitigated Build and PM Mitigated Build scenarios were modeled for each of the four intersections, for a total of 32 model runs. The No-Build scenario means that no station

improvements (with their associated traffic changes) would take place (Alternatives A and B). The Build scenario assumes that station improvements included in a particular alternative (Alternatives C, D, and E) would take place. The Mitigated Build means that congested intersections associated with the Build Alternatives have been improved to reduce traffic congestion, as recommended by the traffic studies for the DEIS.

Table 2 presents the highest CO reading for each model run. Appendix B contains the CALQVIEW2 model output showing all results for each run. All results are well below the CO NAAQS of 35 ppm for one hour and 9 ppm for eight hours. The highest future CO occurs at the Route 7 / Bridge Street intersection under the 2010 Existing PM or 2030 Mitigated Build PM scenario, with one-hour CO concentration of 8.8 ppm and an eight-hour CO concentration of 6.2 ppm.

The results show that no violations of federal CO standards are expected near the stations forecasted to have the highest traffic volumes and worst level-of-service for any of the Build alternatives. Since the traffic analysis expects these four intersections to be the worst-impacted intersections in any of the alternatives, there is little concern regarding air quality impacts at all other signalized intersections near the stations.

These findings appear to be reasonable, based on the following:

- Air quality monitoring data show that existing CO levels in the overall region and state are well below the CO NAAQS. Therefore, CO hot spots would be highly unlikely in the vicinity of the planned project.
- The low level of trips that would be generated by this initiative relative to total regional trips is unlikely to negatively impact regional air quality. The VOC, NO<sub>x</sub>, and CO emissions from the transportation system are currently below those allowed by DEP. Thus, the effects of increased travel near the stations can be accommodated without causing the emission budgets to be violated, and as a result, would not cause or contribute to further violations of the NAAQS. Furthermore, recent monitored ozone exceedances are primarily due to the transport of ozone and other pollutants from beyond Connecticut. The low number of additional vehicle trips is unlikely to cause or contribute to further ozone exceedances.

**Table 2: Highest Predicted CO Concentrations**

| Model Run  | Highest 1-hour Concentration (ppm) | Corresponding 8-hour Concentration (ppm) | Receptor Location         |
|--|------------------------------------|--|---------------------------|
| Federal Road (Route 202) / Station Road (Route 25) 2010 Existing AM        | 5.3                                | 3.7                                      | Westbound east midblock   |
| Federal Road (Route 202) / Station Road (Route 25) 2010 Existing PM        | 5.2                                | 3.6                                      | Westbound east midblock   |
| Federal Road (Route 202) / Station Road (Route 25) 2030 No Build AM        | 5.2                                | 3.6                                      | Southbound north midblock |
| Federal Road (Route 202) / Station Road (Route 25) 2030 No Build PM        | 5.4                                | 3.8                                      | Southbound north midblock |
| Federal Road (Route 202) / Station Road (Route 25) 2030 Build AM           | 5.2                                | 3.6                                      | Southbound north midblock |
| Federal Road (Route 202) / Station Road (Route 25) 2030 Build PM           | 5.5                                | 3.9                                      | Southbound north midblock |
| Federal Road (Route 202) / Station Road (Route 25) 2030 Mitigated Build AM | 5.2                                | 3.6                                      | Southbound north midblock |
| Federal Road (Route 202) / Station Road (Route 25) 2030 Mitigated Build PM | 5.4                                | 3.8                                      | Southbound north midblock |
| Grist Mill Road (Route 7) / Glover Avenue 2010 Existing AM                 | 6.3                                | 4.4                                      | Northbound south midblock |
| Grist Mill Road (Route 7) / Glover Avenue 2010 Existing PM                 | 6.6                                | 4.6                                      | Northbound south midblock |
| Grist Mill Road (Route 7) / Glover Avenue 2030 No Build AM                 | 6                                  | 4.2                                      | Northbound south midblock |
| Grist Mill Road (Route 7) / Glover Avenue 2030 No Build PM                 | 6.2                                | 4.3                                      | Northbound south midblock |
| Grist Mill Road (Route 7) / Glover Avenue 2030 Build AM                    | 6                                  | 4.2                                      | Northbound south midblock |
| Grist Mill Road (Route 7) / Glover Avenue 2030 Build PM                    | 6.2                                | 4.3                                      | Northbound south midblock |
| Grist Mill Road (Route 7) / Glover Avenue 2030 Mitigated Build AM          | 6                                  | 4.2                                      | Northbound south midblock |
| Grist Mill Road (Route 7) / Glover Avenue 2030 Mitigated Build PM          | 6.1                                | 4.3                                      | Northbound south midblock |
| Route 7 / Bridge Street (Route 202) 2010 Existing AM                       | 6.7                                | 4.7                                      | Westbound east midblock   |
| Route 7 / Bridge Street (Route 202) 2010 Existing PM                       | 8.8                                | 6.2                                      | Northbound north midblock |
| Route 7 / Bridge Street (Route 202) 2030 No Build AM                       | 6.3                                | 4.4                                      | Westbound east midblock   |
| Route 7 / Bridge Street (Route 202) 2030 No Build PM                       | 8.6                                | 6.0                                      | Northbound north midblock |
| Route 7 / Bridge Street (Route 202) 2030 Build AM                          | 7.4                                | 5.2                                      | Northbound north midblock |
| Route 7 / Bridge Street (Route 202) 2030 Build PM                          | 8.7                                | 6.1                                      | Northbound north midblock |
| Route 7 / Bridge Street (Route 202) 2030 Mitigated Build AM                | 7.2                                | 5.0                                      | Northbound north midblock |
| Route 7 / Bridge Street (Route 202) 2030 Mitigated Build PM                | 8.8                                | 6.2                                      | Northbound north midblock |
| Grist Mill Road (Route 7) / Main Avenue 2010 Existing AM                   | 7.9                                | 5.5                                      | Westbound east midblock   |
| Grist Mill Road (Route 7) / Main Avenue 2010 Existing PM                   | 7.7                                | 5.4                                      | Southwest corner          |
| Grist Mill Road (Route 7) / Main Avenue 2030 No Build AM                   | 6.9                                | 4.8                                      | Northwest corner          |
| Grist Mill Road (Route 7) / Main Avenue 2030 No Build PM                   | 6.7                                | 4.7                                      | Northwest corner          |
| Grist Mill Road (Route 7) / Main Avenue 2030 Build AM                      | 6.9                                | 4.8                                      | Northwest corner          |
| Grist Mill Road (Route 7) / Main Avenue 2030 Build PM                      | 6.7                                | 4.7                                      | Northwest corner          |
| Grist Mill Road (Route 7) / Main Avenue 2030 Mitigated Build AM            | 6.9                                | 4.8                                      | Northwest corner          |
| Grist Mill Road (Route 7) / Main Avenue 2030 Mitigated Build PM            | 6.6                                | 4.6                                      | Southbound south midblock |

### Mobile Source Air Toxics

In addition to the NAAQS pollutants, EPA regulates a number of mobile source air toxics (MSATs), identified in an EPA Final Rule, Control of Hazardous Air Pollutants from Mobile Sources (Federal Register, Vol. 72, No. 37, page 8430, February 26, 2007). The EPA subsequently identified six of these from mobile sources that pose especially high cancer risks. These are acrolein, benzene, 1, 3-butadiene, formaldehyde, naphthalene, and polycyclic organic matter.

The U.S. Department of Transportation, Federal Highway Administration (FHWA), has outlined a tiered approach for analyzing MSATs in National Environmental Policy Act (NEPA)

documents, with three tiers representing the levels of potential impacts from projects (Memorandum, *Interim Guidance Update on Mobile Source Air Toxic Analysis in NEPA*, dated September 30, 2009). In addition to the EPA identified six MSAT compounds listed above, FHWA and EPA cite diesel particulate matter plus diesel exhaust organic gases (diesel PM) as a high cancer risk driver. While the FHWA considers these the priority mobile source air toxics, the list is subject to change and may be adjusted in consideration of future EPA rules.

Based on the guidance, the Danbury Branch Improvement Program falls in the middle tier, likely having low potential MSAT effects, because it is a project that would improve transit or freight operations. For this tier, FHWA recommends a qualitative analysis of potential MSAT effects.

For each alternative in this EIS, the amount of MSAT emitted would be proportional to the amount of rail activity as well as vehicle miles traveled (VMT), assuming that other variables (such as travel not associated with the rail stations) are the same for each alternative. The estimated MSATs (particularly diesel particulate matter) emitted along the rail line from the rail activity in the Build Alternatives could theoretically be higher or lower than that for the No Build Alternative, depending on the fuel source selected. The No Build and TSM alternatives (Alternatives A and B) would require continued use of diesel powered locomotives to operate Danbury Branch trains. There are currently two fuel source combinations under consideration for the Build Alternatives: all electric (Alternatives C, E, and the electrified Alternative D); or a diesel/electric combination (Alternative C with the diesel-fueled Alternative D). The estimated MSATs emitted from the diesel/electric Build scenario (Alternative C with the diesel-fueled Alternative D) would be higher than the all-electric Build scenario. If the trains are all electrified, the MSATs produced from the rail activity would decrease compared to the No Build scenario.

Regardless of fuel type, the anticipated mode shift of travelers to rail transit from their cars under Alternatives B, C, D, and E would reduce emissions associated with vehicular travel on the region's highways, based on: 1) a decrease in regional vehicular traffic volumes; and 2) increased vehicular speeds (lower emissions per mile traveled) on area highways due to the decrease in traffic. The extent of the potential emissions reductions would correspond to the reduction in VMTs associated with each alternative, which is currently not known. These reductions are only one portion of the emissions associated with each alternative. The train fuel type, as noted above, is a major factor. Associated travel patterns are also important. In the case of Alternative B (TSM), the planned increased use of bus shuttles (presumed to be diesel) could counteract any emissions reductions associated with the decrease in passenger vehicle VMTs.

The on-road VMT estimates at nearby intersections are the same or only slightly higher in the Build Alternatives than they are for the No Build Alternative. Thus, no appreciable difference in overall MSAT emissions at the nearby roadway intersections is anticipated among the various alternatives.

Comparing the net effects of all of the study alternatives, Alternative B (TSM) with diesel-powered buses would likely have little effect on reducing regional MSAT emissions; it could result in a neutral, slightly positive or slightly negative effect on emissions. Alternative C would result in the greatest reductions in MSAT emissions since it replaces existing diesel service by



electric trains and increases the frequency of rail service which will remove vehicles from the region's highways. Alternative E would be the next most effective alternative in reducing emissions for the same reasons; however, it would be less effective than Alternative C because it is only about one-third the length. The electric version of Alternative D would have a slight positive effect (decrease in regional emissions) due to the anticipated mode shift and resultant decrease in roadway VMTs. The diesel version of Alternative D would introduce a new source of diesel fuel-related MSAT emissions and would likely result in higher levels of MSAT emissions in certain local areas.

No matter what alternative is chosen, year 2030 emissions will likely be lower than present levels due to nationally mandated cleaner vehicles and fuels. These EPA control programs are projected to reduce annual MSAT emissions by 72 percent nationwide from the year 1999 to 2050. Local conditions may differ from these national projections in terms of fleet mix and turnover, VMT growth rates, and local control measures. However, the EPA-projected reductions are so significant (even after accounting for VMT growth) that future MSAT emissions in the study area are anticipated to be lower as well.

### **PM<sub>2.5</sub> Hot-Spot Analysis**

The Danbury Branch Improvement Program could potentially be a project of local air quality concern because of the potential increase of diesel vehicles at one or more locations. Beginning in March 2012, a quantitative PM<sub>2.5</sub> hot-spot analysis will be required to meet the Clean Air Act and 40 CFR 93.116 requirements. At that time, the EPA MOVES model will be required as the industry standard to conduct this analysis. Because this study will be completed before MOVES is implemented, a qualitative discussion of PM<sub>2.5</sub> is provided below.

Similar to the MSAT analysis, the potential for PM<sub>2.5</sub> hot-spots along the rail line from the rail activity in the Build Alternatives could theoretically be higher or lower than that for the No Build Alternative, depending on the fuel source selected. The potential for PM<sub>2.5</sub> hot-spots from the diesel/electric Build scenario (Alternative C with the diesel-fueled Alternative D) would be higher than the all-electric Build scenario. If the trains are all electrified, the potential for PM<sub>2.5</sub> hot-spots from the rail activity would likely be less than the No Build scenario.

### **Construction-Period Air Quality Protection Measures**

During any earth-clearing and other construction activities associated with the Build Alternatives, potential air quality impacts include airborne dust particles from exposed soils and emissions from idling and mobile construction vehicles. To minimize impacts during construction, the following best management practices will be followed:

- Minimization of exposed erodible earth area to the extent possible.
- Stabilization of exposed earth with grass, pavement, or other cover as early as possible.
- Application of stabilizing agent (i.e., calcium chloride, water) to the work areas and haul roads.
- Covering, shielding, or stabilizing stockpiled material as necessary.
- Use of covered haul trucks.

- To minimize drag out, the incidental transport of soil by construction equipment from unpaved to paved surfaces, rinsing of construction equipment with water or any other equivalent method.
- Use of clean fuels including ultra-low sulfur diesel fuel (15 ppm sulfur), compressed natural gas or emulsified fuels.
- Eliminating any unnecessary idling of construction vehicles to no more than three minutes.

## **MITIGATION**

It is not anticipated that any short-term or long-term adverse air quality impacts will occur as a result of the project. Therefore, no specific air quality mitigation measures are proposed.

## **APPENDIX A**

### **MOBILE6.2 Model Input / Output**



## MOBILE6.2 Input Files

### 2010 Run - Fairfield County

#### MOBILE6 INPUT FILE :

> Generic 2010 Winter CO Intersection Inputs for Hartford & Southwest CT Maintenance Areas, as well as all other areas of Connecticut, EXCEPT the New Haven Maintenance Area.

SPREADSHEET :  
POLLUTANTS : CO

#### RUN DATA

> 2010 Generic Run for Intersection Analysis in Fairfield County, CT

> April, 2011

>

> \*\*\*\*\*

> Note that the composite emission factors produced with this input file include both start and running emissions. EPA Guidance indicates that start emissions are typically negligible at intersections; therefore, use of composite emission factors will produce CO impacts that are conservatively high. If modeled impacts (including background CO) approach or exceed the CO NAAQS, consult CTDEP to discuss applying a more refined method that excludes start emissions.

> \*\*\*\*\*

>

>\*\*\*\*\* Expressway Freeflow (USE FOR FREEWAYS ONLY, NOT RAMPS)

#### \* Northeast NLEV inputs

94+ LDG IMP : NLEVNE.D

#### \* Fuel Data

FUEL PROGRAM : 2 N

NO REFUELING :

>2002 Registration Age distribution most recent data available

REG DIST : CTreg05.d

#### \* I/M Data

I/M DESC FILE : CTIM05pl.d

ANTI-TAMP PROG :

83 71 50 22222 21111111 1 12 096. 12111112

#### \* VMT Data

VMT BY HOUR : cthvmt09.def

SPEED VMT : 10svmt1W.cty

VMT BY FACILITY : FCVMTF.CTY

#### \* 2010 expressway/ramp VMT fractions

VMT FRACTIONS :

0.3720 0.0935 0.3112 0.0959 0.0441 0.0263 0.0026 0.0022

0.0016 0.0059 0.0069 0.0075 0.0269 0.0013 0.0007 0.0014

SCENARIO RECORD : 2010 winter intersection: Freeway Freeflow @ 55 mph (REPLACE ?? WITH SPEED)

AVERAGE SPEED : 55. Non-Ramp 100.0 0.0 0.0 0.0

CALENDAR YEAR : 2010

EVALUATION MONTH : 1

FUEL RVP : 11.95

#### \* Weather Data for all of CT, EXCEPT New Haven Maintenance Area

MIN/MAX TEMP : 41. 41.

END OF RUN

---

>\*\*\*\*\* Arterial/Collector/Local Freeflow (DO NOT USE FOR RAMPS)

\* Northeast NLEV inputs  
94+ LDG IMP : NLEVNE.D

\* Fuel Data  
FUEL PROGRAM : 2 N  
NO REFUELING :

>2002 Registration Age distribution most recent data available  
REG DIST : CTreg05.d

\* I/M Data  
I/M DESC FILE : CTIM05pl.d  
ANTI-TAMP PROG :  
83 71 50 22222 21111111 1 12 096. 12111112

\* VMT Data  
VMT BY HOUR : cthvmt09.def  
SPEED VMT : 10svmt1W.cty  
VMT BY FACILITY : FCVMTA.CTY

\* 2010 arterial/collector VMT fractions  
VMT FRACTIONS :  
0.3918 0.0985 0.3277 0.1010 0.0464 0.0084 0.0008 0.0007  
0.0005 0.0019 0.0022 0.0024 0.0086 0.0004 0.0002 0.0085

SCENARIO RECORD : 2010 winter intersection: Arterial/Collector/Local @ 25 mph (REPLACE ??? WITH SPEED)  
AVERAGE SPEED : 25. Arterial 0.0 100.0 0.0 0.0  
CALENDAR YEAR : 2010  
EVALUATION MONTH : 1  
FUEL RVP : 11.95

\* Weather Data for Weather Data for all of CT, EXCEPT New Haven Maintenance Area  
MIN/MAX TEMP : 41. 41.

END OF RUN

>\*\*\*\*\* Ramp Freeflow (Use for all freeway ramps; MOBILE6 assumes avg freeflow ramp speed=34.6mph)

\* Northeast NLEV inputs  
94+ LDG IMP : NLEVNE.D

\* Fuel Data  
FUEL PROGRAM : 2 N  
NO REFUELING :

>2002 Registration Age distribution most recent data available  
REG DIST : CTreg05.d

\* I/M Data  
I/M DESC FILE : CTIM05pl.d  
ANTI-TAMP PROG :  
83 71 50 22222 21111111 1 12 096. 12111112

\* VMT Data (File FCVMTR.CTY assigns all VMT for this portion of the M6 run to RAMPS)  
VMT BY FACILITY : FCVMTR.CTY

---

\* VMT Data  
VMT BY HOUR : cthvmt09.def  
SPEED VMT : 10svmt1W.cty  
VMT BY FACILITY : FCVMTR.CTY

\* 2010 expressway/ramp VMT fractions  
VMT FRACTIONS :  
0.3720 0.0935 0.3112 0.0959 0.0441 0.0263 0.0026 0.0022  
0.0016 0.0059 0.0069 0.0075 0.0269 0.0013 0.0007 0.0014

SCENARIO RECORD : 2010 winter intersection: M6 assumes Ramp @ 34.6mph  
CALENDAR YEAR : 2010  
EVALUATION MONTH : 1  
FUEL RVP : 11.95

\* Weather Data for Weather Data for all of CT, EXCEPT New Haven Maintenance Area  
MIN/MAX TEMP : 41. 41.

END OF RUN

>\*\*\*\*\* Arterial/Collector/Local Idle @ 2.5 mph (Use for queues after multiplying by 2.5)

\* Northeast NLEV inputs  
94+ LDG IMP : NLEVNE.D

\* Fuel Data  
FUEL PROGRAM : 2 N  
NO REFUELING :

>2002 Registration Age distribution most recent data available  
REG DIST : CTreg05.d

\* I/M Data  
I/M DESC FILE : CTIM05pl.d  
ANTI-TAMP PROG :  
83 71 50 22222 21111111 1 12 096. 12111112

\* VMT Data  
VMT BY HOUR : cthvmt09.def  
SPEED VMT : 10svmt1W.cty  
VMT BY FACILITY : FCVMTL.CTY

\* 2010 arterial/collector VMT fractions  
VMT FRACTIONS :  
0.3909 0.0982 0.3269 0.1008 0.0463 0.0088 0.0009 0.0007  
0.0005 0.0020 0.0023 0.0025 0.0090 0.0004 0.0002 0.0096

SCENARIO RECORD : 2010 winter intersection: Idle @ 2.5 mph (x 2.5 to get idle rate for CAL3QHC)  
AVERAGE SPEED : 2.5 Arterial 0.0 100.0 0.0 0.0  
CALENDAR YEAR : 2010  
EVALUATION MONTH : 1  
FUEL RVP : 11.95

\* Weather Data for Weather Data for all of CT, EXCEPT New Haven Maintenance Area  
MIN/MAX TEMP : 41. 41.

END OF RUN

**2010 Run - Litchfield County**

MOBILE6 INPUT FILE :

> Generic 2010 Winter CO Intersection Inputs for Hartford & Southwest CT Maintenance Areas, as  
> well as all other areas of Connecticut, EXCEPT the New Haven Maintenance Area.

SPREADSHEET :  
POLLUTANTS : CO

RUN DATA

> 2010 Generic Run for Intersection Analysis in Litchfield County, CT  
> April, 2011

>  
> \*\*\*\*\*  
> Note that the composite emission factors produced with this input file include both start  
> and running emissions. EPA Guidance indicates that start emissions are typically negligible  
> at intersections; therefore, use of composite emission factors will produce CO impacts that  
> are conservatively high. If modeled impacts (including background CO) approach or exceed the  
> CO NAAQS, consult CTDEP to discuss applying a more refined method that excludes start emissions.  
> \*\*\*\*\*  
>

>\*\*\*\*\* Expressway Freeflow (USE FOR FREEWAYS ONLY, NOT RAMPS)

\* Northeast NLEV inputs  
94+ LDG IMP : NLEVNE.D

\* Fuel Data  
FUEL PROGRAM : 2 N  
NO REFUELING :

>2002 Registration Age distribution most recent data available  
REG DIST : CTreg05.d

\* I/M Data  
I/M DESC FILE : CTIM05pl.d  
ANTI-TAMP PROG :  
83 71 50 22222 21111111 1 12 096. 12111112

\* VMT Data  
VMT BY HOUR : cthvmt09.def  
SPEED VMT : 10svmt3W.cty  
VMT BY FACILITY : FCVMTF.CTY

\* 2010 expressway/ramp VMT fractions  
VMT FRACTIONS :  
0.3720 0.0935 0.3112 0.0959 0.0441 0.0263 0.0026 0.0022  
0.0016 0.0059 0.0069 0.0075 0.0269 0.0013 0.0007 0.0014

SCENARIO RECORD : 2010 winter intersection: Freeway Freeflow @ 55 mph (REPLACE ?? WITH SPEED)  
AVERAGE SPEED : 55. Non-Ramp 100.0 0.0 0.0 0.0  
CALENDAR YEAR : 2010  
EVALUATION MONTH : 1  
FUEL RVP : 11.95

\* Weather Data for all of CT, EXCEPT New Haven Maintenance Area  
MIN/MAX TEMP : 41. 41.

END OF RUN

>\*\*\*\*\* Arterial/Collector/Local Freeflow (DO NOT USE FOR RAMPS)

---

\* Northeast NLEV inputs  
94+ LDG IMP : NLEVNE.D

\* Fuel Data  
FUEL PROGRAM : 2 N  
NO REFUELING :

>2002 Registration Age distribution most recent data available  
REG DIST : CTreg05.d

\* I/M Data  
I/M DESC FILE : CTIM05pl.d  
ANTI-TAMP PROG :  
83 71 50 22222 21111111 1 12 096. 12111112

\* VMT Data  
VMT BY HOUR : cthvmt09.def  
SPEED VMT : 10svmt3W.cty  
VMT BY FACILITY : FCVMTA.CTY

\* 2010 arterial/collector VMT fractions  
VMT FRACTIONS :  
0.3918 0.0985 0.3277 0.1010 0.0464 0.0084 0.0008 0.0007  
0.0005 0.0019 0.0022 0.0024 0.0086 0.0004 0.0002 0.0085

SCENARIO RECORD : 2010 winter intersection: Arterial/Collector/Local @ 25 mph (REPLACE ??? WITH SPEED)  
AVERAGE SPEED : 25. Arterial 0.0 100.0 0.0 0.0  
CALENDAR YEAR : 2010  
EVALUATION MONTH : 1  
FUEL RVP : 11.95

\* Weather Data for Weather Data for all of CT, EXCEPT New Haven Maintenance Area  
MIN/MAX TEMP : 41. 41.

END OF RUN

>\*\*\*\*\* Ramp Freeflow (Use for all freeway ramps; MOBILE6 assumes avg freeflow ramp speed=34.6mph)

\* Northeast NLEV inputs  
94+ LDG IMP : NLEVNE.D

\* Fuel Data  
FUEL PROGRAM : 2 N  
NO REFUELING :

>2002 Registration Age distribution most recent data available  
REG DIST : CTreg05.d

\* I/M Data  
I/M DESC FILE : CTIM05pl.d  
ANTI-TAMP PROG :  
83 71 50 22222 21111111 1 12 096. 12111112

\* VMT Data (File FCVMTR.CTY assigns all VMT for this portion of the M6 run to RAMPS)  
VMT BY FACILITY : FCVMTR.CTY

\* VMT Data  
VMT BY HOUR : cthvmt09.def  
SPEED VMT : 10svmt3W.cty

---



VMT BY FACILITY : FCVMTR.CTY

\* 2010 expressway/ramp VMT fractions

VMT FRACTIONS :  
0.3720 0.0935 0.3112 0.0959 0.0441 0.0263 0.0026 0.0022  
0.0016 0.0059 0.0069 0.0075 0.0269 0.0013 0.0007 0.0014

SCENARIO RECORD : 2010 winter intersection: M6 assumes Ramp @ 34.6mph  
CALENDAR YEAR : 2010  
EVALUATION MONTH : 1  
FUEL RVP : 11.95

\* Weather Data for Weather Data for all of CT, EXCEPT New Haven Maintenance Area  
MIN/MAX TEMP : 41. 41.

END OF RUN

>\*\*\*\*\* Arterial/Collector/Local Idle @ 2.5 mph (Use for queues after multiplying by 2.5)

\* Northeast NLEV inputs  
94+ LDG IMP : NLEVNE.D

\* Fuel Data  
FUEL PROGRAM : 2 N  
NO REFUELING :

>2002 Registration Age distribution most recent data available  
REG DIST : CTreg05.d

\* I/M Data  
I/M DESC FILE : CTIM05pl.d  
ANTI-TAMP PROG :  
83 71 50 22222 21111111 1 12 096. 12111112

\* VMT Data  
VMT BY HOUR : cthvmt09.def  
SPEED VMT : 10svmt3W.cty  
VMT BY FACILITY : FCVMTL.CTY

\* 2010 arterial/collector VMT fractions  
VMT FRACTIONS :  
0.3909 0.0982 0.3269 0.1008 0.0463 0.0088 0.0009 0.0007  
0.0005 0.0020 0.0023 0.0025 0.0090 0.0004 0.0002 0.0096

SCENARIO RECORD : 2010 winter intersection: Idle @ 2.5 mph (x 2.5 to get idle rate for CAL3QHC)  
AVERAGE SPEED : 2.5 Arterial 0.0 100.0 0.0 0.0  
CALENDAR YEAR : 2010  
EVALUATION MONTH : 1  
FUEL RVP : 11.95

\* Weather Data for Weather Data for all of CT, EXCEPT New Haven Maintenance Area  
MIN/MAX TEMP : 41. 41.

END OF RUN

---

## 2030 Run – Fairfield County

### MOBILE6 INPUT FILE :

> Generic 2030 Winter CO Intersection Inputs for Hartford & Southwest CT Maintenance Areas, as well as all other areas of Connecticut, EXCEPT the New Haven Maintenance Area.  
SPREADSHEET :  
POLLUTANTS : CO

### RUN DATA

> 2030 Generic Run for Intersection Analysis in Fairfield County, CT  
> April, 2011

>  
> \*\*\*\*\*  
> Note that the composite emission factors produced with this input file include both start and running emissions. EPA Guidance indicates that start emissions are typically negligible at intersections; therefore, use of composite emission factors will produce CO impacts that are conservatively high. If modeled impacts (including background CO) approach or exceed the CO NAAQS, consult CTDEP to discuss applying a more refined method that excludes start emissions.  
> \*\*\*\*\*  
>

>\*\*\*\*\* Expressway Freeflow (USE FOR FREEWAYS ONLY, NOT RAMPS)

\* Northeast NLEV inputs  
94+ LDG IMP : NLEVNE.D

\* Fuel Data  
FUEL PROGRAM : 2 N  
NO REFUELING :

>2002 Registration Age distribution most recent data available  
REG DIST : CTreg05.d

\* I/M Data  
I/M DESC FILE : CTIM05pl.d  
ANTI-TAMP PROG :  
83 71 50 22222 21111111 1 12 096. 12111112

\* VMT Data  
VMT BY HOUR : cthvmt09.def  
SPEED VMT : 30svmt1W.cty  
VMT BY FACILITY : FCVMTF.CTY

\* 2030 expressway/ramp VMT fractions  
VMT FRACTIONS :  
0.2938 0.1070 0.3559 0.1097 0.0505 0.0262 0.0026 0.0022  
0.0017 0.0059 0.0069 0.0075 0.0268 0.0013 0.0007 0.0013

SCENARIO RECORD : 2030 winter intersection: Freeway Freeflow @ 55 mph (REPLACE ?? WITH SPEED)  
AVERAGE SPEED : 55. Non-Ramp 100.0 0.0 0.0 0.0  
CALENDAR YEAR : 2030  
EVALUATION MONTH : 1  
FUEL RVP : 11.95

\* Weather Data for all of CT, EXCEPT New Haven Maintenance Area  
MIN/MAX TEMP : 41. 41.

END OF RUN

>\*\*\*\*\* Arterial/Collector/Local Freeflow (DO NOT USE FOR RAMPS)



\* Northeast NLEV inputs  
94+ LDG IMP : NLEVNE.D

\* Fuel Data  
FUEL PROGRAM : 2 N  
NO REFUELING :

>2002 Registration Age distribution most recent data available  
REG DIST : CTreg05.d

\* I/M Data  
I/M DESC FILE : CTIM05pl.d  
ANTI-TAMP PROG :  
83 71 50 22222 21111111 1 12 096. 12111112

\* VMT Data  
VMT BY HOUR : cthvmt09.def  
SPEED VMT : 30svmt1W.cty  
VMT BY FACILITY : FCVMTA.CTY

\* 2030 arterial/collector VMT fractions  
VMT FRACTIONS :  
0.3094 0.1126 0.3747 0.1155 0.0532 0.0084 0.0008 0.0007  
0.0005 0.0019 0.0022 0.0024 0.0086 0.0004 0.0002 0.0085

SCENARIO RECORD : 2030 winter intersection: Arterial/Collector/Local @ 25 mph (REPLACE ??? WITH SPEED)  
AVERAGE SPEED : 25. Arterial 0.0 100.0 0.0 0.0  
CALENDAR YEAR : 2030  
EVALUATION MONTH : 1  
FUEL RVP : 11.95

\* Weather Data for Weather Data for all of CT, EXCEPT New Haven Maintenance Area  
MIN/MAX TEMP : 41. 41.

END OF RUN

>\*\*\*\*\* Ramp Freeflow (Use for all freeway ramps; MOBILE6 assumes avg freeflow ramp speed=34.6mph)

\* Northeast NLEV inputs  
94+ LDG IMP : NLEVNE.D

\* Fuel Data  
FUEL PROGRAM : 2 N  
NO REFUELING :

>2002 Registration Age distribution most recent data available  
REG DIST : CTreg05.d

\* I/M Data  
I/M DESC FILE : CTIM05pl.d  
ANTI-TAMP PROG :  
83 71 50 22222 21111111 1 12 096. 12111112

\* VMT Data (File FCVMTR.CTY assigns all VMT for this portion of the M6 run to RAMPS)  
VMT BY FACILITY : FCVMTR.CTY

\* VMT Data  
VMT BY HOUR : cthvmt09.def  
SPEED VMT : 30svmt1W.cty

---

VMT BY FACILITY : FCVMTR.CTY

\* 2030 expressway/ramp VMT fractions

VMT FRACTIONS :  
0.2938 0.1070 0.3559 0.1097 0.0505 0.0262 0.0026 0.0022  
0.0017 0.0059 0.0069 0.0075 0.0268 0.0013 0.0007 0.0013

SCENARIO RECORD : 2030 winter intersection: M6 assumes Ramp @ 34.6mph  
CALENDAR YEAR : 2030  
EVALUATION MONTH : 1  
FUEL RVP : 11.95

\* Weather Data for Weather Data for all of CT, EXCEPT New Haven Maintenance Area  
MIN/MAX TEMP : 41. 41.

END OF RUN

>\*\*\*\*\* Arterial/Collector/Local Idle @ 2.5 mph (Use for queues after multiplying by 2.5)

\* Northeast NLEV inputs  
94+ LDG IMP : NLEVNE.D

\* Fuel Data  
FUEL PROGRAM : 2 N  
NO REFUELING :

>2002 Registration Age distribution most recent data available  
REG DIST : CTreg05.d

\* I/M Data  
I/M DESC FILE : CTIM05pl.d  
ANTI-TAMP PROG :  
83 71 50 22222 21111111 1 12 096. 12111112

\* VMT Data  
VMT BY HOUR : cthvmt09.def  
SPEED VMT : 30svmt1W.cty  
VMT BY FACILITY : FCVMTL.CTY

\* 2030 arterial/collector VMT fractions  
VMT FRACTIONS :  
0.3087 0.1123 0.3738 0.1152 0.0530 0.0088 0.0009 0.0007  
0.0006 0.0020 0.0023 0.0025 0.0090 0.0004 0.0002 0.0096

SCENARIO RECORD : 2030 winter intersection: Idle @ 2.5 mph (x 2.5 to get idle rate for CAL3QHC)  
AVERAGE SPEED : 2.5 Arterial 0.0 100.0 0.0 0.0  
CALENDAR YEAR : 2030  
EVALUATION MONTH : 1  
FUEL RVP : 11.95

\* Weather Data for Weather Data for all of CT, EXCEPT New Haven Maintenance Area  
MIN/MAX TEMP : 41. 41.

END OF RUN

## 2030 Run – Litchfield County

### MOBILE6 INPUT FILE :

> Generic 2030 Winter CO Intersection Inputs for Hartford & Southwest CT Maintenance Areas, as well as all other areas of Connecticut, EXCEPT the New Haven Maintenance Area.  
SPREADSHEET :  
POLLUTANTS : CO

### RUN DATA

> 2030 Generic Run for Intersection Analysis in Litchfield County, CT  
> April, 2011

>  
> \*\*\*\*\*  
> Note that the composite emission factors produced with this input file include both start and running emissions. EPA Guidance indicates that start emissions are typically negligible at intersections; therefore, use of composite emission factors will produce CO impacts that are conservatively high. If modeled impacts (including background CO) approach or exceed the CO NAAQS, consult CTDEP to discuss applying a more refined method that excludes start emissions.  
> \*\*\*\*\*  
>

>\*\*\*\*\* Expressway Freeflow (USE FOR FREEWAYS ONLY, NOT RAMPS)

\* Northeast NLEV inputs  
94+ LDG IMP : NLEVNE.D

\* Fuel Data  
FUEL PROGRAM : 2 N  
NO REFUELING :

>2002 Registration Age distribution most recent data available  
REG DIST : CTreg05.d

\* I/M Data  
I/M DESC FILE : CTIM05pl.d  
ANTI-TAMP PROG :  
83 71 50 22222 21111111 1 12 096. 12111112

\* VMT Data  
VMT BY HOUR : cthvmt09.def  
SPEED VMT : 30svmt3W.cty  
VMT BY FACILITY : FCVMTF.CTY

\* 2030 expressway/ramp VMT fractions  
VMT FRACTIONS :  
0.2938 0.1070 0.3559 0.1097 0.0505 0.0262 0.0026 0.0022  
0.0017 0.0059 0.0069 0.0075 0.0268 0.0013 0.0007 0.0013

SCENARIO RECORD : 2030 winter intersection: Freeway Freeflow @ 55 mph (REPLACE ?? WITH SPEED)  
AVERAGE SPEED : 55. Non-Ramp 100.0 0.0 0.0 0.0  
CALENDAR YEAR : 2030  
EVALUATION MONTH : 1  
FUEL RVP : 11.95

\* Weather Data for all of CT, EXCEPT New Haven Maintenance Area  
MIN/MAX TEMP : 41. 41.

END OF RUN

>\*\*\*\*\* Arterial/Collector/Local Freeflow (DO NOT USE FOR RAMPS)

\* Northeast NLEV inputs  
94+ LDG IMP : NLEVNE.D

\* Fuel Data  
FUEL PROGRAM : 2 N  
NO REFUELING :

>2002 Registration Age distribution most recent data available  
REG DIST : CTreg05.d

\* I/M Data  
I/M DESC FILE : CTIM05pl.d  
ANTI-TAMP PROG :  
83 71 50 22222 21111111 1 12 096. 12111112

\* VMT Data  
VMT BY HOUR : cthvmt09.def  
SPEED VMT : 30svmt3W.cty  
VMT BY FACILITY : FCVMTA.CTY

\* 2030 arterial/collector VMT fractions  
VMT FRACTIONS :  
0.3094 0.1126 0.3747 0.1155 0.0532 0.0084 0.0008 0.0007  
0.0005 0.0019 0.0022 0.0024 0.0086 0.0004 0.0002 0.0085

SCENARIO RECORD : 2030 winter intersection: Arterial/Collector/Local @ 25 mph (REPLACE ??? WITH SPEED)  
AVERAGE SPEED : 25. Arterial 0.0 100.0 0.0 0.0  
CALENDAR YEAR : 2030  
EVALUATION MONTH : 1  
FUEL RVP : 11.95

\* Weather Data for Weather Data for all of CT, EXCEPT New Haven Maintenance Area  
MIN/MAX TEMP : 41. 41.

END OF RUN

>\*\*\*\*\* Ramp Freeflow (Use for all freeway ramps; MOBILE6 assumes avg freeflow ramp speed=34.6mph)

\* Northeast NLEV inputs  
94+ LDG IMP : NLEVNE.D

\* Fuel Data  
FUEL PROGRAM : 2 N  
NO REFUELING :

>2002 Registration Age distribution most recent data available  
REG DIST : CTreg05.d

\* I/M Data  
I/M DESC FILE : CTIM05pl.d  
ANTI-TAMP PROG :  
83 71 50 22222 21111111 1 12 096. 12111112

\* VMT Data (File FCVMTR.CTY assigns all VMT for this portion of the M6 run to RAMPS)  
VMT BY FACILITY : FCVMTR.CTY

\* VMT Data  
VMT BY HOUR : cthvmt09.def  
SPEED VMT : 30svmt3W.cty

---

VMT BY FACILITY : FCVMTR.CTY

\* 2030 expressway/ramp VMT fractions

VMT FRACTIONS :  
0.2938 0.1070 0.3559 0.1097 0.0505 0.0262 0.0026 0.0022  
0.0017 0.0059 0.0069 0.0075 0.0268 0.0013 0.0007 0.0013

SCENARIO RECORD : 2030 winter intersection: M6 assumes Ramp @ 34.6mph  
CALENDAR YEAR : 2030  
EVALUATION MONTH : 1  
FUEL RVP : 11.95

\* Weather Data for Weather Data for all of CT, EXCEPT New Haven Maintenance Area  
MIN/MAX TEMP : 41. 41.

END OF RUN

>\*\*\*\*\* Arterial/Collector/Local Idle @ 2.5 mph (Use for queues after multiplying by 2.5)

\* Northeast NLEV inputs  
94+ LDG IMP : NLEVNE.D

\* Fuel Data  
FUEL PROGRAM : 2 N  
NO REFUELING :

>2002 Registration Age distribution most recent data available  
REG DIST : CTreg05.d

\* I/M Data  
I/M DESC FILE : CTIM05pl.d  
ANTI-TAMP PROG :  
83 71 50 22222 21111111 1 12 096. 12111112

\* VMT Data  
VMT BY HOUR : cthvmt09.def  
SPEED VMT : 30svmt3W.cty  
VMT BY FACILITY : FCVMTL.CTY

\* 2030 arterial/collector VMT fractions  
VMT FRACTIONS :  
0.3087 0.1123 0.3738 0.1152 0.0530 0.0088 0.0009 0.0007  
0.0006 0.0020 0.0023 0.0025 0.0090 0.0004 0.0002 0.0096

SCENARIO RECORD : 2030 winter intersection: Idle @ 2.5 mph (x 2.5 to get idle rate for CAL3QHC)  
AVERAGE SPEED : 2.5 Arterial 0.0 100.0 0.0 0.0  
CALENDAR YEAR : 2030  
EVALUATION MONTH : 1  
FUEL RVP : 11.95

\* Weather Data for Weather Data for all of CT, EXCEPT New Haven Maintenance Area  
MIN/MAX TEMP : 41. 41.

END

OF

RUN

---

## MOBILE6.2 Output Files

### 2010 Run – Fairfield County

\*\*\*\*\*

\* MOBILE6.2.03 (24-Sep-2003) \*  
\* Input file: C:\MOBILE62\MOBILE6\RUN\FAIR10.IN (file 1, run 1). \*  
\*\*\*\*\*

\* 2010 Generic Run for Intersection Analysis in Fairfield County, CT  
\* April, 2011  
\*

\*\*\*\*\*

\* Note that the composite emission factors produced with this input file include both start  
\* and running emissions. EPA Guidance indicates that start emissions are typically negligible  
\* at intersections; therefore, use of composite emission factors will produce CO impacts that  
\* are conservatively high. If modeled impacts (including background CO) approach or exceed the  
\* CO NAAQS, consult CTDEP to discuss applying a more refined method that excludes start emissions.  
\*\*\*\*\*

\*

\*\*\*\*\* Expressway Freeflow (USE FOR FREEWAYS ONLY, NOT RAMPS)

\* Reading 94+ LEV IMPLEMENTATION SCHEDULE from the following external  
\* data file: NLEVNE.D  
M616 Comment:  
User has supplied post-1999 sulfur levels.  
M603 Comment:  
User has disabled the calculation of REFUELING emissions.

\*2002 Registration Age distribution most recent data available

\* Reading Registration Distributions from the following external  
\* data file: CTREG05.D

M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)  
M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)  
M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)  
M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)  
M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)  
M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)  
M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)

\* Reading I/M program description records from the following external  
\* data file: CTIM05PL.D

\*CT I/M PROGRAMS for all years 2005 and later (modified Jun 05 PMB/AG to reflect DMV info that 8,501-  
10,000 lb get TSI & GC (no OBD)  
\*Biennial OBDII I/M "tailpipe" test for post-MY1995 gasoline vehicles up to 8,500 lbs GVWR. Program start  
year reflects OBD test that replaced the ASM  
\*Biennial OBDII evaporative "test" for post-MY1995 gasoline vehicles up to 8,500 lbs GVWR  
\*Biennial 2500/IDLE I/M tailpipe test for all HDGT 8,501 - 10,000 lbs GVWR (per above comment)  
\*Biennial GC evaporative "test" for all HDGT 8,501 - 10,000 lbs (per above comment)  
\*Biennial ASM I/M tailpipe test for pre-96 gasoline vehicles up to 8,500 lbs GVWR

\* Reading ASM I/M Test Credits from ASMDATA.D  
\*Biennial Gas Cap evaporative test for pre-96 gasoline vehicles up to 8,500 lbs GVWR

---



- \* Reading Hourly VMT distribution from the following external  
\* data file: CTHVMT09.DEF
- \* Reading Hourly, Roadway, and Speed VMT dist. from the following external  
\* data file: 10SVMT1W.CTY
- \* Reading Hourly Roadway VMT distribution from the following external  
\* data file: FCVMTF.CTY

Reading User Supplied ROADWAY VMT Factors  
M615 Comment:  
User supplied VMT mix.

- \* #####
- \* 2010 winter intersection: Freeway Freeflow @ 55 mph (REPLACE ?? WITH SPEED)
- \* File 1, Run 1, Scenario 1.
- \* #####

M581 Warning:  
The user supplied freeway average speed of 55.0  
will be used for all hours of the day. 100% of VMT  
has been assigned to the freeway roadway type for  
all hours of the day and all vehicle types.

M112 Warning:  
Wintertime Reformulated Gasoline Rules Apply

- \*\*\* I/M credits for Tech1&2 vehicles were read from the following external  
data file: TECH12.D

M 48 Warning:  
there are no sales for vehicle class HDGV8b

LEV phase-in data read from file NLEVNE.D  
Calendar Year: 2010

Month: Jan.  
Altitude: Low  
Minimum Temperature: 41.0 (F)  
Maximum Temperature: 41.0 (F)  
Absolute Humidity: 75. grains/lb  
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: Yes  
Evap I/M Program: Yes  
ATP Program: Yes  
Reformulated Gas: Yes

| Vehicle Type:     | LDGV   | LDGT12 | LDGT34 | LDGT | HDGV   | LDDV   | LDDT   | HDDV   | MC     |
|-------------------|--------|--------|--------|------|--------|--------|--------|--------|--------|
| All Veh           |        |        |        |      |        |        |        |        |        |
| GVWR:             | <6000  | >6000  | (All)  |      |        |        |        |        |        |
| VMT Distribution: | 0.3717 | 0.4047 | 0.1379 |      | 0.0241 | 0.0003 | 0.0021 | 0.0578 | 0.0014 |
| 1.0000            |        |        |        |      |        |        |        |        |        |

-----

Composite Emission Factors (g/mi):

|                |       |       |       |       |      |       |       |       |       |
|----------------|-------|-------|-------|-------|------|-------|-------|-------|-------|
| Composite CO : | 12.61 | 12.70 | 13.50 | 12.90 | 6.75 | 0.755 | 0.430 | 1.264 | 10.45 |
| 11.938         |       |       |       |       |      |       |       |       |       |

-----

- \*\*\*\*\*
- \* MOBILE6.2.03 (24-Sep-2003) \*
- \* Input file: C:\MOBILE62\MOBILE6\RUN\FAIR10.IN (file 1, run 2). \*
- \*\*\*\*\*
- \*\*\*\*\* Arterial/Collector/Local Freeflow (DO NOT USE FOR RAMPS)

- \* Reading 94+ LEV IMPLEMENTATION SCHEDULE from the following external
-

\* data file: NLEVNE.D  
M616 Comment:  
    User has supplied post-1999 sulfur levels.  
M603 Comment:  
    User has disabled the calculation of REFUELING emissions.

\*2002 Registration Age distribution most recent data available

\* Reading Registration Distributions from the following external

\* data file: CTREG05.D

M 49 Warning:  
    1.00 MYR sum not = 1. (will normalize)  
M 49 Warning:  
    1.00 MYR sum not = 1. (will normalize)  
M 49 Warning:  
    1.00 MYR sum not = 1. (will normalize)  
M 49 Warning:  
    1.00 MYR sum not = 1. (will normalize)  
M 49 Warning:  
    1.00 MYR sum not = 1. (will normalize)  
M 49 Warning:  
    1.00 MYR sum not = 1. (will normalize)  
M 49 Warning:  
    1.00 MYR sum not = 1. (will normalize)  
M 49 Warning:  
    1.00 MYR sum not = 1. (will normalize)

\* Reading I/M program description records from the following external

\* data file: CTIM05PL.D

\*CT I/M PROGRAMS for all years 2005 and later (modified Jun 05 PMB/AG to reflect DMV info that 8,501 - 10,000 lb get TSI & GC (no OBD)  
\*Biennial OBDII I/M "tailpipe" test for post-MY1995 gasoline vehicles up to 8,500 lbs GVWR. Program start year reflects OBD test that replaced the ASM  
\*Biennial OBDII evaporative "test" for post-MY1995 gasoline vehicles up to 8,500 lbs GVWR  
\*Biennial 2500/IDLE I/M tailpipe test for all HDGT 8,501 - 10,000 lbs GVWR (per above comment)  
\*Biennial GC evaporative "test" for all HDGT 8,501 - 10,000 lbs (per above comment)  
\*Biennial ASM I/M tailpipe test for pre-96 gasoline vehicles up to 8,500 lbs GVWR

\* Reading ASM I/M Test Credits from ASMDATA.D

\*Biennial Gas Cap evaporative test for pre-96 gasoline vehicles up to 8,500 lbs GVWR

\* Reading Hourly VMT distribution from the following external

\* data file: CTHVMT09.DEF

\* Reading Hourly, Roadway, and Speed VMT dist. from the following external

\* data file: 10SVMT1W.CTY

\* Reading Hourly Roadway VMT distribution from the following external

\* data file: FCVMTA.CTY

Reading User Supplied ROADWAY VMT Factors

M615 Comment:

    User supplied VMT mix.

\* #####

\* 2010 winter intersection: Arterial/Collector/Local @ 25 mph (REPLACE ??? WITH SPEED)

\* File 1, Run 2, Scenario 1.

\* #####

M583 Warning:

    The user supplied arterial average speed of 25.0  
    will be used for all hours of the day. 100% of VMT  
    has been assigned to the arterial/collector roadway  
    type for all hours of the day and all vehicle types.

---

M112 Warning:

Wintertime Reformulated Gasoline Rules Apply

\*\*\* I/M credits for Tech1&2 vehicles were read from the following external data file: TECH12.D

M 48 Warning:

there are no sales for vehicle class HDGV8b

LEV phase-in data read from file NLEVNE.D

Calendar Year: 2010

Month: Jan.

Altitude: Low

Minimum Temperature: 41.0 (F)

Maximum Temperature: 41.0 (F)

Absolute Humidity: 75. grains/lb

Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: Yes

Evap I/M Program: Yes

ATP Program: Yes

Reformulated Gas: Yes

| Vehicle Type:     | LDGV   | LDGT12 | LDGT34 | LDGT | HDGV   | LDDV   | LDDT   | HDDV   | MC     |
|-------------------|--------|--------|--------|------|--------|--------|--------|--------|--------|
| All Veh           |        |        |        |      |        |        |        |        |        |
| GVWR:             | <6000  | >6000  | (All)  |      |        |        |        |        |        |
| VMT Distribution: | 0.3914 | 0.4262 | 0.1452 |      | 0.0077 | 0.0004 | 0.0022 | 0.0184 | 0.0085 |
| 1.0000            |        |        |        |      |        |        |        |        |        |

-----  
Composite Emission Factors (g/mi):

|                |       |       |       |       |      |       |       |       |       |
|----------------|-------|-------|-------|-------|------|-------|-------|-------|-------|
| Composite CO : | 11.30 | 11.30 | 11.97 | 11.47 | 9.11 | 0.974 | 0.571 | 1.996 | 15.59 |
| 11.219         |       |       |       |       |      |       |       |       |       |

-----  
\*\*\*\*\*

\* MOBILE6.2.03 (24-Sep-2003) \*

\* Input file: C:\MOBILE62\MOBILE6\RUN\FAIR10.IN (file 1, run 3). \*

\*\*\*\*\*

\*\*\*\*\* Ramp Freeflow (Use for all freeway ramps; MOBILE6 assumes avg freeflow ramp speed=34.6mph)

\* Reading 94+ LEV IMPLEMENTATION SCHEDULE from the following external

\* data file: NLEVNE.D

M616 Comment:

User has supplied post-1999 sulfur levels.

M603 Comment:

User has disabled the calculation of REFUELING emissions.

\*2002 Registration Age distribution most recent data available

\* Reading Registration Distributions from the following external

\* data file: CTREG05.D

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)  
M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)

- \* Reading I/M program description records from the following external
- \* data file: CTIM05PL.D
- \*CT I/M PROGRAMS for all years 2005 and later (modified Jun 05 PMB/AG to reflect DMV info that 8,501-10,000 lb get TSI & GC (no OBD)
- \*Biennial OBDII I/M "tailpipe" test for post-MY1995 gasoline vehicles up to 8,500 lbs GVWR. Program start year reflects OBD test that replaced the ASM
- \*Biennial OBDII evaporative "test" for post-MY1995 gasoline vehicles up to 8,500 lbs GVWR
- \*Biennial 2500/IDLE I/M tailpipe test for all HDGT 8,501 - 10,000 lbs GVWR (per above comment)
- \*Biennial GC evaporative "test" for all HDGT 8,501 - 10,000 lbs (per above comment)
- \*Biennial ASM I/M tailpipe test for pre-96 gasoline vehicles up to 8,500 lbs GVWR

- \* Reading ASM I/M Test Credits from ASMDATA.D
- \*Biennial Gas Cap evaporative test for pre-96 gasoline vehicles up to 8,500 lbs GVWR

- \* Reading Hourly Roadway VMT distribution from the following external
- \* data file: FCVMTR.CTY

Reading User Supplied ROADWAY VMT Factors

- \* Reading Hourly VMT distribution from the following external
- \* data file: CTHVMT09.DEF
- \* Reading Hourly, Roadway, and Speed VMT dist. from the following external
- \* data file: 10SVMT1W.CTY
- \* Reading Hourly Roadway VMT distribution from the following external
- \* data file: FCVMTR.CTY

Reading User Supplied ROADWAY VMT Factors  
M615 Comment:

User supplied VMT mix.

- \* #####
- \* 2010 winter intersection: M6 assumes Ramp @ 34.6mph
- \* File 1, Run 3, Scenario 1.
- \* #####

M112 Warning:

Wintertime Reformulated Gasoline Rules Apply

- \*\*\* I/M credits for Tech1&2 vehicles were read from the following external
- data file: TECH12.D

M 48 Warning:

there are no sales for vehicle class HDGV8b

LEV phase-in data read from file NLEVNE.D

Calendar Year: 2010

Month: Jan.

Altitude: Low

Minimum Temperature: 41.0 (F)

Maximum Temperature: 41.0 (F)

Absolute Humidity: 75. grains/lb

Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: Yes

Evap I/M Program: Yes

ATP Program: Yes

Reformulated Gas: Yes



| Vehicle Type:     | LDGV   | LDGT12 | LDGT34 | LDGT | HDGV   | LDDV   | LDDT   | HDDV   | MC     |
|-------------------|--------|--------|--------|------|--------|--------|--------|--------|--------|
| All Veh           |        |        |        |      |        |        |        |        |        |
| GVWR:             | <6000  | >6000  | (All)  |      |        |        |        |        |        |
| VMT Distribution: | 0.3717 | 0.4047 | 0.1379 |      | 0.0241 | 0.0003 | 0.0021 | 0.0578 | 0.0014 |
| 1.0000            |        |        |        |      |        |        |        |        |        |

-----  
Composite Emission Factors (g/mi):

|                |       |       |       |       |      |       |       |       |       |
|----------------|-------|-------|-------|-------|------|-------|-------|-------|-------|
| Composite CO : | 15.40 | 14.89 | 15.37 | 15.01 | 6.68 | 0.808 | 0.465 | 1.442 | 12.32 |
| 14.130         |       |       |       |       |      |       |       |       |       |

-----  
\*\*\*\*\*

\* MOBILE6.2.03 (24-Sep-2003) \*

\* Input file: C:\MOBILE62\MOBILE6\RUN\FAIR10.IN (file 1, run 4). \*

\*\*\*\*\*

\*\*\*\*\* Arterial/Collector/Local Idle @ 2.5 mph (Use for queues after multiplying by 2.5)

\* Reading 94+ LEV IMPLEMENTATION SCHEDULE from the following external

\* data file: NLEVNE.D

M616 Comment:

User has supplied post-1999 sulfur levels.

M603 Comment:

User has disabled the calculation of REFUELING emissions.

\*2002 Registration Age distribution most recent data available

\* Reading Registration Distributions from the following external

\* data file: CTREG05.D

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

\* Reading I/M program description records from the following external

\* data file: CTIM05PL.D

\*CT I/M PROGRAMS for all years 2005 and later (modified Jun 05 PMB/AG to reflect DMV info that 8,501-10,000 lb get TSI & GC (no OBD)

\*Biennial OBDII I/M "tailpipe" test for post-MY1995 gasoline vehicles up to 8,500 lbs GVWR. Program start year reflects OBD test that replaced the ASM

\*Biennial OBDII evaporative "test" for post-MY1995 gasoline vehicles up to 8,500 lbs GVWR

\*Biennial 2500/IDLE I/M tailpipe test for all HDGT 8,501 - 10,000 lbs GVWR (per above comment)

\*Biennial GC evaporative "test" for all HDGT 8,501 - 10,000 lbs (per above comment)

\*Biennial ASM I/M tailpipe test for pre-96 gasoline vehicles up to 8,500 lbs GVWR

\* Reading ASM I/M Test Credits from ASMDATA.D

\*Biennial Gas Cap evaporative test for pre-96 gasoline vehicles up to 8,500 lbs GVWR

\* Reading Hourly VMT distribution from the following external

\* data file: CTHVMT09.DEF

\* Reading Hourly, Roadway, and Speed VMT dist. from the following external

---

\* data file: 10SVMT1W.CTY

\* Reading Hourly Roadway VMT distribution from the following external  
\* data file: FCVMTL.CTY

Reading User Supplied ROADWAY VMT Factors

M615 Comment:

User supplied VMT mix.

\* #####

\* 2010 winter intersection: Idle @ 2.5 mph (x 2.5 to get idle rate for CAL3QHC)

\* File 1, Run 4, Scenario 1.

\* #####

M583 Warning:

The user supplied arterial average speed of 2.5  
will be used for all hours of the day. 100% of VMT  
has been assigned to the arterial/collector roadway  
type for all hours of the day and all vehicle types.

M112 Warning:

Wintertime Reformulated Gasoline Rules Apply

\*\*\* I/M credits for Tech1&2 vehicles were read from the following external  
data file: TECH12.D

M 48 Warning:

there are no sales for vehicle class HDGV8b

LEV phase-in data read from file NLEVNE.D

Calendar Year: 2010

Month: Jan.

Altitude: Low

Minimum Temperature: 41.0 (F)

Maximum Temperature: 41.0 (F)

Absolute Humidity: 75. grains/lb

Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: Yes

Evap I/M Program: Yes

ATP Program: Yes

Reformulated Gas: Yes

| Vehicle Type: | LDGV  | LDGT12 | LDGT34 | LDGT | HDGV | LDDV | LDDT | HDDV | MC |
|---------------|-------|--------|--------|------|------|------|------|------|----|
| All Veh       |       |        |        |      |      |      |      |      |    |
| GVWR:         | <6000 | >6000  | (All)  |      |      |      |      |      |    |

|                   |        |        |        |  |        |        |        |        |        |
|-------------------|--------|--------|--------|--|--------|--------|--------|--------|--------|
| VMT Distribution: | 0.3905 | 0.4251 | 0.1449 |  | 0.0080 | 0.0004 | 0.0022 | 0.0193 | 0.0096 |
| 1.0000            |        |        |        |  |        |        |        |        |        |

-----  
Composite Emission Factors (g/mi):

|                |       |       |       |       |       |       |       |       |        |
|----------------|-------|-------|-------|-------|-------|-------|-------|-------|--------|
| Composite CO : | 25.04 | 24.18 | 27.40 | 25.00 | 41.82 | 2.845 | 1.768 | 8.226 | 100.86 |
| 25.498         |       |       |       |       |       |       |       |       |        |



## 2010 Run – Litchfield County

\*\*\*\*\*

\* MOBILE6.2.03 (24-Sep-2003) \*  
\* Input file: C:\MOBILE62\MOBILE6\RUN\LITCH10.IN (file 1, run 1). \*  
\*\*\*\*\*

\* 2010 Generic Run for Intersection Analysis in Litchfield County, CT  
\* April, 2011  
\*

\*\*\*\*\*

\* Note that the composite emission factors produced with this input file include both start  
\* and running emissions. EPA Guidance indicates that start emissions are typically negligible  
\* at intersections; therefore, use of composite emission factors will produce CO impacts that  
\* are conservatively high. If modeled impacts (including background CO) approach or exceed the  
\* CO NAAQS, consult CTDEP to discuss applying a more refined method that excludes start emissions.  
\*\*\*\*\*

\*

\*\*\*\*\* Expressway Freeflow (USE FOR FREEWAYS ONLY, NOT RAMPS)

\* Reading 94+ LEV IMPLEMENTATION SCHEDULE from the following external  
\* data file: NLEVNE.D  
M616 Comment:  
User has supplied post-1999 sulfur levels.  
M603 Comment:  
User has disabled the calculation of REFUELING emissions.

\*2002 Registration Age distribution most recent data available

\* Reading Registration Distributions from the following external  
\* data file: CTREG05.D  
M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)  
M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)  
M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)  
M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)  
M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)  
M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)  
M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)  
M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)

\* Reading I/M program description records from the following external  
\* data file: CTIM05PL.D  
\*CT I/M PROGRAMS for all years 2005 and later (modified Jun 05 PMB/AG to reflect DMV info that 8,501-  
10,000 lb get TSI & GC (no OBD)  
\*Biennial OBDII I/M "tailpipe" test for post-MY1995 gasoline vehicles up to 8,500 lbs GVWR. Program start  
year reflects OBD test that replaced the ASM  
\*Biennial OBDII evaporative "test" for post-MY1995 gasoline vehicles up to 8,500 lbs GVWR  
\*Biennial 2500/IDLE I/M tailpipe test for all HDGT 8,501 - 10,000 lbs GVWR (per above comment)  
\*Biennial GC evaporative "test" for all HDGT 8,501 - 10,000 lbs (per above comment)  
\*Biennial ASM I/M tailpipe test for pre-96 gasoline vehicles up to 8,500 lbs GVWR

\* Reading ASM I/M Test Credits from ASMDATA.D  
\*Biennial Gas Cap evaporative test for pre-96 gasoline vehicles up to 8,500 lbs GVWR

\* Reading Hourly VMT distribution from the following external  
\* data file: CTHVMT09.DEF

---

\* Reading Hourly, Roadway, and Speed VMT dist. from the following external  
\* data file: 10SVMT3W.CTY

\* Reading Hourly Roadway VMT distribution from the following external  
\* data file: FCVMTF.CTY

Reading User Supplied ROADWAY VMT Factors  
M615 Comment:  
User supplied VMT mix.

\* #####  
\* 2010 winter intersection: Freeway Freeflow @ 55 mph (REPLACE ?? WITH SPEED)  
\* File 1, Run 1, Scenario 1.  
\* #####

M581 Warning:  
The user supplied freeway average speed of 55.0  
will be used for all hours of the day. 100% of VMT  
has been assigned to the freeway roadway type for  
all hours of the day and all vehicle types.

M112 Warning:  
Wintertime Reformulated Gasoline Rules Apply

\*\*\* I/M credits for Tech1&2 vehicles were read from the following external  
data file: TECH12.D

M 48 Warning:  
there are no sales for vehicle class HDGV8b

LEV phase-in data read from file NLEVNE.D

Calendar Year: 2010  
Month: Jan.  
Altitude: Low  
Minimum Temperature: 41.0 (F)  
Maximum Temperature: 41.0 (F)  
Absolute Humidity: 75. grains/lb  
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: Yes  
Evap I/M Program: Yes  
ATP Program: Yes  
Reformulated Gas: Yes

| Vehicle Type:                      | LDGV   | LDGT12 | LDGT34 | LDGT  | HDGV   | LDDV   | LDDT   | HDDV   | MC     |
|------------------------------------|--------|--------|--------|-------|--------|--------|--------|--------|--------|
| All Veh                            |        |        |        |       |        |        |        |        |        |
| GVWR:                              | <6000  | >6000  | (All)  |       |        |        |        |        |        |
| VMT Distribution:                  | 0.3717 | 0.4047 | 0.1379 |       | 0.0241 | 0.0003 | 0.0021 | 0.0578 | 0.0014 |
| 1.0000                             |        |        |        |       |        |        |        |        |        |
| -----                              |        |        |        |       |        |        |        |        |        |
| Composite Emission Factors (g/mi): |        |        |        |       |        |        |        |        |        |
| Composite CO :                     | 12.61  | 12.70  | 13.50  | 12.90 | 6.75   | 0.755  | 0.430  | 1.264  | 10.45  |
| 11.938                             |        |        |        |       |        |        |        |        |        |
| -----                              |        |        |        |       |        |        |        |        |        |

\*\*\*\*\*  
\* MOBILE6.2.03 (24-Sep-2003) \*  
\* Input file: C:\MOBILE62\MOBILE6\RUN\LITCH10.IN (file 1, run 2). \*  
\*\*\*\*\*  
\*\*\*\*\* Arterial/Collector/Local Freeflow (DO NOT USE FOR RAMPS)

\* Reading 94+ LEV IMPLEMENTATION SCHEDULE from the following external  
\* data file: NLEVNE.D  
M616 Comment:



User has supplied post-1999 sulfur levels.  
M603 Comment:  
User has disabled the calculation of REFUELING emissions.

\*2002 Registration Age distribution most recent data available

\* Reading Registration Distributions from the following external

\* data file: CTREG05.D

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

\* Reading I/M program description records from the following external

\* data file: CTIM05PL.D

\*CT I/M PROGRAMS for all years 2005 and later (modified Jun 05 PMB/AG to reflect DMV info that 8,501-10,000 lb get TSI & GC (no OBD)

\*Biennial OBDII I/M "tailpipe" test for post-MY1995 gasoline vehicles up to 8,500 lbs GVWR. Program start year reflects OBD test that replaced the ASM

\*Biennial OBDII evaporative "test" for post-MY1995 gasoline vehicles up to 8,500 lbs GVWR

\*Biennial 2500/IDLE I/M tailpipe test for all HDGT 8,501 - 10,000 lbs GVWR (per above comment)

\*Biennial GC evaporative "test" for all HDGT 8,501 - 10,000 lbs (per above comment)

\*Biennial ASM I/M tailpipe test for pre-96 gasoline vehicles up to 8,500 lbs GVWR

\* Reading ASM I/M Test Credits from ASMDATA.D

\*Biennial Gas Cap evaporative test for pre-96 gasoline vehicles up to 8,500 lbs GVWR

\* Reading Hourly VMT distribution from the following external

\* data file: CTHVMT09.DEF

\* Reading Hourly, Roadway, and Speed VMT dist. from the following external

\* data file: 10SVMT3W.CTY

\* Reading Hourly Roadway VMT distribution from the following external

\* data file: FCVMTA.CTY

Reading User Supplied ROADWAY VMT Factors

M615 Comment:

User supplied VMT mix.

\* #####

\* 2010 winter intersection: Arterial/Collector/Local @ 25 mph (REPLACE ??? WITH SPEED)

\* File 1, Run 2, Scenario 1.

\* #####

M583 Warning:

The user supplied arterial average speed of 25.0 will be used for all hours of the day. 100% of VMT has been assigned to the arterial/collector roadway type for all hours of the day and all vehicle types.

M112 Warning:

Wintertime Reformulated Gasoline Rules Apply



\*\*\* I/M credits for Tech1&2 vehicles were read from the following external data file: TECH12.D

M 48 Warning:  
there are no sales for vehicle class HDGV8b

LEV phase-in data read from file NLEVNE.D

Calendar Year: 2010  
Month: Jan.  
Altitude: Low  
Minimum Temperature: 41.0 (F)  
Maximum Temperature: 41.0 (F)  
Absolute Humidity: 75. grains/lb  
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: Yes  
Evap I/M Program: Yes  
ATP Program: Yes  
Reformulated Gas: Yes

| Vehicle Type:                      | LDGV   | LDGT12 | LDGT34 | LDGT  | HDGV   | LDDV   | LDDT   | HDDV   | MC     |
|------------------------------------|--------|--------|--------|-------|--------|--------|--------|--------|--------|
| All Veh                            |        |        |        |       |        |        |        |        |        |
| GVWR:                              | <6000  | >6000  | (All)  |       |        |        |        |        |        |
| VMT Distribution:                  | 0.3914 | 0.4262 | 0.1452 |       | 0.0077 | 0.0004 | 0.0022 | 0.0184 | 0.0085 |
| 1.0000                             |        |        |        |       |        |        |        |        |        |
| -----                              |        |        |        |       |        |        |        |        |        |
| Composite Emission Factors (g/mi): |        |        |        |       |        |        |        |        |        |
| Composite CO :                     | 11.30  | 11.30  | 11.97  | 11.47 | 9.11   | 0.974  | 0.571  | 1.996  | 15.59  |
| 11.219                             |        |        |        |       |        |        |        |        |        |

\*\*\*\*\*

\* MOBILE6.2.03 (24-Sep-2003) \*

\* Input file: C:\MOBILE62\MOBILE6\RUN\LITCH10.IN (file 1, run 3). \*

\*\*\*\*\*

\*\*\*\*\* Ramp Freeflow (Use for all freeway ramps; MOBILE6 assumes avg freeflow ramp speed=34.6mph)

\* Reading 94+ LEV IMPLEMENTATION SCHEDULE from the following external data file: NLEVNE.D

M616 Comment:  
User has supplied post-1999 sulfur levels.

M603 Comment:  
User has disabled the calculation of REFUELING emissions.

\*2002 Registration Age distribution most recent data available

\* Reading Registration Distributions from the following external data file: CTREG05.D

M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)

M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)

M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)

M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)

M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)

M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)

M 49 Warning:



1.00 MYR sum not = 1. (will normalize)

- \* Reading I/M program description records from the following external
- \* data file: CTIM05PL.D
- \*CT I/M PROGRAMS for all years 2005 and later (modified Jun 05 PMB/AG to reflect DMV info that 8,501-10,000 lb get TSI & GC (no OBD)
- \*Biennial OBDII I/M "tailpipe" test for post-MY1995 gasoline vehicles up to 8,500 lbs GVWR. Program start year reflects OBD test that replaced the ASM
- \*Biennial OBDII evaporative "test" for post-MY1995 gasoline vehicles up to 8,500 lbs GVWR
- \*Biennial 2500/IDLE I/M tailpipe test for all HDGT 8,501 - 10,000 lbs GVWR (per above comment)
- \*Biennial GC evaporative "test" for all HDGT 8,501 - 10,000 lbs (per above comment)
- \*Biennial ASM I/M tailpipe test for pre-96 gasoline vehicles up to 8,500 lbs GVWR

- \* Reading ASM I/M Test Credits from ASMDATA.D
- \*Biennial Gas Cap evaporative test for pre-96 gasoline vehicles up to 8,500 lbs GVWR

- \* Reading Hourly Roadway VMT distribution from the following external
- \* data file: FCVMTR.CTY

Reading User Supplied ROADWAY VMT Factors

- \* Reading Hourly VMT distribution from the following external
- \* data file: CTHVMT09.DEF

- \* Reading Hourly, Roadway, and Speed VMT dist. from the following external
- \* data file: 10SVMT3W.CTY

- \* Reading Hourly Roadway VMT distribution from the following external
- \* data file: FCVMTR.CTY

Reading User Supplied ROADWAY VMT Factors

M615 Comment:

User supplied VMT mix.

- \* #####
- \* 2010 winter intersection: M6 assumes Ramp @ 34.6mph
- \* File 1, Run 3, Scenario 1.
- \* #####

M112 Warning:

Wintertime Reformulated Gasoline Rules Apply

- \*\*\* I/M credits for Tech1&2 vehicles were read from the following external
- data file: TECH12.D

M 48 Warning:

there are no sales for vehicle class HDGV8b

LEV phase-in data read from file NLEVNE.D

Calendar Year: 2010

Month: Jan.

Altitude: Low

Minimum Temperature: 41.0 (F)

Maximum Temperature: 41.0 (F)

Absolute Humidity: 75. grains/lb

Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: Yes

Evap I/M Program: Yes

ATP Program: Yes

Reformulated Gas: Yes

Vehicle Type: LDGV LDGT12 LDGT34 LDGT HDGV LDDV LDDT HDDV MC  
 All Veh

| GVWR:             | <6000  | >6000  | (All)  |  |        |        |        |        |        |
|-------------------|--------|--------|--------|--|--------|--------|--------|--------|--------|
| VMT Distribution: | 0.3717 | 0.4047 | 0.1379 |  | 0.0241 | 0.0003 | 0.0021 | 0.0578 | 0.0014 |
| 1.0000            |        |        |        |  |        |        |        |        |        |

-----  
Composite Emission Factors (g/mi):  
Composite CO : 15.40 14.89 15.37 15.01 6.68 0.808 0.465 1.442 12.32  
14.130  
-----

\*\*\*\*\*  
\* MOBILE6.2.03 (24-Sep-2003) \*  
\* Input file: C:\MOBILE62\MOBILE6\RUN\LITCH10.IN (file 1, run 4). \*  
\*\*\*\*\*  
\*\*\*\*\* Arterial/Collector/Local Idle @ 2.5 mph (Use for queues after multiplying by 2.5)

\* Reading 94+ LEV IMPLEMENTATION SCHEDULE from the following external  
\* data file: NLEVNE.D  
M616 Comment:  
User has supplied post-1999 sulfur levels.  
M603 Comment:  
User has disabled the calculation of REFUELING emissions.

\*2002 Registration Age distribution most recent data available

\* Reading Registration Distributions from the following external  
\* data file: CTREG05.D  
M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)  
M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)  
M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)  
M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)  
M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)  
M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)  
M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)  
M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)

\* Reading I/M program description records from the following external  
\* data file: CTIM05PL.D  
\*CT I/M PROGRAMS for all years 2005 and later (modified Jun 05 PMB/AG to reflect DMV info that 8,501-10,000 lb get TSI & GC (no OBD)  
\*Biennial OBDII I/M "tailpipe" test for post-MY1995 gasoline vehicles up to 8,500 lbs GVWR. Program start year reflects OBD test that replaced the ASM  
\*Biennial OBDII evaporative "test" for post-MY1995 gasoline vehicles up to 8,500 lbs GVWR  
\*Biennial 2500/IDLE I/M tailpipe test for all HDGT 8,501 - 10,000 lbs GVWR (per above comment)  
\*Biennial GC evaporative "test" for all HDGT 8,501 - 10,000 lbs (per above comment)  
\*Biennial ASM I/M tailpipe test for pre-96 gasoline vehicles up to 8,500 lbs GVWR

\* Reading ASM I/M Test Credits from ASMDATA.D  
\*Biennial Gas Cap evaporative test for pre-96 gasoline vehicles up to 8,500 lbs GVWR

\* Reading Hourly VMT distribution from the following external  
\* data file: CTHVMT09.DEF

\* Reading Hourly, Roadway, and Speed VMT dist. from the following external  
\* data file: 10SVMT3W.CTY

\* Reading Hourly Roadway VMT distribution from the following external  
 \* data file: FCVMTL.CTY

Reading User Supplied ROADWAY VMT Factors  
 M615 Comment:  
 User supplied VMT mix.

\* #####  
 \* 2010 winter intersection: Idle @ 2.5 mph (x 2.5 to get idle rate for CAL3QHC)  
 \* File 1, Run 4, Scenario 1.  
 \* #####

M583 Warning:  
 The user supplied arterial average speed of 2.5  
 will be used for all hours of the day. 100% of VMT  
 has been assigned to the arterial/collector roadway  
 type for all hours of the day and all vehicle types.

M112 Warning:  
 Wintertime Reformulated Gasoline Rules Apply

\*\*\* I/M credits for Tech1&2 vehicles were read from the following external  
 data file: TECH12.D

M 48 Warning:  
 there are no sales for vehicle class HDGV8b

LEV phase-in data read from file NLEVNE.D

Calendar Year: 2010  
 Month: Jan.  
 Altitude: Low  
 Minimum Temperature: 41.0 (F)  
 Maximum Temperature: 41.0 (F)  
 Absolute Humidity: 75. grains/lb  
 Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: Yes  
 Evap I/M Program: Yes  
 ATP Program: Yes  
 Reformulated Gas: Yes

| Vehicle Type:                      | LDGV   | LDGT12 | LDGT34 | LDGT  | HDGV   | LDDV   | LDDT   | HDDV   | MC     |
|------------------------------------|--------|--------|--------|-------|--------|--------|--------|--------|--------|
| All Veh                            |        |        |        |       |        |        |        |        |        |
| GVWR:                              | <6000  | >6000  | (All)  |       |        |        |        |        |        |
| VMT Distribution:                  | 0.3905 | 0.4251 | 0.1449 |       | 0.0080 | 0.0004 | 0.0022 | 0.0193 | 0.0096 |
| 1.0000                             |        |        |        |       |        |        |        |        |        |
| -----                              |        |        |        |       |        |        |        |        |        |
| Composite Emission Factors (g/mi): |        |        |        |       |        |        |        |        |        |
| Composite CO :                     | 25.04  | 24.18  | 27.40  | 25.00 | 41.82  | 2.845  | 1.768  | 8.226  | 100.86 |
| 25.498                             |        |        |        |       |        |        |        |        |        |
| -----                              |        |        |        |       |        |        |        |        |        |

## 2030 Run – Fairfield County

\*\*\*\*\*

\* MOBILE6.2.03 (24-Sep-2003) \*  
\* Input file: C:\MOBILE62\MOBILE6\RUN\FAIR30.IN (file 1, run 1). \*

\*\*\*\*\*

\* 2030 Generic Run for Intersection Analysis in Fairfield County, CT  
\* April, 2011

\*

\*\*\*\*\*

\* Note that the composite emission factors produced with this input file include both start  
\* and running emissions. EPA Guidance indicates that start emissions are typically negligible  
\* at intersections; therefore, use of composite emission factors will produce CO impacts that  
\* are conservatively high. If modeled impacts (including background CO) approach or exceed the  
\* CO NAAQS, consult CTDEP to discuss applying a more refined method that excludes start emissions.

\*\*\*\*\*

\*

\*\*\*\*\* Expressway Freeflow (USE FOR FREEWAYS ONLY, NOT RAMPS)

\* Reading 94+ LEV IMPLEMENTATION SCHEDULE from the following external  
\* data file: NLEVNE.D

M616 Comment:

User has supplied post-1999 sulfur levels.

M603 Comment:

User has disabled the calculation of REFUELING emissions.

\*2002 Registration Age distribution most recent data available

\* Reading Registration Distributions from the following external

\* data file: CTREG05.D

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

\* Reading I/M program description records from the following external

\* data file: CTIM05PL.D

\*CT I/M PROGRAMS for all years 2005 and later (modified Jun 05 PMB/AG to reflect DMV info that 8,501-  
10,000 lb get TSI & GC (no OBD)

\*Biennial OBDII I/M "tailpipe" test for post-MY1995 gasoline vehicles up to 8,500 lbs GVWR. Program start  
year reflects OBD test that replaced the ASM

\*Biennial OBDII evaporative "test" for post-MY1995 gasoline vehicles up to 8,500 lbs GVWR

\*Biennial 2500/IDLE I/M tailpipe test for all HDGT 8,501 - 10,000 lbs GVWR (per above comment)

\*Biennial GC evaporative "test" for all HDGT 8,501 - 10,000 lbs (per above comment)

\*Biennial ASM I/M tailpipe test for pre-96 gasoline vehicles up to 8,500 lbs GVWR

\* Reading ASM I/M Test Credits from ASMDATA.D

\*Biennial Gas Cap evaporative test for pre-96 gasoline vehicles up to 8,500 lbs GVWR

\* Reading Hourly VMT distribution from the following external

---

\* data file: CTHVMT09.DEF

\* Reading Hourly, Roadway, and Speed VMT dist. from the following external  
\* data file: 30SVMT1W.CTY

\* Reading Hourly Roadway VMT distribution from the following external  
\* data file: FCVMTF.CTY

Reading User Supplied ROADWAY VMT Factors  
M615 Comment:

User supplied VMT mix.

\* #####  
\* 2030 winter intersection: Freeway Freeflow @ 55 mph (REPLACE ?? WITH SPEED)  
\* File 1, Run 1, Scenario 1.

\* #####  
M581 Warning:  
The user supplied freeway average speed of 55.0  
will be used for all hours of the day. 100% of VMT  
has been assigned to the freeway roadway type for  
all hours of the day and all vehicle types.

M112 Warning:  
Wintertime Reformulated Gasoline Rules Apply

\*\*\* I/M credits for Tech1&2 vehicles were read from the following external  
data file: TECH12.D

M 48 Warning:  
there are no sales for vehicle class HDGV8b

M 48 Warning:  
there are no sales for vehicle class LDDT12

LEV phase-in data read from file NLEVNE.D

Calendar Year: 2030

Month: Jan.

Altitude: Low

Minimum Temperature: 41.0 (F)

Maximum Temperature: 41.0 (F)

Absolute Humidity: 75. grains/lb

Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: Yes

Evap I/M Program: Yes

ATP Program: Yes

Reformulated Gas: Yes

Vehicle Type: LDGV LDGT12 LDGT34 LDGT HDGV LDDV LDDT HDDV MC  
All Veh

GVWR: <6000 >6000 (All)

VMT Distribution: 0.2935 0.4629 0.1578 0.0240 0.0003 0.0024 0.0578 0.0013  
1.0000

-----  
Composite Emission Factors (g/mi):

Composite CO : 10.06 9.13 9.08 9.12 5.68 0.475 0.238 0.173 10.45  
8.774  
-----

\*\*\*\*\*

\* MOBILE6.2.03 (24-Sep-2003) \*

\* Input file: C:\MOBILE62\MOBILE6\RUN\FAIR30.IN (file 1, run 2). \*

\*\*\*\*\*

\*\*\*\*\* Arterial/Collector/Local Freeflow (DO NOT USE FOR RAMPS)

\* Reading 94+ LEV IMPLEMENTATION SCHEDULE from the following external  
\* data file: NLEVNE.D

M616 Comment:  
User has supplied post-1999 sulfur levels.

M603 Comment:  
User has disabled the calculation of REFUELING emissions.

\*2002 Registration Age distribution most recent data available

\* Reading Registration Distributions from the following external  
\* data file: CTREG05.D

M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)  
M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)  
M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)  
M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)  
M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)  
M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)  
M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)  
M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)

\* Reading I/M program description records from the following external  
\* data file: CTIM05PL.D

\*CT I/M PROGRAMS for all years 2005 and later (modified Jun 05 PMB/AG to reflect DMV info that 8,501-10,000 lb get TSI & GC (no OBD)  
\*Biennial OBDII I/M "tailpipe" test for post-MY1995 gasoline vehicles up to 8,500 lbs GVWR. Program start year reflects OBD test that replaced the ASM  
\*Biennial OBDII evaporative "test" for post-MY1995 gasoline vehicles up to 8,500 lbs GVWR  
\*Biennial 2500/IDLE I/M tailpipe test for all HDGT 8,501 - 10,000 lbs GVWR (per above comment)  
\*Biennial GC evaporative "test" for all HDGT 8,501 - 10,000 lbs (per above comment)  
\*Biennial ASM I/M tailpipe test for pre-96 gasoline vehicles up to 8,500 lbs GVWR

\* Reading ASM I/M Test Credits from ASMDATA.D  
\*Biennial Gas Cap evaporative test for pre-96 gasoline vehicles up to 8,500 lbs GVWR

\* Reading Hourly VMT distribution from the following external  
\* data file: CTHVMT09.DEF

\* Reading Hourly, Roadway, and Speed VMT dist. from the following external  
\* data file: 30SVMT1W.CTY

\* Reading Hourly Roadway VMT distribution from the following external  
\* data file: FCVMTA.CTY

Reading User Supplied ROADWAY VMT Factors  
M615 Comment:  
User supplied VMT mix.

\* #####  
\* 2030 winter intersection: Arterial/Collector/Local @ 25 mph (REPLACE ??? WITH SPEED)  
\* File 1, Run 2, Scenario 1.  
\* #####

M583 Warning:  
The user supplied arterial average speed of 25.0  
will be used for all hours of the day. 100% of VMT  
has been assigned to the arterial/collector roadway

---



type for all hours of the day and all vehicle types.

M112 Warning:

Wintertime Reformulated Gasoline Rules Apply

\*\*\* I/M credits for Tech1&2 vehicles were read from the following external data file: TECH12.D

M 48 Warning:

there are no sales for vehicle class HDGV8b

M 48 Warning:

there are no sales for vehicle class LDDT12

LEV phase-in data read from file NLEVNE.D

Calendar Year: 2030

Month: Jan.

Altitude: Low

Minimum Temperature: 41.0 (F)

Maximum Temperature: 41.0 (F)

Absolute Humidity: 75. grains/lb

Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: Yes

Evap I/M Program: Yes

ATP Program: Yes

Reformulated Gas: Yes

| Vehicle Type: | LDGV  | LDGT12 | LDGT34 | LDGT  | HDGV | LDDV | LDDT | HDDV | MC |
|---------------|-------|--------|--------|-------|------|------|------|------|----|
| All Veh       | GVWR: | <6000  | >6000  | (All) |      |      |      |      |    |

|                   |        |        |        |  |        |        |        |        |        |
|-------------------|--------|--------|--------|--|--------|--------|--------|--------|--------|
| VMT Distribution: | 0.3091 | 0.4873 | 0.1662 |  | 0.0077 | 0.0003 | 0.0025 | 0.0184 | 0.0085 |
| 1.0000            |        |        |        |  |        |        |        |        |        |

-----  
Composite Emission Factors (g/mi):

|                |      |      |      |      |      |       |       |       |       |
|----------------|------|------|------|------|------|-------|-------|-------|-------|
| Composite CO : | 9.08 | 8.05 | 7.98 | 8.03 | 7.66 | 0.621 | 0.324 | 0.274 | 15.59 |
| 8.252          |      |      |      |      |      |       |       |       |       |

-----  
\*\*\*\*\*

\* MOBILE6.2.03 (24-Sep-2003) \*

\* Input file: C:\MOBILE62\MOBILE6\RUN\FAIR30.IN (file 1, run 3). \*

\*\*\*\*\*

\*\*\*\*\* Ramp Freeflow (Use for all freeway ramps; MOBILE6 assumes avg freeflow ramp speed=34.6mph)

\* Reading 94+ LEV IMPLEMENTATION SCHEDULE from the following external

\* data file: NLEVNE.D

M616 Comment:

User has supplied post-1999 sulfur levels.

M603 Comment:

User has disabled the calculation of REFUELING emissions.

\*2002 Registration Age distribution most recent data available

\* Reading Registration Distributions from the following external

\* data file: CTREG05.D

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)  
M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)  
M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)

\* Reading I/M program description records from the following external  
\* data file: CTIM05PL.D  
\*CT I/M PROGRAMS for all years 2005 and later (modified Jun 05 PMB/AG to reflect DMV info that 8,501-10,000 lb get TSI & GC (no OBD)  
\*Biennial OBDII I/M "tailpipe" test for post-MY1995 gasoline vehicles up to 8,500 lbs GVWR. Program start year reflects OBD test that replaced the ASM  
\*Biennial OBDII evaporative "test" for post-MY1995 gasoline vehicles up to 8,500 lbs GVWR  
\*Biennial 2500/IDLE I/M tailpipe test for all HDGT 8,501 - 10,000 lbs GVWR (per above comment)  
\*Biennial GC evaporative "test" for all HDGT 8,501 - 10,000 lbs (per above comment)  
\*Biennial ASM I/M tailpipe test for pre-96 gasoline vehicles up to 8,500 lbs GVWR  
  
\* Reading ASM I/M Test Credits from ASMDATA.D  
\*Biennial Gas Cap evaporative test for pre-96 gasoline vehicles up to 8,500 lbs GVWR

\* Reading Hourly Roadway VMT distribution from the following external  
\* data file: FCMVTR.CTY

Reading User Supplied ROADWAY VMT Factors

\* Reading Hourly VMT distribution from the following external  
\* data file: CTHVMT09.DEF

\* Reading Hourly, Roadway, and Speed VMT dist. from the following external  
\* data file: 30SVMT1W.CTY

\* Reading Hourly Roadway VMT distribution from the following external  
\* data file: FCMVTR.CTY

Reading User Supplied ROADWAY VMT Factors

M615 Comment:  
User supplied VMT mix.

\* #####  
\* 2030 winter intersection: M6 assumes Ramp @ 34.6mph  
\* File 1, Run 3, Scenario 1.  
\* #####

M112 Warning:  
Wintertime Reformulated Gasoline Rules Apply  
\*\*\* I/M credits for Tech1&2 vehicles were read from the following external  
data file: TECH12.D  
M 48 Warning:  
there are no sales for vehicle class HDGV8b  
M 48 Warning:  
there are no sales for vehicle class LDDT12

LEV phase-in data read from file NLEVNE.D  
Calendar Year: 2030  
Month: Jan.  
Altitude: Low  
Minimum Temperature: 41.0 (F)  
Maximum Temperature: 41.0 (F)  
Absolute Humidity: 75. grains/lb  
Fuel Sulfur Content: 30. ppm

---

Exhaust I/M Program: Yes  
Evap I/M Program: Yes  
ATP Program: Yes  
Reformulated Gas: Yes

| Vehicle Type:     | LDGV   | LDGT12 | LDGT34 | LDGT | HDGV   | LDDV   | LDDT   | HDDV   | MC     |
|-------------------|--------|--------|--------|------|--------|--------|--------|--------|--------|
| All Veh           |        |        |        |      |        |        |        |        |        |
| GVWR:             | <6000  | >6000  | (All)  |      |        |        |        |        |        |
| VMT Distribution: | 0.2935 | 0.4629 | 0.1578 |      | 0.0240 | 0.0003 | 0.0024 | 0.0578 | 0.0013 |
| 1.0000            |        |        |        |      |        |        |        |        |        |

-----  
Composite Emission Factors (g/mi):

|                |       |       |       |       |      |       |       |       |       |
|----------------|-------|-------|-------|-------|------|-------|-------|-------|-------|
| Composite CO : | 11.34 | 10.22 | 10.17 | 10.21 | 5.62 | 0.511 | 0.259 | 0.198 | 12.32 |
| 9.828          |       |       |       |       |      |       |       |       |       |

-----  
\*\*\*\*\*

\* MOBILE6.2.03 (24-Sep-2003) \*

\* Input file: C:\MOBILE62\MOBILE6\RUN\FAIR30.IN (file 1, run 4). \*

\*\*\*\*\*

\*\*\*\*\* Arterial/Collector/Local Idle @ 2.5 mph (Use for queues after multiplying by 2.5)

\* Reading 94+ LEV IMPLEMENTATION SCHEDULE from the following external

\* data file: NLEVNE.D

M616 Comment:

User has supplied post-1999 sulfur levels.

M603 Comment:

User has disabled the calculation of REFUELING emissions.

\*2002 Registration Age distribution most recent data available

\* Reading Registration Distributions from the following external

\* data file: CTREG05.D

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

\* Reading I/M program description records from the following external

\* data file: CTIM05PL.D

\*CT I/M PROGRAMS for all years 2005 and later (modified Jun 05 PMB/AG to reflect DMV info that 8,501-10,000 lb get TSI & GC (no OBD)

\*Biennial OBDII I/M "tailpipe" test for post-MY1995 gasoline vehicles up to 8,500 lbs GVWR. Program start year reflects OBD test that replaced the ASM

\*Biennial OBDII evaporative "test" for post-MY1995 gasoline vehicles up to 8,500 lbs GVWR

\*Biennial 2500/IDLE I/M tailpipe test for all HDGT 8,501 - 10,000 lbs GVWR (per above comment)

\*Biennial GC evaporative "test" for all HDGT 8,501 - 10,000 lbs (per above comment)

\*Biennial ASM I/M tailpipe test for pre-96 gasoline vehicles up to 8,500 lbs GVWR

\* Reading ASM I/M Test Credits from ASMDATA.D

\*Biennial Gas Cap evaporative test for pre-96 gasoline vehicles up to 8,500 lbs GVWR

---

\* Reading Hourly VMT distribution from the following external  
 \* data file: CTHVMT09.DEF

\* Reading Hourly, Roadway, and Speed VMT dist. from the following external  
 \* data file: 30SVMT1W.CTY

\* Reading Hourly Roadway VMT distribution from the following external  
 \* data file: FCVMTL.CTY

Reading User Supplied ROADWAY VMT Factors  
 M615 Comment:  
 User supplied VMT mix.

\* #####  
 \* 2030 winter intersection: Idle @ 2.5 mph (x 2.5 to get idle rate for CAL3QHC)  
 \* File 1, Run 4, Scenario 1.  
 \* #####

M583 Warning:  
 The user supplied arterial average speed of 2.5  
 will be used for all hours of the day. 100% of VMT  
 has been assigned to the arterial/collector roadway  
 type for all hours of the day and all vehicle types.

M112 Warning:  
 Wintertime Reformulated Gasoline Rules Apply

\*\*\* I/M credits for Tech1&2 vehicles were read from the following external  
 data file: TECH12.D

M 48 Warning:  
 there are no sales for vehicle class HDGV8b

M 48 Warning:  
 there are no sales for vehicle class LDDT12

LEV phase-in data read from file NLEVNE.D

Calendar Year: 2030  
 Month: Jan.  
 Altitude: Low  
 Minimum Temperature: 41.0 (F)  
 Maximum Temperature: 41.0 (F)  
 Absolute Humidity: 75. grains/lb  
 Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: Yes  
 Evap I/M Program: Yes  
 ATP Program: Yes  
 Reformulated Gas: Yes

| Vehicle Type:                      | LDGV   | LDGT12 | LDGT34 | LDGT  | HDGV   | LDDV   | LDDT   | HDDV   | MC     |
|------------------------------------|--------|--------|--------|-------|--------|--------|--------|--------|--------|
| All Veh                            |        |        |        |       |        |        |        |        |        |
| GVWR:                              | <6000  | >6000  | (All)  |       |        |        |        |        |        |
| VMT Distribution:                  | 0.3084 | 0.4861 | 0.1657 |       | 0.0081 | 0.0003 | 0.0025 | 0.0193 | 0.0096 |
| 1.0000                             |        |        |        |       |        |        |        |        |        |
| -----                              |        |        |        |       |        |        |        |        |        |
| Composite Emission Factors (g/mi): |        |        |        |       |        |        |        |        |        |
| Composite CO :                     | 18.22  | 17.12  | 17.57  | 17.23 | 35.26  | 1.870  | 1.054  | 1.128  | 100.86 |
| 18.132                             |        |        |        |       |        |        |        |        |        |
| -----                              |        |        |        |       |        |        |        |        |        |

## 2030 Run – Litchfield County

\*\*\*\*\*

\* MOBILE6.2.03 (24-Sep-2003) \*  
\* Input file: C:\MOBILE62\MOBILE6\RUN\LITCH30.IN (file 1, run 1). \*  
\*\*\*\*\*

\* 2030 Generic Run for Intersection Analysis in Litchfield County, CT  
\* April, 2011

\*  
\*\*\*\*\*  
\* Note that the composite emission factors produced with this input file include both start  
\* and running emissions. EPA Guidance indicates that start emissions are typically negligible  
\* at intersections; therefore, use of composite emission factors will produce CO impacts that  
\* are conservatively high. If modeled impacts (including background CO) approach or exceed the  
\* CO NAAQS, consult CTDEP to discuss applying a more refined method that excludes start emissions.  
\*\*\*\*\*  
\*

\*\*\*\*\* Expressway Freeflow (USE FOR FREEWAYS ONLY, NOT RAMPS)

\* Reading 94+ LEV IMPLEMENTATION SCHEDULE from the following external  
\* data file: NLEVNE.D  
M616 Comment:  
User has supplied post-1999 sulfur levels.  
M603 Comment:  
User has disabled the calculation of REFUELING emissions.

\*2002 Registration Age distribution most recent data available

\* Reading Registration Distributions from the following external  
\* data file: CTREG05.D  
M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)  
M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)  
M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)  
M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)  
M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)  
M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)  
M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)  
M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)

\* Reading I/M program description records from the following external  
\* data file: CTIM05PL.D  
\*CT I/M PROGRAMS for all years 2005 and later (modified Jun 05 PMB/AG to reflect DMV info that 8,501-  
10,000 lb get TSI & GC (no OBD)  
\*Biennial OBDII I/M "tailpipe" test for post-MY1995 gasoline vehicles up to 8,500 lbs GVWR. Program start  
year reflects OBD test that replaced the ASM  
\*Biennial OBDII evaporative "test" for post-MY1995 gasoline vehicles up to 8,500 lbs GVWR  
\*Biennial 2500/IDLE I/M tailpipe test for all HDGT 8,501 - 10,000 lbs GVWR (per above comment)  
\*Biennial GC evaporative "test" for all HDGT 8,501 - 10,000 lbs (per above comment)  
\*Biennial ASM I/M tailpipe test for pre-96 gasoline vehicles up to 8,500 lbs GVWR

\* Reading ASM I/M Test Credits from ASMDATA.D  
\*Biennial Gas Cap evaporative test for pre-96 gasoline vehicles up to 8,500 lbs GVWR

\* Reading Hourly VMT distribution from the following external  
\* data file: CTHVMT09.DEF

---

\* Reading Hourly, Roadway, and Speed VMT dist. from the following external  
\* data file: 30SVMT3W.CTY

\* Reading Hourly Roadway VMT distribution from the following external  
\* data file: FCVMTF.CTY

Reading User Supplied ROADWAY VMT Factors  
M615 Comment:  
User supplied VMT mix.

\* #####  
\* 2030 winter intersection: Freeway Freeflow @ 55 mph (REPLACE ?? WITH SPEED)  
\* File 1, Run 1, Scenario 1.  
\* #####

M581 Warning:  
The user supplied freeway average speed of 55.0  
will be used for all hours of the day. 100% of VMT  
has been assigned to the freeway roadway type for  
all hours of the day and all vehicle types.

M112 Warning:  
Wintertime Reformulated Gasoline Rules Apply

\*\*\* I/M credits for Tech1&2 vehicles were read from the following external  
data file: TECH12.D

M 48 Warning:  
there are no sales for vehicle class HDGV8b

M 48 Warning:  
there are no sales for vehicle class LDDT12

LEV phase-in data read from file NLEVNE.D  
Calendar Year: 2030

Month: Jan.  
Altitude: Low  
Minimum Temperature: 41.0 (F)  
Maximum Temperature: 41.0 (F)  
Absolute Humidity: 75. grains/lb  
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: Yes  
Evap I/M Program: Yes  
ATP Program: Yes  
Reformulated Gas: Yes

| Vehicle Type:     | LDGV   | LDGT12 | LDGT34 | LDGT | HDGV   | LDDV   | LDDT   | HDDV   | MC     |
|-------------------|--------|--------|--------|------|--------|--------|--------|--------|--------|
| All Veh           |        |        |        |      |        |        |        |        |        |
| GVWR:             | <6000  | >6000  | (All)  |      |        |        |        |        |        |
| VMT Distribution: | 0.2935 | 0.4629 | 0.1578 |      | 0.0240 | 0.0003 | 0.0024 | 0.0578 | 0.0013 |

-----

| Composite Emission Factors (g/mi): |       |      |      |      |      |       |       |       |       |
|------------------------------------|-------|------|------|------|------|-------|-------|-------|-------|
| Composite CO :                     | 10.06 | 9.13 | 9.08 | 9.12 | 5.68 | 0.475 | 0.238 | 0.173 | 10.45 |

8.774

-----

\*\*\*\*\*  
\* MOBILE6.2.03 (24-Sep-2003) \*  
\* Input file: C:\MOBILE62\MOBILE6\RUN\LITCH30.IN (file 1, run 2). \*  
\*\*\*\*\*  
\*\*\*\*\* Arterial/Collector/Local Freeflow (DO NOT USE FOR RAMPS)

\* Reading 94+ LEV IMPLEMENTATION SCHEDULE from the following external



M112 Warning:

Wintertime Reformulated Gasoline Rules Apply

\*\*\* I/M credits for Tech1&2 vehicles were read from the following external data file: TECH12.D

M 48 Warning:

there are no sales for vehicle class HDGV8b

M 48 Warning:

there are no sales for vehicle class LDDT12

LEV phase-in data read from file NLEVNE.D

Calendar Year: 2030

Month: Jan.

Altitude: Low

Minimum Temperature: 41.0 (F)

Maximum Temperature: 41.0 (F)

Absolute Humidity: 75. grains/lb

Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: Yes

Evap I/M Program: Yes

ATP Program: Yes

Reformulated Gas: Yes

| Vehicle Type: | LDGV  | LDGT12 | LDGT34 | LDGT | HDGV | LDDV | LDDT | HDDV | MC |
|---------------|-------|--------|--------|------|------|------|------|------|----|
| All Veh       |       |        |        |      |      |      |      |      |    |
| GVWR:         | <6000 | >6000  | (All)  |      |      |      |      |      |    |

|                   |        |        |        |  |        |        |        |        |        |
|-------------------|--------|--------|--------|--|--------|--------|--------|--------|--------|
| VMT Distribution: | 0.3091 | 0.4873 | 0.1662 |  | 0.0077 | 0.0003 | 0.0025 | 0.0184 | 0.0085 |
| 1.0000            |        |        |        |  |        |        |        |        |        |

-----  
Composite Emission Factors (g/mi):

|                |      |      |      |      |      |       |       |       |       |
|----------------|------|------|------|------|------|-------|-------|-------|-------|
| Composite CO : | 9.08 | 8.05 | 7.98 | 8.03 | 7.66 | 0.621 | 0.324 | 0.274 | 15.59 |
| 8.252          |      |      |      |      |      |       |       |       |       |

-----  
\*\*\*\*\*

\* MOBILE6.2.03 (24-Sep-2003) \*

\* Input file: C:\MOBILE62\MOBILE6\RUN\LITCH30.IN (file 1, run 3). \*

\*\*\*\*\*

\*\*\*\*\* Ramp Freeflow (Use for all freeway ramps; MOBILE6 assumes avg freeflow ramp speed=34.6mph)

\* Reading 94+ LEV IMPLEMENTATION SCHEDULE from the following external

\* data file: NLEVNE.D

M616 Comment:

User has supplied post-1999 sulfur levels.

M603 Comment:

User has disabled the calculation of REFUELING emissions.

\*2002 Registration Age distribution most recent data available

\* Reading Registration Distributions from the following external

\* data file: CTREG05.D

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

M 49 Warning:





1.00 MYR sum not = 1. (will normalize)  
M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)  
M 49 Warning:  
1.00 MYR sum not = 1. (will normalize)

- \* Reading I/M program description records from the following external
- \* data file: CTIM05PL.D
- \*CT I/M PROGRAMS for all years 2005 and later (modified Jun 05 PMB/AG to reflect DMV info that 8,501-10,000 lb get TSI & GC (no OBD)
- \*Biennial OBDII I/M "tailpipe" test for post-MY1995 gasoline vehicles up to 8,500 lbs GVWR. Program start year reflects OBD test that replaced the ASM
- \*Biennial OBDII evaporative "test" for post-MY1995 gasoline vehicles up to 8,500 lbs GVWR
- \*Biennial 2500/IDLE I/M tailpipe test for all HDGT 8,501 - 10,000 lbs GVWR (per above comment)
- \*Biennial GC evaporative "test" for all HDGT 8,501 - 10,000 lbs (per above comment)
- \*Biennial ASM I/M tailpipe test for pre-96 gasoline vehicles up to 8,500 lbs GVWR

- \* Reading ASM I/M Test Credits from ASMDATA.D
- \*Biennial Gas Cap evaporative test for pre-96 gasoline vehicles up to 8,500 lbs GVWR

- \* Reading Hourly Roadway VMT distribution from the following external
- \* data file: FCMVTR.CTY

Reading User Supplied ROADWAY VMT Factors

- \* Reading Hourly VMT distribution from the following external
- \* data file: CTHVMT09.DEF

- \* Reading Hourly, Roadway, and Speed VMT dist. from the following external
- \* data file: 30SVMT3W.CTY

- \* Reading Hourly Roadway VMT distribution from the following external
- \* data file: FCMVTR.CTY

Reading User Supplied ROADWAY VMT Factors

M615 Comment:  
User supplied VMT mix.

- \* #####
- \* 2030 winter intersection: M6 assumes Ramp @ 34.6mph
- \* File 1, Run 3, Scenario 1.
- \* #####

M112 Warning:  
Wintertime Reformulated Gasoline Rules Apply

- \*\*\* I/M credits for Tech1&2 vehicles were read from the following external
- data file: TECH12.D

M 48 Warning:  
there are no sales for vehicle class HDGV8b

M 48 Warning:  
there are no sales for vehicle class LDDT12

LEV phase-in data read from file NLEVNE.D

Calendar Year: 2030

Month: Jan.

Altitude: Low

Minimum Temperature: 41.0 (F)

Maximum Temperature: 41.0 (F)

Absolute Humidity: 75. grains/lb

Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: Yes

---

Evap I/M Program: Yes  
ATP Program: Yes  
Reformulated Gas: Yes

| Vehicle Type:     | LDGV   | LDGT12 | LDGT34 | LDGT | HDGV   | LDDV   | LDDT   | HDDV   | MC     |
|-------------------|--------|--------|--------|------|--------|--------|--------|--------|--------|
| All Veh           |        |        |        |      |        |        |        |        |        |
| GVWR:             | <6000  | >6000  | (All)  |      |        |        |        |        |        |
| VMT Distribution: | 0.2935 | 0.4629 | 0.1578 |      | 0.0240 | 0.0003 | 0.0024 | 0.0578 | 0.0013 |
| 1.0000            |        |        |        |      |        |        |        |        |        |

-----  
Composite Emission Factors (g/mi):

|                |       |       |       |       |      |       |       |       |       |
|----------------|-------|-------|-------|-------|------|-------|-------|-------|-------|
| Composite CO : | 11.34 | 10.22 | 10.17 | 10.21 | 5.62 | 0.511 | 0.259 | 0.198 | 12.32 |
| 9.828          |       |       |       |       |      |       |       |       |       |

-----  
\*\*\*\*\*

\* MOBILE6.2.03 (24-Sep-2003) \*  
\* Input file: C:\MOBILE62\MOBILE6\RUN\LITCH30.IN (file 1, run 4). \*  
\*\*\*\*\*

\*\*\*\*\* Arterial/Collector/Local Idle @ 2.5 mph (Use for queues after multiplying by 2.5)

\* Reading 94+ LEV IMPLEMENTATION SCHEDULE from the following external  
\* data file: NLEVNE.D  
M616 Comment:  
User has supplied post-1999 sulfur levels.  
M603 Comment:  
User has disabled the calculation of REFUELING emissions.

\*2002 Registration Age distribution most recent data available

\* Reading Registration Distributions from the following external

\* data file: CTREG05.D

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

M 49 Warning:

1.00 MYR sum not = 1. (will normalize)

\* Reading I/M program description records from the following external

\* data file: CTIM05PL.D

\*CT I/M PROGRAMS for all years 2005 and later (modified Jun 05 PMB/AG to reflect DMV info that 8,501-10,000 lb get TSI & GC (no OBD)

\*Biennial OBDII I/M "tailpipe" test for post-MY1995 gasoline vehicles up to 8,500 lbs GVWR. Program start year reflects OBD test that replaced the ASM

\*Biennial OBDII evaporative "test" for post-MY1995 gasoline vehicles up to 8,500 lbs GVWR

\*Biennial 2500/IDLE I/M tailpipe test for all HDGT 8,501 - 10,000 lbs GVWR (per above comment)

\*Biennial GC evaporative "test" for all HDGT 8,501 - 10,000 lbs (per above comment)

\*Biennial ASM I/M tailpipe test for pre-96 gasoline vehicles up to 8,500 lbs GVWR

\* Reading ASM I/M Test Credits from ASMDATA.D

\*Biennial Gas Cap evaporative test for pre-96 gasoline vehicles up to 8,500 lbs GVWR

---

\* Reading Hourly VMT distribution from the following external  
\* data file: CTHVMT09.DEF

\* Reading Hourly, Roadway, and Speed VMT dist. from the following external  
\* data file: 30SVMT3W.CTY

\* Reading Hourly Roadway VMT distribution from the following external  
\* data file: FCVMTL.CTY

Reading User Supplied ROADWAY VMT Factors  
M615 Comment:  
User supplied VMT mix.

\* #####  
\* 2030 winter intersection: Idle @ 2.5 mph (x 2.5 to get idle rate for CAL3QHC)  
\* File 1, Run 4, Scenario 1.

\* #####  
M583 Warning:  
The user supplied arterial average speed of 2.5  
will be used for all hours of the day. 100% of VMT  
has been assigned to the arterial/collector roadway  
type for all hours of the day and all vehicle types.

M112 Warning:  
Wintertime Reformulated Gasoline Rules Apply  
\*\*\* I/M credits for Tech1&2 vehicles were read from the following external  
data file: TECH12.D

M 48 Warning:  
there are no sales for vehicle class HDGV8b

M 48 Warning:  
there are no sales for vehicle class LDDT12

LEV phase-in data read from file NLEVNE.D  
Calendar Year: 2030  
Month: Jan.  
Altitude: Low  
Minimum Temperature: 41.0 (F)  
Maximum Temperature: 41.0 (F)  
Absolute Humidity: 75. grains/lb  
Fuel Sulfur Content: 30. ppm

Exhaust I/M Program: Yes  
Evap I/M Program: Yes  
ATP Program: Yes  
Reformulated Gas: Yes

| Vehicle Type:                      | LDGV   | LDGT12 | LDGT34 | LDGT  | HDGV   | LDDV   | LDDT   | HDDV   | MC     |
|------------------------------------|--------|--------|--------|-------|--------|--------|--------|--------|--------|
| All Veh                            |        |        |        |       |        |        |        |        |        |
| GVWR:                              | <6000  | >6000  | (All)  |       |        |        |        |        |        |
| VMT Distribution:                  | 0.3084 | 0.4861 | 0.1657 |       | 0.0081 | 0.0003 | 0.0025 | 0.0193 | 0.0096 |
| 1.0000                             |        |        |        |       |        |        |        |        |        |
| -----                              |        |        |        |       |        |        |        |        |        |
| Composite Emission Factors (g/mi): |        |        |        |       |        |        |        |        |        |
| Composite CO :                     | 18.22  | 17.12  | 17.57  | 17.23 | 35.26  | 1.870  | 1.054  | 1.128  | 100.86 |
| 18.132                             |        |        |        |       |        |        |        |        |        |
| -----                              |        |        |        |       |        |        |        |        |        |

## **APPENDIX B**

### **CALQVIEW2 Model Output**

## Appendix B - CALQVIEW2 Model Output Results

This appendix contains the CALQVIEW2 model results for the following intersections:

- Federal Road (Route 202) / Station Road (Route 25) 2010 Existing AM
  - Federal Road (Route 202) / Station Road (Route 25) 2010 Existing PM
  - Federal Road (Route 202) / Station Road (Route 25) 2030 No Build AM
  - Federal Road (Route 202) / Station Road (Route 25) 2030 No Build PM
  - Federal Road (Route 202) / Station Road (Route 25) 2030 Build AM
  - Federal Road (Route 202) / Station Road (Route 25) 2030 Build PM
  - Federal Road (Route 202) / Station Road (Route 25) 2030 Mitigated Build AM
  - Federal Road (Route 202) / Station Road (Route 25) 2030 Mitigated Build PM
  
  - Grist Mill Road (Route 7) / Glover Avenue 2010 Existing AM
  - Grist Mill Road (Route 7) / Glover Avenue 2010 Existing PM
  - Grist Mill Road (Route 7) / Glover Avenue 2030 No Build AM
  - Grist Mill Road (Route 7) / Glover Avenue 2030 No Build PM
  - Grist Mill Road (Route 7) / Glover Avenue 2030 Build AM
  - Grist Mill Road (Route 7) / Glover Avenue 2030 Build PM
  - Grist Mill Road (Route 7) / Glover Avenue 2030 Mitigated Build AM
  - Grist Mill Road (Route 7) / Glover Avenue 2030 Mitigated Build PM
  
  - Route 7 / Bridge Street (Route 202) 2010 Existing AM
  - Route 7 / Bridge Street (Route 202) 2010 Existing PM
  - Route 7 / Bridge Street (Route 202) 2030 No Build AM
  - Route 7 / Bridge Street (Route 202) 2030 No Build PM
  - Route 7 / Bridge Street (Route 202) 2030 Build AM
  - Route 7 / Bridge Street (Route 202) 2030 Build PM
  - Route 7 / Bridge Street (Route 202) 2030 Mitigated Build AM
  - Route 7 / Bridge Street (Route 202) 2030 Mitigated Build PM
  
  - Grist Mill Road (Route 7) / Main Avenue 2010 Existing AM
  - Grist Mill Road (Route 7) / Main Avenue 2010 Existing PM
  - Grist Mill Road (Route 7) / Main Avenue 2030 No Build AM
  - Grist Mill Road (Route 7) / Main Avenue 2030 No Build PM
  - Grist Mill Road (Route 7) / Main Avenue 2030 Build AM
  - Grist Mill Road (Route 7) / Main Avenue 2030 Build PM
  - Grist Mill Road (Route 7) / Main Avenue 2030 Mitigated Build AM
  - Grist Mill Road (Route 7) / Main Avenue 2030 Mitigated Build PM
-

JOB: FederalStation2010ExistingAM

RUN: FederalStation2010ExistingAM

DATE : 4/ 7/11  
 TIME : 14:57:40

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S      VD = .0 CM/S      Z0 = 175. CM  
 U = 1.0 M/S      CLAS = 4 (D)      ATIM = 60. MINUTES      MIXH = 1000. M      AMB = 4.3 PPM

LINK VARIABLES

| LINK DESCRIPTION     | * X1 | LINK COORDINATES (FT)<br>Y1 | X2    | Y2    | * LENGTH (FT) | BRG TYPE (DEG) | VPH     | EF (G/MI) | H (FT) | W (FT)  | V/C | QUEUE (VEH) |
|----------------------|------|-----------------------------|-------|-------|---------------|----------------|---------|-----------|--------|---------|-----|-------------|
| 1. Station EB in     | *    | .0                          | 418.0 | 200.0 | 418.0         | * 200.         | 90. AG  | 101.      | 11.2   | .0 24.0 |     |             |
| 2. Station EB L      | *    | 200.0                       | 424.0 | 204.5 | 424.0         | * 4.           | 90. AG  | 303.      | 100.0  | .0 12.0 | .04 | .2          |
| 3. Station EB TR     | *    | 200.0                       | 412.0 | 217.1 | 412.0         | * 17.          | 90. AG  | 303.      | 100.0  | .0 12.0 | .17 | .9          |
| 4. Whisconier EB out | *    | 454.0                       | 418.0 | 848.0 | 418.0         | * 394.         | 90. AG  | 101.      | 11.2   | .0 24.0 |     |             |
| 5. Whisconier WB in  | *    | 848.0                       | 442.0 | 648.0 | 442.0         | * 200.         | 270. AG | 494.      | 11.2   | .0 24.0 |     |             |
| 6. Whisconier WB LT  | *    | 648.0                       | 436.0 | 594.9 | 436.0         | * 53.          | 270. AG | 241.      | 100.0  | .0 12.0 | .61 | 2.7         |
| 7. Whisconier WB R   | *    | 648.0                       | 448.0 | 623.3 | 448.0         | * 25.          | 270. AG | 194.      | 100.0  | .0 12.0 | .25 | 1.3         |
| 8. Station WB out    | *    | 406.0                       | 442.0 | .0    | 442.0         | * 406.         | 270. AG | 494.      | 11.2   | .0 24.0 |     |             |
| 9. Federal NB in     | *    | 442.0                       | .0    | 442.0 | 200.0         | * 200.         | 360. AG | 184.      | 11.2   | .0 12.0 |     |             |
| 10. Federal NB LTR   | *    | 442.0                       | 200.0 | 442.0 | 231.2         | * 31.          | 360. AG | 241.      | 100.0  | .0 12.0 | .28 | 1.6         |
| 11. Federal NB out   | *    | 442.0                       | 454.0 | 442.0 | 836.0         | * 382.         | 360. AG | 184.      | 11.2   | .0 24.0 |     |             |
| 12. Federal SB in    | *    | 418.0                       | 836.0 | 418.0 | 636.0         | * 200.         | 180. AG | 215.      | 11.2   | .0 24.0 |     |             |
| 13. Federal SB L     | *    | 424.0                       | 636.0 | 424.0 | 621.4         | * 15.          | 180. AG | 241.      | 100.0  | .0 12.0 | .15 | .7          |
| 14. Federal SB TR    | *    | 412.0                       | 636.0 | 412.0 | 615.5         | * 20.          | 180. AG | 225.      | 100.0  | .0 12.0 | .18 | 1.0         |
| 15. Federal SB out   | *    | 424.0                       | 404.0 | 424.0 | .0            | * 404.         | 180. AG | 215.      | 11.2   | .0 24.0 |     |             |

DATE : 4/ 7/11  
 TIME : 14:57:40

-----  
 ADDITIONAL QUEUE LINK PARAMETERS  
 -----

| LINK DESCRIPTION    | *<br>* | CYCLE<br>LENGTH<br>(SEC) | RED<br>TIME<br>(SEC) | CLEARANCE<br>LOST TIME<br>(SEC) | APPROACH<br>VOL<br>(VPH) | SATURATION<br>FLOW RATE<br>(VPH) | IDLE<br>EM FAC<br>(gm/hr) | SIGNAL<br>TYPE | ARRIVAL<br>RATE |
|---------------------|--------|--------------------------|----------------------|---------------------------------|--------------------------|----------------------------------|---------------------------|----------------|-----------------|
| 2. Station EB L     | *      | 60                       | 39                   | 4.0                             | 21                       | 1926                             | 173.64                    | 3              | 3               |
| 3. Station EB TR    | *      | 60                       | 39                   | 4.0                             | 80                       | 1938                             | 173.64                    | 3              | 3               |
| 6. Whisconier WB LT | *      | 60                       | 31                   | 4.0                             | 313                      | 1337                             | 173.64                    | 3              | 3               |
| 7. Whisconier WB R  | *      | 60                       | 25                   | 4.0                             | 181                      | 1515                             | 173.64                    | 3              | 3               |
| 10. Federal NB LTR  | *      | 60                       | 31                   | 5.0                             | 184                      | 1774                             | 173.64                    | 3              | 3               |
| 13. Federal SB L    | *      | 60                       | 31                   | 3.0                             | 86                       | 1429                             | 173.64                    | 3              | 3               |
| 14. Federal SB TR   | *      | 60                       | 29                   | 5.0                             | 129                      | 1753                             | 173.64                    | 3              | 3               |

-----  
 RECEPTOR LOCATIONS  
 -----

| RECEPTOR          | *<br>* | COORDINATES (FT) |       |     | *<br>* |
|-------------------|--------|------------------|-------|-----|--------|
|                   |        | X                | Y     | Z   |        |
| 1. EB W Midblock  | *      | 196.0            | 390.0 | 6.0 | *      |
| 2. SW Corner      | *      | 394.0            | 390.0 | 6.0 | *      |
| 3. SB S Midblock  | *      | 394.0            | 200.0 | 6.0 | *      |
| 4. NB S Midblock  | *      | 464.0            | 200.0 | 6.0 | *      |
| 5. SE Corner      | *      | 464.0            | 390.0 | 6.0 | *      |
| 6. EB E Midblock  | *      | 648.0            | 390.0 | 6.0 | *      |
| 7. WB E Midblock  | *      | 648.0            | 464.0 | 6.0 | *      |
| 8. NE Corner      | *      | 464.0            | 464.0 | 6.0 | *      |
| 9. NB N Midblock  | *      | 464.0            | 640.0 | 6.0 | *      |
| 10. SB N Midblock | *      | 396.0            | 640.0 | 6.0 | *      |
| 11. NW Corner     | *      | 396.0            | 464.0 | 6.0 | *      |
| 12. WB W Midblock | *      | 196.0            | 464.0 | 6.0 | *      |

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

| WIND ANGLE (DEGR) | REC1 | REC2 | REC3 | REC4 | REC5 | REC6 | REC7 | REC8 | REC9 | REC10 | REC11 | REC12 |
|-------------------|------|------|------|------|------|------|------|------|------|-------|-------|-------|
| 0.                | 4.7  | 4.4  | 4.3  | 4.3  | 4.3  | 4.6  | 4.3  | 4.4  | 4.3  | 4.3   | 4.3   | 4.3   |
| 10.               | 4.8  | 4.4  | 4.4  | 4.3  | 4.3  | 4.6  | 4.3  | 4.3  | 4.3  | 4.4   | 4.3   | 4.3   |
| 20.               | 4.9  | 4.3  | 4.4  | 4.3  | 4.3  | 4.4  | 4.3  | 4.3  | 4.3  | 4.4   | 4.3   | 4.3   |
| 30.               | 4.8  | 4.3  | 4.4  | 4.3  | 4.3  | 4.4  | 4.3  | 4.3  | 4.3  | 4.4   | 4.3   | 4.3   |
| 40.               | 4.8  | 4.3  | 4.5  | 4.3  | 4.3  | 4.4  | 4.3  | 4.3  | 4.3  | 4.4   | 4.3   | 4.3   |
| 50.               | 4.7  | 4.3  | 4.5  | 4.3  | 4.3  | 4.4  | 4.3  | 4.3  | 4.3  | 4.4   | 4.3   | 4.3   |
| 60.               | 4.6  | 4.3  | 4.6  | 4.3  | 4.4  | 4.4  | 4.3  | 4.3  | 4.3  | 4.4   | 4.3   | 4.3   |
| 70.               | 4.5  | 4.3  | 4.6  | 4.3  | 4.4  | 4.4  | 4.3  | 4.3  | 4.3  | 4.4   | 4.3   | 4.3   |
| 80.               | 4.4  | 4.4  | 4.6  | 4.3  | 4.4  | 4.4  | 4.4  | 4.3  | 4.3  | 4.6   | 4.3   | 4.4   |
| 90.               | 4.3  | 4.4  | 4.6  | 4.3  | 4.3  | 4.3  | 4.4  | 4.4  | 4.3  | 4.5   | 4.3   | 4.4   |
| 100.              | 4.3  | 4.4  | 4.5  | 4.3  | 4.3  | 4.3  | 4.5  | 4.4  | 4.3  | 4.7   | 4.4   | 4.5   |
| 110.              | 4.3  | 4.4  | 4.4  | 4.3  | 4.3  | 4.3  | 4.5  | 4.4  | 4.3  | 4.9   | 4.3   | 4.5   |
| 120.              | 4.3  | 4.4  | 4.4  | 4.3  | 4.3  | 4.3  | 4.5  | 4.3  | 4.3  | 4.9   | 4.3   | 4.5   |
| 130.              | 4.3  | 4.4  | 4.4  | 4.3  | 4.3  | 4.3  | 4.5  | 4.3  | 4.3  | 5.0   | 4.3   | 4.5   |
| 140.              | 4.3  | 4.4  | 4.4  | 4.3  | 4.3  | 4.3  | 4.5  | 4.3  | 4.3  | 4.8   | 4.3   | 4.6   |
| 150.              | 4.3  | 4.4  | 4.4  | 4.3  | 4.3  | 4.3  | 4.5  | 4.3  | 4.3  | 4.6   | 4.4   | 4.6   |
| 160.              | 4.3  | 4.4  | 4.4  | 4.3  | 4.3  | 4.3  | 4.6  | 4.3  | 4.3  | 4.5   | 4.4   | 4.8   |
| 170.              | 4.3  | 4.4  | 4.4  | 4.3  | 4.3  | 4.3  | 4.7  | 4.3  | 4.3  | 4.4   | 4.5   | 4.8   |
| 180.              | 4.3  | 4.3  | 4.3  | 4.3  | 4.3  | 4.3  | 4.9  | 4.3  | 4.3  | 4.3   | 4.4   | 4.7   |
| 190.              | 4.3  | 4.3  | 4.3  | 4.3  | 4.4  | 4.3  | 4.9  | 4.4  | 4.4  | 4.3   | 4.5   | 4.6   |
| 200.              | 4.3  | 4.3  | 4.3  | 4.5  | 4.4  | 4.3  | 5.1  | 4.3  | 4.4  | 4.3   | 4.5   | 4.5   |
| 210.              | 4.3  | 4.3  | 4.3  | 4.5  | 4.4  | 4.3  | 5.2  | 4.3  | 4.4  | 4.3   | 4.5   | 4.5   |
| 220.              | 4.3  | 4.3  | 4.3  | 4.5  | 4.4  | 4.3  | 5.3  | 4.3  | 4.4  | 4.3   | 4.5   | 4.5   |
| 230.              | 4.3  | 4.3  | 4.3  | 4.4  | 4.4  | 4.3  | 5.1  | 4.3  | 4.6  | 4.3   | 4.5   | 4.5   |
| 240.              | 4.3  | 4.3  | 4.3  | 4.4  | 4.4  | 4.3  | 4.9  | 4.4  | 4.6  | 4.3   | 4.5   | 4.5   |
| 250.              | 4.3  | 4.3  | 4.3  | 4.4  | 4.3  | 4.3  | 4.7  | 4.4  | 4.7  | 4.3   | 4.5   | 4.5   |
| 260.              | 4.3  | 4.3  | 4.3  | 4.5  | 4.3  | 4.3  | 4.5  | 4.4  | 4.7  | 4.3   | 4.5   | 4.5   |
| 270.              | 4.3  | 4.4  | 4.3  | 4.6  | 4.4  | 4.3  | 4.3  | 4.5  | 4.6  | 4.3   | 4.4   | 4.4   |
| 280.              | 4.4  | 4.4  | 4.3  | 4.7  | 4.4  | 4.3  | 4.3  | 4.5  | 4.6  | 4.3   | 4.4   | 4.4   |
| 290.              | 4.4  | 4.4  | 4.3  | 4.8  | 4.4  | 4.3  | 4.3  | 4.4  | 4.4  | 4.3   | 4.3   | 4.3   |
| 300.              | 4.4  | 4.4  | 4.3  | 4.9  | 4.4  | 4.4  | 4.3  | 4.4  | 4.4  | 4.3   | 4.3   | 4.3   |
| 310.              | 4.4  | 4.4  | 4.3  | 4.9  | 4.4  | 4.5  | 4.3  | 4.4  | 4.4  | 4.3   | 4.3   | 4.3   |
| 320.              | 4.4  | 4.4  | 4.3  | 4.8  | 4.3  | 4.6  | 4.3  | 4.4  | 4.5  | 4.3   | 4.3   | 4.3   |
| 330.              | 4.4  | 4.4  | 4.3  | 4.7  | 4.3  | 4.7  | 4.3  | 4.4  | 4.5  | 4.3   | 4.3   | 4.3   |
| 340.              | 4.4  | 4.4  | 4.3  | 4.5  | 4.3  | 4.7  | 4.3  | 4.4  | 4.4  | 4.3   | 4.3   | 4.3   |
| 350.              | 4.5  | 4.4  | 4.3  | 4.4  | 4.3  | 4.6  | 4.3  | 4.4  | 4.4  | 4.3   | 4.3   | 4.3   |
| 360.              | 4.7  | 4.4  | 4.3  | 4.3  | 4.3  | 4.6  | 4.3  | 4.4  | 4.3  | 4.3   | 4.3   | 4.3   |
| MAX DEGR.         | 4.9  | 4.4  | 4.6  | 4.9  | 4.4  | 4.7  | 5.3  | 4.5  | 4.7  | 5.0   | 4.5   | 4.8   |
|                   | 20   | 0    | 60   | 300  | 60   | 330  | 220  | 270  | 250  | 130   | 170   | 160   |

THE HIGHEST CONCENTRATION OF 5.30 PPM OCCURRED AT RECEPTOR REC7 .





JOB: FederalStation2010ExistingPM

RUN: FederalStation2010ExistingPM

DATE : 4/ 7/11  
 TIME : 15: 4:35

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S      VD = .0 CM/S      Z0 = 175. CM  
 U = 1.0 M/S      CLAS = 4 (D)      ATIM = 60. MINUTES      MIXH = 1000. M      AMB = 4.3 PPM

LINK VARIABLES

| LINK DESCRIPTION     | *<br>* X1 | LINK COORDINATES (FT)<br>Y1 | X2    | Y2    | *<br>* LENGTH (FT) | BRG TYPE (DEG) | VPH  | EF (G/MI) | H (FT) | W (FT) | V/C | QUEUE (VEH) |
|----------------------|-----------|-----------------------------|-------|-------|--------------------|----------------|------|-----------|--------|--------|-----|-------------|
| 1. Station EB in     | * .0      | 418.0                       | 200.0 | 418.0 | * 200.             | 90. AG         | 92.  | 11.2      | .0     | 24.0   |     |             |
| 2. Station EB L      | * 200.0   | 424.0                       | 202.8 | 424.0 | * 3.               | 90. AG         | 326. | 100.0     | .0     | 12.0   | .04 | .1          |
| 3. Station EB TR     | * 200.0   | 412.0                       | 218.4 | 412.0 | * 18.              | 90. AG         | 326. | 100.0     | .0     | 12.0   | .23 | .9          |
| 4. Whisconier EB out | * 454.0   | 418.0                       | 848.0 | 418.0 | * 394.             | 90. AG         | 92.  | 11.2      | .0     | 24.0   |     |             |
| 5. Whisconier WB in  | * 848.0   | 442.0                       | 648.0 | 442.0 | * 200.             | 270. AG        | 402. | 11.2      | .0     | 24.0   |     |             |
| 6. Whisconier WB LT  | * 648.0   | 436.0                       | 599.8 | 436.0 | * 48.              | 270. AG        | 272. | 100.0     | .0     | 12.0   | .56 | 2.5         |
| 7. Whisconier WB R   | * 648.0   | 448.0                       | 628.3 | 448.0 | * 20.              | 270. AG        | 186. | 100.0     | .0     | 12.0   | .20 | 1.0         |
| 8. Station WB out    | * 406.0   | 442.0                       | .0    | 442.0 | * 406.             | 270. AG        | 402. | 11.2      | .0     | 24.0   |     |             |
| 9. Federal NB in     | * 442.0   | .0                          | 442.0 | 200.0 | * 200.             | 360. AG        | 436. | 11.2      | .0     | 12.0   |     |             |
| 10. Federal NB LTR   | * 442.0   | 200.0                       | 442.0 | 276.3 | * 76.              | 360. AG        | 248. | 100.0     | .0     | 12.0   | .68 | 3.9         |
| 11. Federal NB out   | * 442.0   | 454.0                       | 442.0 | 836.0 | * 382.             | 360. AG        | 436. | 11.2      | .0     | 24.0   |     |             |
| 12. Federal SB in    | * 418.0   | 836.0                       | 418.0 | 636.0 | * 200.             | 180. AG        | 321. | 11.2      | .0     | 24.0   |     |             |
| 13. Federal SB L     | * 424.0   | 636.0                       | 424.0 | 612.8 | * 23.              | 180. AG        | 210. | 100.0     | .0     | 12.0   | .20 | 1.2         |
| 14. Federal SB TR    | * 412.0   | 636.0                       | 412.0 | 613.6 | * 22.              | 180. AG        | 194. | 100.0     | .0     | 12.0   | .20 | 1.1         |
| 15. Federal SB out   | * 424.0   | 404.0                       | 424.0 | .0    | * 404.             | 180. AG        | 321. | 11.2      | .0     | 24.0   |     |             |

DATE : 4/ 7/11  
 TIME : 15: 4:35

-----  
 ADDITIONAL QUEUE LINK PARAMETERS  
 -----

| LINK DESCRIPTION    | *<br>* | CYCLE<br>LENGTH<br>(SEC) | RED<br>TIME<br>(SEC) | CLEARANCE<br>LOST TIME<br>(SEC) | APPROACH<br>VOL<br>(VPH) | SATURATION<br>FLOW RATE<br>(VPH) | IDLE<br>EM FAC<br>(gm/hr) | SIGNAL<br>TYPE | ARRIVAL<br>RATE |
|---------------------|--------|--------------------------|----------------------|---------------------------------|--------------------------|----------------------------------|---------------------------|----------------|-----------------|
| 2. Station EB L     | *      | 60                       | 42                   | 4.0                             | 12                       | 1689                             | 173.64                    | 3              | 3               |
| 3. Station EB TR    | *      | 60                       | 42                   | 4.0                             | 80                       | 1709                             | 173.64                    | 3              | 3               |
| 6. Whisconier WB LT | *      | 60                       | 35                   | 4.0                             | 252                      | 1422                             | 173.64                    | 3              | 3               |
| 7. Whisconier WB R  | *      | 60                       | 24                   | 4.0                             | 150                      | 1515                             | 173.64                    | 3              | 3               |
| 10. Federal NB LTR  | *      | 60                       | 32                   | 5.0                             | 436                      | 1836                             | 173.64                    | 3              | 3               |
| 13. Federal SB L    | *      | 60                       | 27                   | 3.0                             | 157                      | 1662                             | 173.64                    | 3              | 3               |
| 14. Federal SB TR   | *      | 60                       | 25                   | 5.0                             | 164                      | 1725                             | 173.64                    | 3              | 3               |

-----  
 RECEPTOR LOCATIONS  
 -----

| RECEPTOR          | *<br>* | COORDINATES (FT) |       |     | *<br>* |
|-------------------|--------|------------------|-------|-----|--------|
|                   |        | X                | Y     | Z   |        |
| 1. EB W Midblock  | *      | 196.0            | 390.0 | 6.0 | *      |
| 2. SW Corner      | *      | 394.0            | 390.0 | 6.0 | *      |
| 3. SB S Midblock  | *      | 394.0            | 200.0 | 6.0 | *      |
| 4. NB S Midblock  | *      | 464.0            | 200.0 | 6.0 | *      |
| 5. SE Corner      | *      | 464.0            | 390.0 | 6.0 | *      |
| 6. EB E Midblock  | *      | 648.0            | 390.0 | 6.0 | *      |
| 7. WB E Midblock  | *      | 648.0            | 464.0 | 6.0 | *      |
| 8. NE Corner      | *      | 464.0            | 464.0 | 6.0 | *      |
| 9. NB N Midblock  | *      | 464.0            | 640.0 | 6.0 | *      |
| 10. SB N Midblock | *      | 396.0            | 640.0 | 6.0 | *      |
| 11. NW Corner     | *      | 396.0            | 464.0 | 6.0 | *      |
| 12. WB W Midblock | *      | 196.0            | 464.0 | 6.0 | *      |

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

| WIND ANGLE (DEGR) | REC1 | REC2 | REC3 | REC4 | REC5 | REC6 | REC7 | REC8 | REC9 | REC10 | REC11 | REC12 |
|-------------------|------|------|------|------|------|------|------|------|------|-------|-------|-------|
| 0.                | 4.7  | 4.5  | 4.3  | 4.4  | 4.4  | 4.6  | 4.3  | 4.4  | 4.4  | 4.4   | 4.4   | 4.3   |
| 10.               | 4.8  | 4.4  | 4.4  | 4.3  | 4.4  | 4.6  | 4.3  | 4.4  | 4.3  | 4.5   | 4.4   | 4.3   |
| 20.               | 4.9  | 4.4  | 4.5  | 4.3  | 4.3  | 4.4  | 4.3  | 4.3  | 4.3  | 4.5   | 4.4   | 4.3   |
| 30.               | 4.9  | 4.4  | 4.6  | 4.3  | 4.3  | 4.4  | 4.3  | 4.3  | 4.3  | 4.5   | 4.4   | 4.3   |
| 40.               | 4.8  | 4.3  | 4.7  | 4.3  | 4.3  | 4.4  | 4.3  | 4.3  | 4.3  | 4.5   | 4.4   | 4.3   |
| 50.               | 4.7  | 4.3  | 4.7  | 4.3  | 4.3  | 4.4  | 4.3  | 4.3  | 4.3  | 4.5   | 4.4   | 4.3   |
| 60.               | 4.6  | 4.3  | 4.7  | 4.3  | 4.4  | 4.4  | 4.3  | 4.3  | 4.3  | 4.5   | 4.4   | 4.3   |
| 70.               | 4.5  | 4.4  | 4.7  | 4.3  | 4.4  | 4.4  | 4.3  | 4.3  | 4.3  | 4.5   | 4.4   | 4.3   |
| 80.               | 4.3  | 4.5  | 4.6  | 4.3  | 4.4  | 4.3  | 4.3  | 4.3  | 4.3  | 4.7   | 4.4   | 4.3   |
| 90.               | 4.3  | 4.4  | 4.6  | 4.3  | 4.3  | 4.3  | 4.4  | 4.4  | 4.3  | 4.7   | 4.4   | 4.4   |
| 100.              | 4.3  | 4.4  | 4.5  | 4.3  | 4.3  | 4.3  | 4.4  | 4.4  | 4.3  | 4.9   | 4.5   | 4.4   |
| 110.              | 4.3  | 4.4  | 4.5  | 4.3  | 4.3  | 4.3  | 4.5  | 4.4  | 4.3  | 5.0   | 4.3   | 4.5   |
| 120.              | 4.4  | 4.4  | 4.5  | 4.3  | 4.3  | 4.3  | 4.5  | 4.3  | 4.3  | 5.1   | 4.3   | 4.5   |
| 130.              | 4.3  | 4.4  | 4.5  | 4.3  | 4.3  | 4.3  | 4.5  | 4.3  | 4.3  | 5.0   | 4.3   | 4.5   |
| 140.              | 4.3  | 4.4  | 4.5  | 4.3  | 4.3  | 4.3  | 4.4  | 4.3  | 4.3  | 5.0   | 4.3   | 4.5   |
| 150.              | 4.3  | 4.5  | 4.5  | 4.3  | 4.3  | 4.3  | 4.4  | 4.3  | 4.3  | 4.8   | 4.4   | 4.5   |
| 160.              | 4.3  | 4.5  | 4.5  | 4.3  | 4.3  | 4.3  | 4.6  | 4.3  | 4.3  | 4.6   | 4.6   | 4.6   |
| 170.              | 4.3  | 4.5  | 4.4  | 4.3  | 4.4  | 4.3  | 4.8  | 4.3  | 4.3  | 4.5   | 4.6   | 4.6   |
| 180.              | 4.3  | 4.5  | 4.3  | 4.4  | 4.4  | 4.3  | 4.9  | 4.5  | 4.4  | 4.3   | 4.6   | 4.5   |
| 190.              | 4.3  | 4.3  | 4.3  | 4.5  | 4.5  | 4.3  | 5.0  | 4.5  | 4.5  | 4.3   | 4.4   | 4.5   |
| 200.              | 4.3  | 4.3  | 4.3  | 4.5  | 4.5  | 4.3  | 5.2  | 4.4  | 4.5  | 4.3   | 4.4   | 4.4   |
| 210.              | 4.3  | 4.3  | 4.3  | 4.5  | 4.4  | 4.3  | 5.2  | 4.4  | 4.5  | 4.3   | 4.4   | 4.4   |
| 220.              | 4.3  | 4.3  | 4.3  | 4.5  | 4.4  | 4.3  | 5.2  | 4.3  | 4.6  | 4.3   | 4.4   | 4.4   |
| 230.              | 4.3  | 4.3  | 4.3  | 4.5  | 4.4  | 4.4  | 5.0  | 4.3  | 4.7  | 4.3   | 4.5   | 4.5   |
| 240.              | 4.3  | 4.3  | 4.3  | 4.5  | 4.4  | 4.4  | 4.8  | 4.4  | 4.7  | 4.3   | 4.5   | 4.5   |
| 250.              | 4.3  | 4.3  | 4.3  | 4.6  | 4.4  | 4.3  | 4.6  | 4.5  | 4.7  | 4.3   | 4.5   | 4.5   |
| 260.              | 4.3  | 4.3  | 4.3  | 4.7  | 4.4  | 4.3  | 4.4  | 4.5  | 4.7  | 4.3   | 4.5   | 4.4   |
| 270.              | 4.3  | 4.3  | 4.3  | 4.8  | 4.4  | 4.3  | 4.3  | 4.5  | 4.6  | 4.3   | 4.4   | 4.4   |
| 280.              | 4.3  | 4.4  | 4.3  | 4.8  | 4.5  | 4.3  | 4.3  | 4.5  | 4.6  | 4.3   | 4.4   | 4.3   |
| 290.              | 4.4  | 4.4  | 4.3  | 4.9  | 4.4  | 4.3  | 4.3  | 4.4  | 4.5  | 4.3   | 4.3   | 4.3   |
| 300.              | 4.4  | 4.4  | 4.3  | 4.9  | 4.4  | 4.4  | 4.3  | 4.4  | 4.5  | 4.3   | 4.3   | 4.3   |
| 310.              | 4.4  | 4.4  | 4.3  | 5.0  | 4.3  | 4.5  | 4.3  | 4.5  | 4.6  | 4.3   | 4.3   | 4.3   |
| 320.              | 4.4  | 4.4  | 4.3  | 5.0  | 4.3  | 4.6  | 4.3  | 4.5  | 4.6  | 4.3   | 4.3   | 4.3   |
| 330.              | 4.4  | 4.4  | 4.3  | 5.0  | 4.3  | 4.7  | 4.3  | 4.5  | 4.6  | 4.3   | 4.3   | 4.3   |
| 340.              | 4.4  | 4.4  | 4.3  | 4.9  | 4.4  | 4.7  | 4.3  | 4.5  | 4.6  | 4.3   | 4.3   | 4.3   |
| 350.              | 4.5  | 4.4  | 4.3  | 4.7  | 4.4  | 4.7  | 4.3  | 4.5  | 4.5  | 4.3   | 4.3   | 4.3   |
| 360.              | 4.7  | 4.5  | 4.3  | 4.4  | 4.4  | 4.6  | 4.3  | 4.4  | 4.4  | 4.4   | 4.4   | 4.3   |
| MAX               | 4.9  | 4.5  | 4.7  | 5.0  | 4.5  | 4.7  | 5.2  | 4.5  | 4.7  | 5.1   | 4.6   | 4.6   |
| DEGR.             | 20   | 0    | 40   | 310  | 190  | 330  | 200  | 180  | 230  | 120   | 160   | 160   |

THE HIGHEST CONCENTRATION OF 5.20 PPM OCCURRED AT RECEPTOR REC7 .

DATE : 4/ 7/11  
 TIME : 15: 4:35

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING  
 THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

| LINK # | * | CO/LINK (PPM) |      |      |      |      |      |      |      |      |       |       |       |
|--------|---|---------------|------|------|------|------|------|------|------|------|-------|-------|-------|
|        |   | REC1          | REC2 | REC3 | REC4 | REC5 | REC6 | REC7 | REC8 | REC9 | REC10 | REC11 | REC12 |
| *      | * | 20            | 0    | 40   | 310  | 190  | 330  | 200  | 180  | 230  | 120   | 160   | 160   |
| 1      | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 2      | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 3      | * | .5            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .2    |
| 4      | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 5      | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 6      | * | .0            | .0   | .0   | .0   | .0   | .3   | .5   | .0   | .0   | .0    | .0    | .0    |
| 7      | * | .0            | .0   | .0   | .0   | .0   | .1   | .4   | .0   | .0   | .0    | .0    | .0    |
| 8      | * | .1            | .1   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .1    | .1    |
| 9      | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 10     | * | .0            | .0   | .3   | .6   | .1   | .0   | .0   | .1   | .0   | .0    | .1    | .0    |
| 11     | * | .0            | .1   | .0   | .0   | .0   | .0   | .0   | .0   | .2   | .1    | .0    | .0    |
| 12     | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 13     | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .1   | .3    | .0    | .0    |
| 14     | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .1   | .4    | .0    | .0    |
| 15     | * | .0            | .0   | .1   | .1   | .1   | .0   | .0   | .1   | .0   | .0    | .1    | .0    |

JOB: FederalStation2030NoBuildAM

RUN: FederalStation2030NoBuildAM

DATE : 4/15/11  
 TIME : 13: 1: 2

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S      VD = .0 CM/S      Z0 = 175. CM  
 U = 1.0 M/S      CLAS = 4 (D)      ATIM = 60. MINUTES      MIXH = 1000. M      AMB = 4.3 PPM

LINK VARIABLES

| LINK DESCRIPTION     | *<br>* X1 | LINK COORDINATES (FT)<br>Y1 | X2    | Y2    | *<br>* | LENGTH<br>(FT) | BRG TYPE<br>(DEG) | VPH  | EF<br>(G/MI) | H<br>(FT) | W<br>(FT) | V/C | QUEUE<br>(VEH) |
|----------------------|-----------|-----------------------------|-------|-------|--------|----------------|-------------------|------|--------------|-----------|-----------|-----|----------------|
| 1. Station EB in     | * .0      | 418.0                       | 200.0 | 418.0 | * *    | 200.           | 90. AG            | 149. | 8.3          | .0        | 24.0      |     |                |
| 2. Station EB L      | * 200.0   | 424.0                       | 208.5 | 424.0 | * *    | 9.             | 90. AG            | 223. | 100.0        | .0        | 12.0      | .08 | .4             |
| 3. Station EB TR     | * 200.0   | 412.0                       | 223.2 | 412.0 | * *    | 23.            | 90. AG            | 223. | 100.0        | .0        | 12.0      | .23 | 1.2            |
| 4. Whisconier EB out | * 454.0   | 418.0                       | 848.0 | 418.0 | * *    | 394.           | 90. AG            | 149. | 8.3          | .0        | 24.0      |     |                |
| 5. Whisconier WB in  | * 848.0   | 442.0                       | 648.0 | 442.0 | * *    | 200.           | 270. AG           | 769. | 8.3          | .0        | 24.0      |     |                |
| 6. Whisconier WB LT  | * 648.0   | 436.0                       | 514.5 | 436.0 | * *    | 134.           | 270. AG           | 177. | 100.0        | .0        | 12.0      | .94 | 6.8            |
| 7. Whisconier WB R   | * 648.0   | 448.0                       | 601.1 | 448.0 | * *    | 47.            | 270. AG           | 143. | 100.0        | .0        | 12.0      | .47 | 2.4            |
| 8. Station WB out    | * 406.0   | 442.0                       | .0    | 442.0 | * *    | 406.           | 270. AG           | 769. | 8.3          | .0        | 24.0      |     |                |
| 9. Federal NB in     | * 442.0   | .0                          | 442.0 | 200.0 | * *    | 200.           | 360. AG           | 315. | 8.3          | .0        | 12.0      |     |                |
| 10. Federal NB LTR   | * 442.0   | 200.0                       | 442.0 | 253.4 | * *    | 53.            | 360. AG           | 177. | 100.0        | .0        | 12.0      | .48 | 2.7            |
| 11. Federal NB out   | * 442.0   | 454.0                       | 442.0 | 836.0 | * *    | 382.           | 360. AG           | 315. | 8.3          | .0        | 24.0      |     |                |
| 12. Federal SB in    | * 418.0   | 836.0                       | 418.0 | 636.0 | * *    | 200.           | 180. AG           | 454. | 8.3          | .0        | 24.0      |     |                |
| 13. Federal SB L     | * 424.0   | 636.0                       | 424.0 | 607.2 | * *    | 29.            | 180. AG           | 177. | 100.0        | .0        | 12.0      | .29 | 1.5            |
| 14. Federal SB TR    | * 412.0   | 636.0                       | 412.0 | 591.0 | * *    | 45.            | 180. AG           | 166. | 100.0        | .0        | 12.0      | .40 | 2.3            |
| 15. Federal SB out   | * 424.0   | 404.0                       | 424.0 | .0    | * *    | 404.           | 180. AG           | 454. | 8.3          | .0        | 24.0      |     |                |

DATE : 4/15/11  
 TIME : 13: 1: 2

-----  
 ADDITIONAL QUEUE LINK PARAMETERS  
 -----

| LINK DESCRIPTION    | *<br>* | CYCLE<br>LENGTH<br>(SEC) | RED<br>TIME<br>(SEC) | CLEARANCE<br>LOST TIME<br>(SEC) | APPROACH<br>VOL<br>(VPH) | SATURATION<br>FLOW RATE<br>(VPH) | IDLE<br>EM FAC<br>(gm/hr) | SIGNAL<br>TYPE | ARRIVAL<br>RATE |
|---------------------|--------|--------------------------|----------------------|---------------------------------|--------------------------|----------------------------------|---------------------------|----------------|-----------------|
| 2. Station EB L     | *<br>* | 60                       | 39                   | 4.0                             | 40                       | 1926                             | 127.94                    | 3              | 3               |
| 3. Station EB TR    | *<br>* | 60                       | 39                   | 4.0                             | 109                      | 1938                             | 127.94                    | 3              | 3               |
| 6. Whisconier WB LT | *<br>* | 60                       | 31                   | 4.0                             | 426                      | 1177                             | 127.94                    | 3              | 3               |
| 7. Whisconier WB R  | *<br>* | 60                       | 25                   | 4.0                             | 343                      | 1515                             | 127.94                    | 3              | 3               |
| 10. Federal NB LTR  | *<br>* | 60                       | 31                   | 5.0                             | 315                      | 1794                             | 127.94                    | 3              | 3               |
| 13. Federal SB L    | *<br>* | 60                       | 31                   | 3.0                             | 170                      | 1443                             | 127.94                    | 3              | 3               |
| 14. Federal SB TR   | *<br>* | 60                       | 29                   | 5.0                             | 284                      | 1755                             | 127.94                    | 3              | 3               |

-----  
 RECEPTOR LOCATIONS  
 -----

| RECEPTOR          | *<br>* | COORDINATES (FT) |       |     | *<br>* |
|-------------------|--------|------------------|-------|-----|--------|
|                   |        | X                | Y     | Z   |        |
| 1. EB W Midblock  | *<br>* | 196.0            | 390.0 | 6.0 | *<br>* |
| 2. SW Corner      | *<br>* | 394.0            | 390.0 | 6.0 | *<br>* |
| 3. SB S Midblock  | *<br>* | 394.0            | 200.0 | 6.0 | *<br>* |
| 4. NB S Midblock  | *<br>* | 464.0            | 200.0 | 6.0 | *<br>* |
| 5. SE Corner      | *<br>* | 464.0            | 390.0 | 6.0 | *<br>* |
| 6. EB E Midblock  | *<br>* | 648.0            | 390.0 | 6.0 | *<br>* |
| 7. WB E Midblock  | *<br>* | 648.0            | 464.0 | 6.0 | *<br>* |
| 8. NE Corner      | *<br>* | 464.0            | 464.0 | 6.0 | *<br>* |
| 9. NB N Midblock  | *<br>* | 464.0            | 640.0 | 6.0 | *<br>* |
| 10. SB N Midblock | *<br>* | 396.0            | 640.0 | 6.0 | *<br>* |
| 11. NW Corner     | *<br>* | 396.0            | 464.0 | 6.0 | *<br>* |
| 12. WB W Midblock | *<br>* | 196.0            | 464.0 | 6.0 | *<br>* |

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

| WIND ANGLE (DEGR) | REC1 | REC2 | REC3 | REC4 | REC5 | REC6 | REC7 | REC8 | REC9 | REC10 | REC11 | REC12 |
|-------------------|------|------|------|------|------|------|------|------|------|-------|-------|-------|
| 0.                | 4.6  | 4.4  | 4.3  | 4.4  | 4.4  | 4.6  | 4.3  | 4.4  | 4.4  | 4.4   | 4.4   | 4.3   |
| 10.               | 4.7  | 4.4  | 4.4  | 4.3  | 4.3  | 4.5  | 4.3  | 4.3  | 4.3  | 4.4   | 4.4   | 4.3   |
| 20.               | 4.8  | 4.4  | 4.4  | 4.4  | 4.3  | 4.4  | 4.3  | 4.3  | 4.3  | 4.4   | 4.4   | 4.3   |
| 30.               | 4.9  | 4.3  | 4.6  | 4.4  | 4.3  | 4.4  | 4.3  | 4.3  | 4.3  | 4.5   | 4.4   | 4.3   |
| 40.               | 4.8  | 4.3  | 4.6  | 4.3  | 4.4  | 4.4  | 4.3  | 4.3  | 4.3  | 4.5   | 4.4   | 4.3   |
| 50.               | 4.7  | 4.3  | 4.6  | 4.3  | 4.5  | 4.4  | 4.3  | 4.3  | 4.3  | 4.5   | 4.4   | 4.3   |
| 60.               | 4.6  | 4.4  | 4.6  | 4.3  | 4.5  | 4.4  | 4.3  | 4.3  | 4.3  | 4.5   | 4.4   | 4.3   |
| 70.               | 4.5  | 4.5  | 4.6  | 4.3  | 4.5  | 4.4  | 4.3  | 4.3  | 4.3  | 4.4   | 4.3   | 4.3   |
| 80.               | 4.4  | 4.5  | 4.6  | 4.3  | 4.5  | 4.4  | 4.4  | 4.4  | 4.3  | 4.5   | 4.4   | 4.4   |
| 90.               | 4.3  | 4.5  | 4.5  | 4.3  | 4.4  | 4.3  | 4.4  | 4.5  | 4.3  | 4.6   | 4.4   | 4.4   |
| 100.              | 4.3  | 4.4  | 4.5  | 4.3  | 4.3  | 4.3  | 4.5  | 4.6  | 4.3  | 4.8   | 4.4   | 4.5   |
| 110.              | 4.3  | 4.4  | 4.4  | 4.3  | 4.3  | 4.3  | 4.5  | 4.6  | 4.3  | 4.8   | 4.4   | 4.5   |
| 120.              | 4.3  | 4.4  | 4.4  | 4.3  | 4.3  | 4.3  | 4.5  | 4.5  | 4.3  | 5.0   | 4.3   | 4.5   |
| 130.              | 4.3  | 4.4  | 4.4  | 4.3  | 4.3  | 4.3  | 4.5  | 4.4  | 4.3  | 5.2   | 4.3   | 4.5   |
| 140.              | 4.3  | 4.4  | 4.4  | 4.3  | 4.3  | 4.3  | 4.5  | 4.3  | 4.4  | 5.1   | 4.3   | 4.6   |
| 150.              | 4.3  | 4.4  | 4.4  | 4.3  | 4.3  | 4.3  | 4.5  | 4.3  | 4.4  | 4.9   | 4.4   | 4.7   |
| 160.              | 4.3  | 4.5  | 4.4  | 4.3  | 4.3  | 4.3  | 4.6  | 4.3  | 4.4  | 4.8   | 4.5   | 4.8   |
| 170.              | 4.3  | 4.5  | 4.4  | 4.3  | 4.3  | 4.3  | 4.6  | 4.3  | 4.3  | 4.5   | 4.5   | 4.7   |
| 180.              | 4.3  | 4.4  | 4.3  | 4.3  | 4.4  | 4.3  | 4.8  | 4.4  | 4.4  | 4.4   | 4.6   | 4.7   |
| 190.              | 4.3  | 4.3  | 4.3  | 4.5  | 4.5  | 4.3  | 4.9  | 4.4  | 4.4  | 4.3   | 4.5   | 4.6   |
| 200.              | 4.3  | 4.3  | 4.3  | 4.5  | 4.4  | 4.3  | 4.9  | 4.4  | 4.4  | 4.3   | 4.5   | 4.5   |
| 210.              | 4.3  | 4.3  | 4.3  | 4.5  | 4.4  | 4.3  | 5.0  | 4.4  | 4.4  | 4.3   | 4.5   | 4.5   |
| 220.              | 4.3  | 4.3  | 4.3  | 4.5  | 4.4  | 4.3  | 5.1  | 4.3  | 4.6  | 4.3   | 4.5   | 4.5   |
| 230.              | 4.3  | 4.3  | 4.3  | 4.5  | 4.4  | 4.3  | 5.1  | 4.3  | 4.6  | 4.3   | 4.5   | 4.5   |
| 240.              | 4.3  | 4.3  | 4.3  | 4.5  | 4.4  | 4.3  | 5.1  | 4.4  | 4.8  | 4.3   | 4.5   | 4.5   |
| 250.              | 4.3  | 4.3  | 4.3  | 4.5  | 4.4  | 4.3  | 5.0  | 4.4  | 4.8  | 4.3   | 4.6   | 4.5   |
| 260.              | 4.3  | 4.3  | 4.3  | 4.5  | 4.4  | 4.3  | 4.8  | 4.6  | 4.7  | 4.3   | 4.5   | 4.5   |
| 270.              | 4.3  | 4.4  | 4.3  | 4.6  | 4.5  | 4.3  | 4.6  | 4.5  | 4.6  | 4.3   | 4.5   | 4.4   |
| 280.              | 4.4  | 4.4  | 4.3  | 4.7  | 4.5  | 4.5  | 4.3  | 4.5  | 4.5  | 4.3   | 4.4   | 4.4   |
| 290.              | 4.4  | 4.4  | 4.3  | 4.7  | 4.4  | 4.5  | 4.3  | 4.4  | 4.5  | 4.3   | 4.3   | 4.3   |
| 300.              | 4.4  | 4.4  | 4.3  | 4.8  | 4.4  | 4.6  | 4.3  | 4.4  | 4.5  | 4.3   | 4.3   | 4.3   |
| 310.              | 4.4  | 4.4  | 4.3  | 4.8  | 4.4  | 4.6  | 4.3  | 4.4  | 4.5  | 4.3   | 4.3   | 4.3   |
| 320.              | 4.4  | 4.4  | 4.3  | 4.8  | 4.3  | 4.7  | 4.3  | 4.4  | 4.5  | 4.3   | 4.3   | 4.3   |
| 330.              | 4.4  | 4.4  | 4.3  | 4.7  | 4.3  | 4.7  | 4.3  | 4.4  | 4.5  | 4.3   | 4.3   | 4.3   |
| 340.              | 4.4  | 4.4  | 4.3  | 4.6  | 4.3  | 4.6  | 4.3  | 4.5  | 4.5  | 4.3   | 4.3   | 4.3   |
| 350.              | 4.6  | 4.4  | 4.3  | 4.5  | 4.4  | 4.6  | 4.3  | 4.4  | 4.4  | 4.3   | 4.3   | 4.3   |
| 360.              | 4.6  | 4.4  | 4.3  | 4.4  | 4.4  | 4.6  | 4.3  | 4.4  | 4.4  | 4.4   | 4.4   | 4.3   |
| MAX               | 4.9  | 4.5  | 4.6  | 4.8  | 4.5  | 4.7  | 5.1  | 4.6  | 4.8  | 5.2   | 4.6   | 4.8   |
| DEGR.             | 30   | 70   | 30   | 300  | 50   | 320  | 220  | 100  | 240  | 130   | 180   | 160   |

THE HIGHEST CONCENTRATION OF 5.20 PPM OCCURRED AT RECEPTOR REC10.





JOB: FederalStation2030NoBuildPM

RUN: FederalStation2030NoBuildPM

DATE : 4/15/11  
 TIME : 13: 4:10

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S      VD = .0 CM/S      Z0 = 175. CM  
 U = 1.0 M/S      CLAS = 4 (D)      ATIM = 60. MINUTES      MIXH = 1000. M      AMB = 4.3 PPM

LINK VARIABLES

| LINK DESCRIPTION     | *<br>* X1 | LINK COORDINATES (FT)<br>Y1 | X2    | Y2     | *<br>* LENGTH (FT) | BRG TYPE (DEG) | VPH  | EF (G/MI) | H (FT) | W (FT) | V/C  | QUEUE (VEH) |
|----------------------|-----------|-----------------------------|-------|--------|--------------------|----------------|------|-----------|--------|--------|------|-------------|
| 1. Station EB in     | * .0      | 418.0                       | 200.0 | 418.0  | * 200.             | 90. AG         | 138. | 8.3       | .0     | 24.0   |      |             |
| 2. Station EB L      | * 200.0   | 424.0                       | 206.7 | 424.0  | * 7.               | 90. AG         | 240. | 100.0     | .0     | 12.0   | .09  | .3          |
| 3. Station EB TR     | * 200.0   | 412.0                       | 225.0 | 412.0  | * 25.              | 90. AG         | 240. | 100.0     | .0     | 12.0   | .32  | 1.3         |
| 4. Whisconier EB out | * 454.0   | 418.0                       | 848.0 | 418.0  | * 394.             | 90. AG         | 138. | 8.3       | .0     | 24.0   |      |             |
| 5. Whisconier WB in  | * 848.0   | 442.0                       | 648.0 | 442.0  | * 200.             | 270. AG        | 668. | 8.3       | .0     | 24.0   |      |             |
| 6. Whisconier WB LT  | * 648.0   | 436.0                       | 561.1 | 436.0  | * 87.              | 270. AG        | 200. | 100.0     | .0     | 12.0   | .84  | 4.4         |
| 7. Whisconier WB R   | * 648.0   | 448.0                       | 605.3 | 448.0  | * 43.              | 270. AG        | 137. | 100.0     | .0     | 12.0   | .43  | 2.2         |
| 8. Station WB out    | * 406.0   | 442.0                       | .0    | 442.0  | * 406.             | 270. AG        | 668. | 8.3       | .0     | 24.0   |      |             |
| 9. Federal NB in     | * 442.0   | .0                          | 442.0 | 200.0  | * 200.             | 360. AG        | 765. | 8.3       | .0     | 12.0   |      |             |
| 10. Federal NB LTR   | * 442.0   | 200.0                       | 442.0 | 1582.7 | * 1383.            | 360. AG        | 183. | 100.0     | .0     | 12.0   | 1.17 | 70.2        |
| 11. Federal NB out   | * 442.0   | 454.0                       | 442.0 | 836.0  | * 382.             | 360. AG        | 765. | 8.3       | .0     | 24.0   |      |             |
| 12. Federal SB in    | * 418.0   | 836.0                       | 418.0 | 636.0  | * 200.             | 180. AG        | 733. | 8.3       | .0     | 24.0   |      |             |
| 13. Federal SB L     | * 424.0   | 636.0                       | 424.0 | 583.9  | * 52.              | 180. AG        | 154. | 100.0     | .0     | 12.0   | .44  | 2.6         |
| 14. Federal SB TR    | * 412.0   | 636.0                       | 412.0 | 584.1  | * 52.              | 180. AG        | 143. | 100.0     | .0     | 12.0   | .47  | 2.6         |
| 15. Federal SB out   | * 424.0   | 404.0                       | 424.0 | .0     | * 404.             | 180. AG        | 733. | 8.3       | .0     | 24.0   |      |             |

DATE : 4/15/11  
 TIME : 13: 4:10

-----  
 ADDITIONAL QUEUE LINK PARAMETERS  
 -----

| LINK DESCRIPTION    | *<br>* | CYCLE<br>LENGTH<br>(SEC) | RED<br>TIME<br>(SEC) | CLEARANCE<br>LOST TIME<br>(SEC) | APPROACH<br>VOL<br>(VPH) | SATURATION<br>FLOW RATE<br>(VPH) | IDLE<br>EM FAC<br>(gm/hr) | SIGNAL<br>TYPE | ARRIVAL<br>RATE |
|---------------------|--------|--------------------------|----------------------|---------------------------------|--------------------------|----------------------------------|---------------------------|----------------|-----------------|
| 2. Station EB L     | *<br>* | 60                       | 42                   | 4.0                             | 29                       | 1689                             | 127.94                    | 3              | 3               |
| 3. Station EB TR    | *<br>* | 60                       | 42                   | 4.0                             | 109                      | 1709                             | 127.94                    | 3              | 3               |
| 6. Whisconier WB LT | *<br>* | 60                       | 35                   | 4.0                             | 343                      | 1286                             | 127.94                    | 3              | 3               |
| 7. Whisconier WB R  | *<br>* | 60                       | 24                   | 4.0                             | 325                      | 1515                             | 127.94                    | 3              | 3               |
| 10. Federal NB LTR  | *<br>* | 60                       | 32                   | 5.0                             | 765                      | 1867                             | 127.94                    | 3              | 3               |
| 13. Federal SB L    | *<br>* | 60                       | 27                   | 3.0                             | 353                      | 1709                             | 127.94                    | 3              | 3               |
| 14. Federal SB TR   | *<br>* | 60                       | 25                   | 5.0                             | 380                      | 1728                             | 127.94                    | 3              | 3               |

-----  
 RECEPTOR LOCATIONS  
 -----

| RECEPTOR          | *<br>* | COORDINATES (FT) |       |     | *<br>* |
|-------------------|--------|------------------|-------|-----|--------|
|                   |        | X                | Y     | Z   |        |
| 1. EB W Midblock  | *<br>* | 196.0            | 390.0 | 6.0 | *<br>* |
| 2. SW Corner      | *<br>* | 394.0            | 390.0 | 6.0 | *<br>* |
| 3. SB S Midblock  | *<br>* | 394.0            | 200.0 | 6.0 | *<br>* |
| 4. NB S Midblock  | *<br>* | 464.0            | 200.0 | 6.0 | *<br>* |
| 5. SE Corner      | *<br>* | 464.0            | 390.0 | 6.0 | *<br>* |
| 6. EB E Midblock  | *<br>* | 648.0            | 390.0 | 6.0 | *<br>* |
| 7. WB E Midblock  | *<br>* | 648.0            | 464.0 | 6.0 | *<br>* |
| 8. NE Corner      | *<br>* | 464.0            | 464.0 | 6.0 | *<br>* |
| 9. NB N Midblock  | *<br>* | 464.0            | 640.0 | 6.0 | *<br>* |
| 10. SB N Midblock | *<br>* | 396.0            | 640.0 | 6.0 | *<br>* |
| 11. NW Corner     | *<br>* | 396.0            | 464.0 | 6.0 | *<br>* |
| 12. WB W Midblock | *<br>* | 196.0            | 464.0 | 6.0 | *<br>* |

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

| WIND ANGLE (DEGR) | REC1 | REC2 | REC3 | REC4 | REC5 | REC6 | REC7 | REC8 | REC9 | REC10 | REC11 | REC12 |
|-------------------|------|------|------|------|------|------|------|------|------|-------|-------|-------|
| 0.                | 4.7  | 4.8  | 4.7  | 4.8  | 4.9  | 4.5  | 4.3  | 5.0  | 4.9  | 4.6   | 4.8   | 4.3   |
| 10.               | 4.9  | 4.9  | 4.8  | 4.5  | 4.6  | 4.5  | 4.3  | 4.6  | 4.6  | 5.0   | 5.0   | 4.4   |
| 20.               | 5.0  | 4.8  | 4.9  | 4.4  | 4.4  | 4.4  | 4.3  | 4.4  | 4.4  | 5.0   | 4.9   | 4.4   |
| 30.               | 5.0  | 4.7  | 4.8  | 4.4  | 4.3  | 4.4  | 4.3  | 4.3  | 4.3  | 4.9   | 4.7   | 4.4   |
| 40.               | 4.9  | 4.7  | 4.8  | 4.3  | 4.3  | 4.4  | 4.3  | 4.3  | 4.3  | 4.9   | 4.7   | 4.4   |
| 50.               | 4.8  | 4.6  | 4.8  | 4.3  | 4.4  | 4.4  | 4.3  | 4.3  | 4.3  | 4.9   | 4.7   | 4.4   |
| 60.               | 4.7  | 4.7  | 4.8  | 4.3  | 4.4  | 4.4  | 4.3  | 4.3  | 4.3  | 4.9   | 4.7   | 4.4   |
| 70.               | 4.6  | 4.8  | 4.6  | 4.3  | 4.4  | 4.4  | 4.3  | 4.3  | 4.3  | 4.9   | 4.7   | 4.4   |
| 80.               | 4.5  | 4.8  | 4.6  | 4.3  | 4.4  | 4.4  | 4.4  | 4.3  | 4.3  | 4.8   | 4.7   | 4.5   |
| 90.               | 4.4  | 4.8  | 4.5  | 4.3  | 4.4  | 4.3  | 4.4  | 4.4  | 4.3  | 5.0   | 4.8   | 4.5   |
| 100.              | 4.4  | 4.7  | 4.6  | 4.3  | 4.3  | 4.3  | 4.5  | 4.4  | 4.3  | 5.2   | 4.8   | 4.6   |
| 110.              | 4.4  | 4.8  | 4.5  | 4.3  | 4.3  | 4.3  | 4.5  | 4.4  | 4.3  | 5.2   | 4.7   | 4.6   |
| 120.              | 4.4  | 4.8  | 4.6  | 4.3  | 4.3  | 4.3  | 4.5  | 4.4  | 4.3  | 5.3   | 4.6   | 4.6   |
| 130.              | 4.3  | 4.8  | 4.6  | 4.3  | 4.3  | 4.3  | 4.5  | 4.3  | 4.3  | 5.3   | 4.6   | 4.6   |
| 140.              | 4.3  | 4.8  | 4.6  | 4.3  | 4.3  | 4.3  | 4.5  | 4.3  | 4.4  | 5.4   | 4.6   | 4.6   |
| 150.              | 4.3  | 4.8  | 4.6  | 4.3  | 4.3  | 4.3  | 4.5  | 4.3  | 4.4  | 5.3   | 4.8   | 4.6   |
| 160.              | 4.3  | 4.7  | 4.6  | 4.3  | 4.3  | 4.3  | 4.6  | 4.3  | 4.3  | 5.1   | 4.8   | 4.8   |
| 170.              | 4.3  | 4.7  | 4.5  | 4.3  | 4.4  | 4.3  | 4.6  | 4.4  | 4.6  | 5.0   | 4.7   | 4.8   |
| 180.              | 4.3  | 4.5  | 4.4  | 4.4  | 4.7  | 4.3  | 4.8  | 4.7  | 4.8  | 4.7   | 4.6   | 4.7   |
| 190.              | 4.3  | 4.3  | 4.3  | 4.6  | 4.8  | 4.3  | 4.8  | 4.9  | 5.1  | 4.4   | 4.6   | 4.6   |
| 200.              | 4.3  | 4.3  | 4.3  | 4.6  | 5.0  | 4.3  | 4.9  | 4.9  | 5.2  | 4.3   | 4.5   | 4.5   |
| 210.              | 4.3  | 4.3  | 4.3  | 4.6  | 5.0  | 4.3  | 5.0  | 4.9  | 5.1  | 4.3   | 4.5   | 4.5   |
| 220.              | 4.3  | 4.3  | 4.3  | 4.6  | 4.9  | 4.3  | 5.2  | 4.9  | 5.3  | 4.3   | 4.5   | 4.5   |
| 230.              | 4.3  | 4.3  | 4.3  | 4.6  | 4.8  | 4.4  | 5.2  | 4.7  | 5.2  | 4.3   | 4.5   | 4.5   |
| 240.              | 4.3  | 4.3  | 4.3  | 4.5  | 4.8  | 4.4  | 5.1  | 4.9  | 5.3  | 4.3   | 4.5   | 4.5   |
| 250.              | 4.3  | 4.3  | 4.3  | 4.6  | 4.8  | 4.4  | 5.0  | 4.9  | 5.2  | 4.3   | 4.5   | 4.5   |
| 260.              | 4.3  | 4.3  | 4.3  | 4.6  | 4.8  | 4.4  | 4.8  | 4.9  | 5.1  | 4.3   | 4.5   | 4.5   |
| 270.              | 4.3  | 4.4  | 4.3  | 4.7  | 4.9  | 4.4  | 4.6  | 5.0  | 5.2  | 4.3   | 4.5   | 4.4   |
| 280.              | 4.4  | 4.4  | 4.3  | 4.7  | 4.9  | 4.4  | 4.4  | 5.0  | 5.0  | 4.3   | 4.4   | 4.4   |
| 290.              | 4.4  | 4.4  | 4.3  | 4.7  | 4.9  | 4.5  | 4.4  | 4.9  | 5.0  | 4.3   | 4.3   | 4.3   |
| 300.              | 4.4  | 4.4  | 4.3  | 4.8  | 4.8  | 4.6  | 4.4  | 4.9  | 5.0  | 4.3   | 4.3   | 4.3   |
| 310.              | 4.4  | 4.4  | 4.3  | 4.8  | 4.8  | 4.7  | 4.4  | 4.9  | 5.0  | 4.3   | 4.3   | 4.3   |
| 320.              | 4.4  | 4.4  | 4.3  | 4.9  | 4.8  | 4.8  | 4.4  | 5.0  | 5.1  | 4.3   | 4.3   | 4.3   |
| 330.              | 4.4  | 4.4  | 4.3  | 4.9  | 4.9  | 4.8  | 4.4  | 5.0  | 5.1  | 4.3   | 4.3   | 4.3   |
| 340.              | 4.4  | 4.4  | 4.3  | 5.0  | 5.0  | 4.7  | 4.4  | 5.4  | 5.2  | 4.3   | 4.3   | 4.3   |
| 350.              | 4.5  | 4.5  | 4.4  | 5.0  | 5.1  | 4.7  | 4.4  | 5.2  | 5.2  | 4.5   | 4.4   | 4.3   |
| 360.              | 4.7  | 4.8  | 4.7  | 4.8  | 4.9  | 4.5  | 4.3  | 5.0  | 4.9  | 4.6   | 4.8   | 4.3   |
| MAX               | 5.0  | 4.9  | 4.9  | 5.0  | 5.1  | 4.8  | 5.2  | 5.4  | 5.3  | 5.4   | 5.0   | 4.8   |
| DEGR.             | 20   | 10   | 20   | 340  | 350  | 320  | 220  | 340  | 220  | 140   | 10    | 160   |

THE HIGHEST CONCENTRATION OF 5.40 PPM OCCURRED AT RECEPTOR REC10.



JOB: FederalStation2030BuildAM

RUN: FederalStation2030BuildAM

DATE : 4/15/11  
 TIME : 13: 7: 2

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S      VD = .0 CM/S      Z0 = 175. CM  
 U = 1.0 M/S      CLAS = 4 (D)      ATIM = 60. MINUTES      MIXH = 1000. M      AMB = 4.3 PPM

LINK VARIABLES

| LINK DESCRIPTION     | *<br>* X1 | LINK COORDINATES (FT)<br>Y1 | X2    | Y2    | *<br>* | LENGTH<br>(FT) | BRG TYPE<br>(DEG) | VPH  | EF<br>(G/MI) | H<br>(FT) | W<br>(FT) | V/C | QUEUE<br>(VEH) |
|----------------------|-----------|-----------------------------|-------|-------|--------|----------------|-------------------|------|--------------|-----------|-----------|-----|----------------|
| 1. Station EB in     | * .0      | 418.0                       | 200.0 | 418.0 | * *    | 200.           | 90. AG            | 161. | 8.3          | .0        | 24.0      |     |                |
| 2. Station EB L      | * 200.0   | 424.0                       | 208.5 | 424.0 | * *    | 9.             | 90. AG            | 223. | 100.0        | .0        | 12.0      | .08 | .4             |
| 3. Station EB TR     | * 200.0   | 412.0                       | 225.8 | 412.0 | * *    | 26.            | 90. AG            | 223. | 100.0        | .0        | 12.0      | .25 | 1.3            |
| 4. Whisconier EB out | * 454.0   | 418.0                       | 848.0 | 418.0 | * *    | 394.           | 90. AG            | 161. | 8.3          | .0        | 24.0      |     |                |
| 5. Whisconier WB in  | * 848.0   | 442.0                       | 648.0 | 442.0 | * *    | 200.           | 270. AG           | 774. | 8.3          | .0        | 24.0      |     |                |
| 6. Whisconier WB LT  | * 648.0   | 436.0                       | 490.5 | 436.0 | * *    | 158.           | 270. AG           | 177. | 100.0        | .0        | 12.0      | .98 | 8.0            |
| 7. Whisconier WB R   | * 648.0   | 448.0                       | 600.8 | 448.0 | * *    | 47.            | 270. AG           | 143. | 100.0        | .0        | 12.0      | .47 | 2.4            |
| 8. Station WB out    | * 406.0   | 442.0                       | .0    | 442.0 | * *    | 406.           | 270. AG           | 774. | 8.3          | .0        | 24.0      |     |                |
| 9. Federal NB in     | * 442.0   | .0                          | 442.0 | 200.0 | * *    | 200.           | 360. AG           | 345. | 8.3          | .0        | 12.0      |     |                |
| 10. Federal NB LTR   | * 442.0   | 200.0                       | 442.0 | 258.5 | * *    | 58.            | 360. AG           | 177. | 100.0        | .0        | 12.0      | .53 | 3.0            |
| 11. Federal NB out   | * 442.0   | 454.0                       | 442.0 | 836.0 | * *    | 382.           | 360. AG           | 345. | 8.3          | .0        | 24.0      |     |                |
| 12. Federal SB in    | * 418.0   | 836.0                       | 418.0 | 636.0 | * *    | 200.           | 180. AG           | 484. | 8.3          | .0        | 24.0      |     |                |
| 13. Federal SB L     | * 424.0   | 636.0                       | 424.0 | 602.1 | * *    | 34.            | 180. AG           | 177. | 100.0        | .0        | 12.0      | .35 | 1.7            |
| 14. Federal SB TR    | * 412.0   | 636.0                       | 412.0 | 591.0 | * *    | 45.            | 180. AG           | 166. | 100.0        | .0        | 12.0      | .40 | 2.3            |
| 15. Federal SB out   | * 424.0   | 404.0                       | 424.0 | .0    | * *    | 404.           | 180. AG           | 484. | 8.3          | .0        | 24.0      |     |                |

DATE : 4/15/11  
 TIME : 13: 7: 2

-----  
 ADDITIONAL QUEUE LINK PARAMETERS  
 -----

| LINK DESCRIPTION    | *<br>* | CYCLE<br>LENGTH<br>(SEC) | RED<br>TIME<br>(SEC) | CLEARANCE<br>LOST TIME<br>(SEC) | APPROACH<br>VOL<br>(VPH) | SATURATION<br>FLOW RATE<br>(VPH) | IDLE<br>EM FAC<br>(gm/hr) | SIGNAL<br>TYPE | ARRIVAL<br>RATE |
|---------------------|--------|--------------------------|----------------------|---------------------------------|--------------------------|----------------------------------|---------------------------|----------------|-----------------|
| 2. Station EB L     | *      | 60                       | 39                   | 4.0                             | 40                       | 1926                             | 127.94                    | 3              | 3               |
| 3. Station EB TR    | *      | 60                       | 39                   | 4.0                             | 121                      | 1946                             | 127.94                    | 3              | 3               |
| 6. Whisconier WB LT | *      | 60                       | 31                   | 4.0                             | 429                      | 1143                             | 127.94                    | 3              | 3               |
| 7. Whisconier WB R  | *      | 60                       | 25                   | 4.0                             | 345                      | 1515                             | 127.94                    | 3              | 3               |
| 10. Federal NB LTR  | *      | 60                       | 31                   | 5.0                             | 345                      | 1778                             | 127.94                    | 3              | 3               |
| 13. Federal SB L    | *      | 60                       | 31                   | 3.0                             | 200                      | 1445                             | 127.94                    | 3              | 3               |
| 14. Federal SB TR   | *      | 60                       | 29                   | 5.0                             | 284                      | 1755                             | 127.94                    | 3              | 3               |

-----  
 RECEPTOR LOCATIONS  
 -----

| RECEPTOR          | *<br>* | COORDINATES (FT) |       |     | *<br>* |
|-------------------|--------|------------------|-------|-----|--------|
|                   |        | X                | Y     | Z   |        |
| 1. EB W Midblock  | *      | 196.0            | 390.0 | 6.0 | *      |
| 2. SW Corner      | *      | 394.0            | 390.0 | 6.0 | *      |
| 3. SB S Midblock  | *      | 394.0            | 200.0 | 6.0 | *      |
| 4. NB S Midblock  | *      | 464.0            | 200.0 | 6.0 | *      |
| 5. SE Corner      | *      | 464.0            | 390.0 | 6.0 | *      |
| 6. EB E Midblock  | *      | 648.0            | 390.0 | 6.0 | *      |
| 7. WB E Midblock  | *      | 648.0            | 464.0 | 6.0 | *      |
| 8. NE Corner      | *      | 464.0            | 464.0 | 6.0 | *      |
| 9. NB N Midblock  | *      | 464.0            | 640.0 | 6.0 | *      |
| 10. SB N Midblock | *      | 396.0            | 640.0 | 6.0 | *      |
| 11. NW Corner     | *      | 396.0            | 464.0 | 6.0 | *      |
| 12. WB W Midblock | *      | 196.0            | 464.0 | 6.0 | *      |

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

| WIND ANGLE (DEGR) | REC1 | REC2 | REC3 | REC4 | REC5 | REC6 | REC7 | REC8 | REC9 | REC10 | REC11 | REC12 |
|-------------------|------|------|------|------|------|------|------|------|------|-------|-------|-------|
| 0.                | 4.6  | 4.4  | 4.4  | 4.4  | 4.4  | 4.6  | 4.3  | 4.4  | 4.4  | 4.4   | 4.4   | 4.3   |
| 10.               | 4.7  | 4.5  | 4.4  | 4.4  | 4.3  | 4.5  | 4.3  | 4.3  | 4.3  | 4.4   | 4.5   | 4.3   |
| 20.               | 4.8  | 4.4  | 4.4  | 4.4  | 4.4  | 4.4  | 4.3  | 4.3  | 4.3  | 4.6   | 4.4   | 4.3   |
| 30.               | 4.9  | 4.3  | 4.6  | 4.4  | 4.4  | 4.4  | 4.3  | 4.3  | 4.3  | 4.5   | 4.4   | 4.3   |
| 40.               | 4.8  | 4.3  | 4.6  | 4.3  | 4.5  | 4.4  | 4.3  | 4.3  | 4.3  | 4.5   | 4.4   | 4.3   |
| 50.               | 4.7  | 4.4  | 4.6  | 4.3  | 4.6  | 4.4  | 4.3  | 4.3  | 4.3  | 4.5   | 4.4   | 4.3   |
| 60.               | 4.6  | 4.4  | 4.6  | 4.3  | 4.6  | 4.4  | 4.3  | 4.3  | 4.3  | 4.5   | 4.4   | 4.3   |
| 70.               | 4.5  | 4.6  | 4.6  | 4.3  | 4.5  | 4.4  | 4.3  | 4.3  | 4.3  | 4.5   | 4.4   | 4.3   |
| 80.               | 4.5  | 4.6  | 4.6  | 4.3  | 4.5  | 4.4  | 4.4  | 4.4  | 4.3  | 4.6   | 4.4   | 4.4   |
| 90.               | 4.3  | 4.5  | 4.5  | 4.3  | 4.4  | 4.3  | 4.4  | 4.5  | 4.3  | 4.7   | 4.4   | 4.5   |
| 100.              | 4.3  | 4.4  | 4.5  | 4.3  | 4.3  | 4.3  | 4.5  | 4.6  | 4.3  | 4.9   | 4.5   | 4.6   |
| 110.              | 4.3  | 4.4  | 4.4  | 4.3  | 4.3  | 4.3  | 4.5  | 4.7  | 4.3  | 4.9   | 4.4   | 4.5   |
| 120.              | 4.3  | 4.4  | 4.4  | 4.3  | 4.3  | 4.3  | 4.5  | 4.6  | 4.3  | 5.0   | 4.4   | 4.5   |
| 130.              | 4.3  | 4.4  | 4.4  | 4.3  | 4.3  | 4.3  | 4.5  | 4.6  | 4.3  | 5.2   | 4.3   | 4.5   |
| 140.              | 4.3  | 4.4  | 4.4  | 4.3  | 4.3  | 4.3  | 4.5  | 4.5  | 4.4  | 5.1   | 4.3   | 4.6   |
| 150.              | 4.3  | 4.4  | 4.4  | 4.3  | 4.3  | 4.3  | 4.5  | 4.4  | 4.4  | 5.1   | 4.4   | 4.7   |
| 160.              | 4.3  | 4.5  | 4.4  | 4.3  | 4.3  | 4.3  | 4.6  | 4.3  | 4.4  | 4.9   | 4.5   | 4.8   |
| 170.              | 4.3  | 4.5  | 4.4  | 4.3  | 4.3  | 4.3  | 4.6  | 4.3  | 4.4  | 4.5   | 4.5   | 4.8   |
| 180.              | 4.3  | 4.4  | 4.4  | 4.3  | 4.5  | 4.3  | 4.8  | 4.4  | 4.4  | 4.4   | 4.6   | 4.7   |
| 190.              | 4.3  | 4.3  | 4.3  | 4.5  | 4.5  | 4.3  | 4.9  | 4.4  | 4.4  | 4.3   | 4.5   | 4.6   |
| 200.              | 4.3  | 4.3  | 4.3  | 4.5  | 4.5  | 4.3  | 4.9  | 4.4  | 4.4  | 4.3   | 4.5   | 4.5   |
| 210.              | 4.3  | 4.3  | 4.3  | 4.5  | 4.4  | 4.3  | 5.0  | 4.4  | 4.5  | 4.3   | 4.5   | 4.5   |
| 220.              | 4.3  | 4.3  | 4.3  | 4.5  | 4.4  | 4.3  | 5.1  | 4.3  | 4.6  | 4.3   | 4.5   | 4.5   |
| 230.              | 4.3  | 4.3  | 4.3  | 4.5  | 4.4  | 4.3  | 5.1  | 4.3  | 4.8  | 4.3   | 4.5   | 4.5   |
| 240.              | 4.3  | 4.3  | 4.3  | 4.5  | 4.4  | 4.3  | 5.1  | 4.4  | 4.8  | 4.3   | 4.5   | 4.5   |
| 250.              | 4.3  | 4.3  | 4.3  | 4.6  | 4.4  | 4.3  | 5.0  | 4.4  | 4.8  | 4.3   | 4.6   | 4.5   |
| 260.              | 4.3  | 4.3  | 4.3  | 4.5  | 4.4  | 4.3  | 4.8  | 4.6  | 4.7  | 4.3   | 4.5   | 4.5   |
| 270.              | 4.3  | 4.4  | 4.3  | 4.6  | 4.5  | 4.4  | 4.7  | 4.5  | 4.6  | 4.3   | 4.5   | 4.4   |
| 280.              | 4.4  | 4.4  | 4.3  | 4.7  | 4.5  | 4.5  | 4.4  | 4.5  | 4.5  | 4.3   | 4.4   | 4.4   |
| 290.              | 4.4  | 4.4  | 4.3  | 4.7  | 4.4  | 4.5  | 4.3  | 4.4  | 4.5  | 4.3   | 4.3   | 4.3   |
| 300.              | 4.4  | 4.4  | 4.3  | 4.8  | 4.4  | 4.6  | 4.3  | 4.4  | 4.5  | 4.3   | 4.3   | 4.3   |
| 310.              | 4.4  | 4.4  | 4.3  | 4.8  | 4.4  | 4.6  | 4.3  | 4.4  | 4.5  | 4.3   | 4.3   | 4.3   |
| 320.              | 4.4  | 4.4  | 4.3  | 4.8  | 4.3  | 4.7  | 4.3  | 4.4  | 4.5  | 4.3   | 4.3   | 4.3   |
| 330.              | 4.4  | 4.4  | 4.3  | 4.8  | 4.3  | 4.7  | 4.3  | 4.4  | 4.5  | 4.3   | 4.3   | 4.3   |
| 340.              | 4.4  | 4.4  | 4.3  | 4.7  | 4.4  | 4.6  | 4.3  | 4.5  | 4.5  | 4.3   | 4.3   | 4.3   |
| 350.              | 4.6  | 4.4  | 4.3  | 4.6  | 4.4  | 4.6  | 4.3  | 4.4  | 4.4  | 4.3   | 4.3   | 4.3   |
| 360.              | 4.6  | 4.4  | 4.4  | 4.4  | 4.4  | 4.6  | 4.3  | 4.4  | 4.4  | 4.4   | 4.4   | 4.3   |
| MAX               | 4.9  | 4.6  | 4.6  | 4.8  | 4.6  | 4.7  | 5.1  | 4.7  | 4.8  | 5.2   | 4.6   | 4.8   |
| DEGR.             | 30   | 70   | 30   | 300  | 50   | 320  | 220  | 110  | 230  | 130   | 180   | 160   |

THE HIGHEST CONCENTRATION OF 5.20 PPM OCCURRED AT RECEPTOR REC10.





JOB: FederalStation2030BuildPM

RUN: FederalStation2030BuildPM

DATE : 4/15/11  
 TIME : 13: 9:36

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S      VD = .0 CM/S      Z0 = 175. CM  
 U = 1.0 M/S      CLAS = 4 (D)      ATIM = 60. MINUTES      MIXH = 1000. M      AMB = 4.3 PPM

LINK VARIABLES

| LINK DESCRIPTION     | *<br>* X1 | LINK COORDINATES (FT)<br>Y1 | X2    | Y2     | *<br>*<br>* LENGTH (FT) | BRG TYPE (DEG) | VPH  | EF (G/MI) | H (FT) | W (FT) | V/C  | QUEUE (VEH) |
|----------------------|-----------|-----------------------------|-------|--------|-------------------------|----------------|------|-----------|--------|--------|------|-------------|
| 1. Station EB in     | * .0      | 418.0                       | 200.0 | 418.0  | * 200.                  | 90. AG         | 139. | 8.3       | .0     | 24.0   |      |             |
| 2. Station EB L      | * 200.0   | 424.0                       | 206.7 | 424.0  | * 7.                    | 90. AG         | 240. | 100.0     | .0     | 12.0   | .09  | .3          |
| 3. Station EB TR     | * 200.0   | 412.0                       | 225.3 | 412.0  | * 25.                   | 90. AG         | 240. | 100.0     | .0     | 12.0   | .32  | 1.3         |
| 4. Whisconier EB out | * 454.0   | 418.0                       | 848.0 | 418.0  | * 394.                  | 90. AG         | 139. | 8.3       | .0     | 24.0   |      |             |
| 5. Whisconier WB in  | * 848.0   | 442.0                       | 648.0 | 442.0  | * 200.                  | 270. AG        | 740. | 8.3       | .0     | 24.0   |      |             |
| 6. Whisconier WB LT  | * 648.0   | 436.0                       | 506.0 | 436.0  | * 142.                  | 270. AG        | 200. | 100.0     | .0     | 12.0   | .96  | 7.2         |
| 7. Whisconier WB R   | * 648.0   | 448.0                       | 601.4 | 448.0  | * 47.                   | 270. AG        | 137. | 100.0     | .0     | 12.0   | .47  | 2.4         |
| 8. Station WB out    | * 406.0   | 442.0                       | .0    | 442.0  | * 406.                  | 270. AG        | 740. | 8.3       | .0     | 24.0   |      |             |
| 9. Federal NB in     | * 442.0   | .0                          | 442.0 | 200.0  | * 200.                  | 360. AG        | 767. | 8.3       | .0     | 12.0   |      |             |
| 10. Federal NB LTR   | * 442.0   | 200.0                       | 442.0 | 1603.1 | * 1403.                 | 360. AG        | 183. | 100.0     | .0     | 12.0   | 1.17 | 71.3        |
| 11. Federal NB out   | * 442.0   | 454.0                       | 442.0 | 836.0  | * 382.                  | 360. AG        | 767. | 8.3       | .0     | 24.0   |      |             |
| 12. Federal SB in    | * 418.0   | 836.0                       | 418.0 | 636.0  | * 200.                  | 180. AG        | 735. | 8.3       | .0     | 24.0   |      |             |
| 13. Federal SB L     | * 424.0   | 636.0                       | 424.0 | 583.6  | * 52.                   | 180. AG        | 154. | 100.0     | .0     | 12.0   | .44  | 2.7         |
| 14. Federal SB TR    | * 412.0   | 636.0                       | 412.0 | 584.1  | * 52.                   | 180. AG        | 143. | 100.0     | .0     | 12.0   | .47  | 2.6         |
| 15. Federal SB out   | * 424.0   | 404.0                       | 424.0 | .0     | * 404.                  | 180. AG        | 735. | 8.3       | .0     | 24.0   |      |             |

DATE : 4/15/11  
 TIME : 13: 9:36

-----  
 ADDITIONAL QUEUE LINK PARAMETERS  
 -----

| LINK DESCRIPTION    | *<br>* | CYCLE<br>LENGTH<br>(SEC) | RED<br>TIME<br>(SEC) | CLEARANCE<br>LOST TIME<br>(SEC) | APPROACH<br>VOL<br>(VPH) | SATURATION<br>FLOW RATE<br>(VPH) | IDLE<br>EM FAC<br>(gm/hr) | SIGNAL<br>TYPE | ARRIVAL<br>RATE |
|---------------------|--------|--------------------------|----------------------|---------------------------------|--------------------------|----------------------------------|---------------------------|----------------|-----------------|
| 2. Station EB L     | *      | 60                       | 42                   | 4.0                             | 29                       | 1689                             | 127.94                    | 3              | 3               |
| 3. Station EB TR    | *      | 60                       | 42                   | 4.0                             | 110                      | 1709                             | 127.94                    | 3              | 3               |
| 6. Whisconier WB LT | *      | 60                       | 35                   | 4.0                             | 385                      | 1269                             | 127.94                    | 3              | 3               |
| 7. Whisconier WB R  | *      | 60                       | 24                   | 4.0                             | 355                      | 1515                             | 127.94                    | 3              | 3               |
| 10. Federal NB LTR  | *      | 60                       | 32                   | 5.0                             | 767                      | 1867                             | 127.94                    | 3              | 3               |
| 13. Federal SB L    | *      | 60                       | 27                   | 3.0                             | 355                      | 1710                             | 127.94                    | 3              | 3               |
| 14. Federal SB TR   | *      | 60                       | 25                   | 5.0                             | 380                      | 1728                             | 127.94                    | 3              | 3               |

-----  
 RECEPTOR LOCATIONS  
 -----

| RECEPTOR          | *<br>* | COORDINATES (FT) |       |     | *<br>* |
|-------------------|--------|------------------|-------|-----|--------|
|                   |        | X                | Y     | Z   |        |
| 1. EB W Midblock  | *      | 196.0            | 390.0 | 6.0 | *      |
| 2. SW Corner      | *      | 394.0            | 390.0 | 6.0 | *      |
| 3. SB S Midblock  | *      | 394.0            | 200.0 | 6.0 | *      |
| 4. NB S Midblock  | *      | 464.0            | 200.0 | 6.0 | *      |
| 5. SE Corner      | *      | 464.0            | 390.0 | 6.0 | *      |
| 6. EB E Midblock  | *      | 648.0            | 390.0 | 6.0 | *      |
| 7. WB E Midblock  | *      | 648.0            | 464.0 | 6.0 | *      |
| 8. NE Corner      | *      | 464.0            | 464.0 | 6.0 | *      |
| 9. NB N Midblock  | *      | 464.0            | 640.0 | 6.0 | *      |
| 10. SB N Midblock | *      | 396.0            | 640.0 | 6.0 | *      |
| 11. NW Corner     | *      | 396.0            | 464.0 | 6.0 | *      |
| 12. WB W Midblock | *      | 196.0            | 464.0 | 6.0 | *      |

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

| WIND ANGLE (DEGR) | REC1 | REC2 | REC3 | REC4 | REC5 | REC6 | REC7 | REC8 | REC9 | REC10 | REC11 | REC12 |
|-------------------|------|------|------|------|------|------|------|------|------|-------|-------|-------|
| 0.                | 4.7  | 4.8  | 4.7  | 4.8  | 4.9  | 4.6  | 4.3  | 5.0  | 4.9  | 4.6   | 4.8   | 4.3   |
| 10.               | 4.9  | 4.9  | 4.8  | 4.6  | 4.6  | 4.5  | 4.3  | 4.6  | 4.6  | 5.0   | 5.0   | 4.4   |
| 20.               | 5.0  | 4.8  | 4.9  | 4.5  | 4.4  | 4.4  | 4.3  | 4.4  | 4.4  | 5.0   | 4.9   | 4.4   |
| 30.               | 5.0  | 4.7  | 4.9  | 4.4  | 4.4  | 4.4  | 4.3  | 4.3  | 4.3  | 4.9   | 4.7   | 4.4   |
| 40.               | 4.9  | 4.7  | 4.9  | 4.4  | 4.4  | 4.4  | 4.3  | 4.3  | 4.3  | 4.9   | 4.7   | 4.4   |
| 50.               | 4.8  | 4.6  | 4.8  | 4.3  | 4.5  | 4.4  | 4.3  | 4.3  | 4.3  | 4.9   | 4.7   | 4.4   |
| 60.               | 4.7  | 4.8  | 4.8  | 4.3  | 4.6  | 4.4  | 4.3  | 4.3  | 4.3  | 4.9   | 4.7   | 4.4   |
| 70.               | 4.6  | 4.8  | 4.7  | 4.3  | 4.6  | 4.4  | 4.3  | 4.3  | 4.3  | 4.9   | 4.7   | 4.4   |
| 80.               | 4.6  | 4.9  | 4.6  | 4.3  | 4.5  | 4.4  | 4.4  | 4.4  | 4.3  | 4.8   | 4.8   | 4.5   |
| 90.               | 4.4  | 4.8  | 4.5  | 4.3  | 4.4  | 4.3  | 4.4  | 4.5  | 4.3  | 5.0   | 4.8   | 4.6   |
| 100.              | 4.4  | 4.7  | 4.6  | 4.3  | 4.3  | 4.3  | 4.5  | 4.6  | 4.3  | 5.2   | 4.9   | 4.7   |
| 110.              | 4.4  | 4.8  | 4.6  | 4.3  | 4.3  | 4.3  | 4.5  | 4.6  | 4.3  | 5.2   | 4.7   | 4.6   |
| 120.              | 4.4  | 4.8  | 4.6  | 4.3  | 4.3  | 4.3  | 4.5  | 4.6  | 4.3  | 5.3   | 4.7   | 4.6   |
| 130.              | 4.3  | 4.8  | 4.6  | 4.3  | 4.3  | 4.3  | 4.5  | 4.5  | 4.3  | 5.4   | 4.6   | 4.6   |
| 140.              | 4.3  | 4.8  | 4.6  | 4.3  | 4.3  | 4.3  | 4.5  | 4.4  | 4.4  | 5.5   | 4.6   | 4.6   |
| 150.              | 4.3  | 4.8  | 4.6  | 4.3  | 4.3  | 4.3  | 4.5  | 4.3  | 4.4  | 5.4   | 4.8   | 4.6   |
| 160.              | 4.3  | 4.7  | 4.6  | 4.3  | 4.3  | 4.3  | 4.7  | 4.3  | 4.4  | 5.1   | 4.8   | 4.8   |
| 170.              | 4.3  | 4.7  | 4.5  | 4.3  | 4.4  | 4.3  | 4.6  | 4.4  | 4.7  | 5.0   | 4.7   | 4.8   |
| 180.              | 4.3  | 4.5  | 4.4  | 4.4  | 4.7  | 4.3  | 4.8  | 4.7  | 4.8  | 4.7   | 4.7   | 4.7   |
| 190.              | 4.3  | 4.3  | 4.3  | 4.6  | 4.8  | 4.3  | 4.9  | 4.9  | 5.1  | 4.4   | 4.6   | 4.6   |
| 200.              | 4.3  | 4.3  | 4.3  | 4.6  | 5.0  | 4.3  | 4.9  | 4.9  | 5.2  | 4.3   | 4.5   | 4.5   |
| 210.              | 4.3  | 4.3  | 4.3  | 4.6  | 5.0  | 4.3  | 5.0  | 4.9  | 5.1  | 4.3   | 4.5   | 4.5   |
| 220.              | 4.3  | 4.3  | 4.3  | 4.6  | 4.9  | 4.3  | 5.2  | 4.9  | 5.3  | 4.3   | 4.5   | 4.5   |
| 230.              | 4.3  | 4.3  | 4.3  | 4.6  | 4.8  | 4.4  | 5.2  | 4.7  | 5.2  | 4.3   | 4.5   | 4.5   |
| 240.              | 4.3  | 4.3  | 4.3  | 4.5  | 4.8  | 4.4  | 5.3  | 4.9  | 5.3  | 4.3   | 4.5   | 4.5   |
| 250.              | 4.3  | 4.3  | 4.3  | 4.6  | 4.8  | 4.4  | 5.1  | 4.9  | 5.2  | 4.3   | 4.6   | 4.5   |
| 260.              | 4.3  | 4.3  | 4.3  | 4.6  | 4.8  | 4.4  | 4.9  | 5.0  | 5.1  | 4.3   | 4.5   | 4.5   |
| 270.              | 4.3  | 4.4  | 4.3  | 4.7  | 4.9  | 4.4  | 4.8  | 5.0  | 5.2  | 4.3   | 4.5   | 4.4   |
| 280.              | 4.4  | 4.4  | 4.3  | 4.7  | 4.9  | 4.6  | 4.5  | 5.0  | 5.0  | 4.3   | 4.4   | 4.4   |
| 290.              | 4.4  | 4.4  | 4.3  | 4.7  | 4.9  | 4.6  | 4.4  | 4.9  | 5.0  | 4.3   | 4.3   | 4.3   |
| 300.              | 4.4  | 4.4  | 4.3  | 4.8  | 4.8  | 4.7  | 4.4  | 4.9  | 5.0  | 4.3   | 4.3   | 4.3   |
| 310.              | 4.4  | 4.4  | 4.3  | 4.8  | 4.8  | 4.7  | 4.4  | 4.9  | 5.0  | 4.3   | 4.3   | 4.3   |
| 320.              | 4.4  | 4.4  | 4.3  | 4.9  | 4.8  | 4.8  | 4.4  | 5.0  | 5.1  | 4.3   | 4.3   | 4.3   |
| 330.              | 4.4  | 4.4  | 4.3  | 4.9  | 4.9  | 4.8  | 4.4  | 5.0  | 5.1  | 4.3   | 4.3   | 4.3   |
| 340.              | 4.4  | 4.4  | 4.3  | 5.0  | 5.0  | 4.7  | 4.4  | 5.4  | 5.2  | 4.3   | 4.3   | 4.3   |
| 350.              | 4.5  | 4.5  | 4.4  | 5.0  | 5.1  | 4.7  | 4.4  | 5.2  | 5.2  | 4.5   | 4.4   | 4.3   |
| 360.              | 4.7  | 4.8  | 4.7  | 4.8  | 4.9  | 4.6  | 4.3  | 5.0  | 4.9  | 4.6   | 4.8   | 4.3   |
| MAX               | 5.0  | 4.9  | 4.9  | 5.0  | 5.1  | 4.8  | 5.3  | 5.4  | 5.3  | 5.5   | 5.0   | 4.8   |
| DEGR.             | 20   | 10   | 20   | 340  | 350  | 320  | 240  | 340  | 220  | 140   | 10    | 160   |

THE HIGHEST CONCENTRATION OF 5.50 PPM OCCURRED AT RECEPTOR REC10.



JOB: FederalStation2030MitigatedBuildAM

RUN: FederalStation2030MitigatedBuildAM

DATE : 4/15/11  
 TIME : 13:11:35

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S      VD = .0 CM/S      Z0 = 175. CM  
 U = 1.0 M/S      CLAS = 4 (D)      ATIM = 60. MINUTES      MIXH = 1000. M      AMB = 4.3 PPM

LINK VARIABLES

| LINK DESCRIPTION     | *<br>* X1 | LINK COORDINATES (FT)<br>Y1 | X2    | Y2    | *<br>* | LENGTH<br>(FT) | BRG TYPE<br>(DEG) | VPH  | EF<br>(G/MI) | H<br>(FT) | W<br>(FT) | V/C | QUEUE<br>(VEH) |
|----------------------|-----------|-----------------------------|-------|-------|--------|----------------|-------------------|------|--------------|-----------|-----------|-----|----------------|
| 1. Station EB in     | * .0      | 418.0                       | 200.0 | 418.0 | * *    | 200.           | 90. AG            | 161. | 8.3          | .0        | 24.0      |     |                |
| 2. Station EB L      | * 200.0   | 424.0                       | 208.5 | 424.0 | * *    | 9.             | 90. AG            | 223. | 100.0        | .0        | 12.0      | .08 | .4             |
| 3. Station EB TR     | * 200.0   | 412.0                       | 225.8 | 412.0 | * *    | 26.            | 90. AG            | 223. | 100.0        | .0        | 12.0      | .25 | 1.3            |
| 4. Whisconier EB out | * 454.0   | 418.0                       | 848.0 | 418.0 | * *    | 394.           | 90. AG            | 161. | 8.3          | .0        | 24.0      |     |                |
| 5. Whisconier WB in  | * 848.0   | 442.0                       | 648.0 | 442.0 | * *    | 200.           | 270. AG           | 774. | 8.3          | .0        | 24.0      |     |                |
| 6. Whisconier WB LT  | * 648.0   | 436.0                       | 531.8 | 436.0 | * *    | 116.           | 270. AG           | 172. | 100.0        | .0        | 12.0      | .91 | 5.9            |
| 7. Whisconier WB R   | * 648.0   | 448.0                       | 606.5 | 448.0 | * *    | 42.            | 270. AG           | 126. | 100.0        | .0        | 12.0      | .43 | 2.1            |
| 8. Station WB out    | * 406.0   | 442.0                       | .0    | 442.0 | * *    | 406.           | 270. AG           | 774. | 8.3          | .0        | 24.0      |     |                |
| 9. Federal NB in     | * 442.0   | .0                          | 442.0 | 200.0 | * *    | 200.           | 360. AG           | 345. | 8.3          | .0        | 12.0      |     |                |
| 10. Federal NB LTR   | * 442.0   | 200.0                       | 442.0 | 260.4 | * *    | 60.            | 360. AG           | 183. | 100.0        | .0        | 12.0      | .55 | 3.1            |
| 11. Federal NB out   | * 442.0   | 454.0                       | 442.0 | 836.0 | * *    | 382.           | 360. AG           | 345. | 8.3          | .0        | 24.0      |     |                |
| 12. Federal SB in    | * 418.0   | 836.0                       | 418.0 | 636.0 | * *    | 200.           | 180. AG           | 484. | 8.3          | .0        | 24.0      |     |                |
| 13. Federal SB L     | * 424.0   | 636.0                       | 424.0 | 601.0 | * *    | 35.            | 180. AG           | 183. | 100.0        | .0        | 12.0      | .35 | 1.8            |
| 14. Federal SB TR    | * 412.0   | 636.0                       | 412.0 | 589.4 | * *    | 47.            | 180. AG           | 172. | 100.0        | .0        | 12.0      | .42 | 2.4            |
| 15. Federal SB out   | * 424.0   | 404.0                       | 424.0 | .0    | * *    | 404.           | 180. AG           | 484. | 8.3          | .0        | 24.0      |     |                |

DATE : 4/15/11  
 TIME : 13:11:35

-----  
 ADDITIONAL QUEUE LINK PARAMETERS  
 -----

| LINK DESCRIPTION    | *<br>* | CYCLE<br>LENGTH<br>(SEC) | RED<br>TIME<br>(SEC) | CLEARANCE<br>LOST TIME<br>(SEC) | APPROACH<br>VOL<br>(VPH) | SATURATION<br>FLOW RATE<br>(VPH) | IDLE<br>EM FAC<br>(gm/hr) | SIGNAL<br>TYPE | ARRIVAL<br>RATE |
|---------------------|--------|--------------------------|----------------------|---------------------------------|--------------------------|----------------------------------|---------------------------|----------------|-----------------|
| 2. Station EB L     | *<br>* | 60                       | 39                   | 4.0                             | 40                       | 1926                             | 127.94                    | 3              | 3               |
| 3. Station EB TR    | *<br>* | 60                       | 39                   | 4.0                             | 121                      | 1946                             | 127.94                    | 3              | 3               |
| 6. Whisconier WB LT | *<br>* | 60                       | 30                   | 4.0                             | 429                      | 1174                             | 127.94                    | 3              | 3               |
| 7. Whisconier WB R  | *<br>* | 60                       | 22                   | 4.0                             | 345                      | 1515                             | 127.94                    | 3              | 3               |
| 10. Federal NB LTR  | *<br>* | 60                       | 32                   | 5.0                             | 345                      | 1778                             | 127.94                    | 3              | 3               |
| 13. Federal SB L    | *<br>* | 60                       | 32                   | 3.0                             | 200                      | 1475                             | 127.94                    | 3              | 3               |
| 14. Federal SB TR   | *<br>* | 60                       | 30                   | 5.0                             | 284                      | 1755                             | 127.94                    | 3              | 3               |

-----  
 RECEPTOR LOCATIONS  
 -----

| RECEPTOR          | *<br>* | COORDINATES (FT) |       |     | *<br>* |
|-------------------|--------|------------------|-------|-----|--------|
|                   |        | X                | Y     | Z   |        |
| 1. EB W Midblock  | *<br>* | 196.0            | 390.0 | 6.0 | *<br>* |
| 2. SW Corner      | *<br>* | 394.0            | 390.0 | 6.0 | *<br>* |
| 3. SB S Midblock  | *<br>* | 394.0            | 200.0 | 6.0 | *<br>* |
| 4. NB S Midblock  | *<br>* | 464.0            | 200.0 | 6.0 | *<br>* |
| 5. SE Corner      | *<br>* | 464.0            | 390.0 | 6.0 | *<br>* |
| 6. EB E Midblock  | *<br>* | 648.0            | 390.0 | 6.0 | *<br>* |
| 7. WB E Midblock  | *<br>* | 648.0            | 464.0 | 6.0 | *<br>* |
| 8. NE Corner      | *<br>* | 464.0            | 464.0 | 6.0 | *<br>* |
| 9. NB N Midblock  | *<br>* | 464.0            | 640.0 | 6.0 | *<br>* |
| 10. SB N Midblock | *<br>* | 396.0            | 640.0 | 6.0 | *<br>* |
| 11. NW Corner     | *<br>* | 396.0            | 464.0 | 6.0 | *<br>* |
| 12. WB W Midblock | *<br>* | 196.0            | 464.0 | 6.0 | *<br>* |

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

| WIND ANGLE (DEGR)* | REC1 | REC2 | REC3 | REC4 | REC5 | REC6 | REC7 | REC8 | REC9 | REC10 | REC11 | REC12 |
|--------------------|------|------|------|------|------|------|------|------|------|-------|-------|-------|
| 0.                 | 4.6  | 4.4  | 4.4  | 4.4  | 4.4  | 4.6  | 4.3  | 4.4  | 4.4  | 4.4   | 4.4   | 4.3   |
| 10.                | 4.7  | 4.5  | 4.4  | 4.3  | 4.3  | 4.5  | 4.3  | 4.3  | 4.3  | 4.4   | 4.5   | 4.3   |
| 20.                | 4.8  | 4.4  | 4.4  | 4.4  | 4.3  | 4.4  | 4.3  | 4.3  | 4.3  | 4.6   | 4.4   | 4.3   |
| 30.                | 4.9  | 4.3  | 4.5  | 4.4  | 4.3  | 4.4  | 4.3  | 4.3  | 4.3  | 4.5   | 4.4   | 4.3   |
| 40.                | 4.8  | 4.3  | 4.6  | 4.3  | 4.3  | 4.4  | 4.3  | 4.3  | 4.3  | 4.5   | 4.4   | 4.3   |
| 50.                | 4.7  | 4.3  | 4.6  | 4.3  | 4.4  | 4.4  | 4.3  | 4.3  | 4.3  | 4.5   | 4.4   | 4.3   |
| 60.                | 4.6  | 4.4  | 4.6  | 4.3  | 4.5  | 4.4  | 4.3  | 4.3  | 4.3  | 4.5   | 4.4   | 4.3   |
| 70.                | 4.5  | 4.5  | 4.6  | 4.3  | 4.5  | 4.4  | 4.3  | 4.3  | 4.3  | 4.5   | 4.4   | 4.3   |
| 80.                | 4.4  | 4.5  | 4.6  | 4.3  | 4.4  | 4.4  | 4.4  | 4.4  | 4.3  | 4.6   | 4.3   | 4.4   |
| 90.                | 4.3  | 4.5  | 4.5  | 4.3  | 4.4  | 4.3  | 4.4  | 4.4  | 4.3  | 4.7   | 4.4   | 4.4   |
| 100.               | 4.3  | 4.4  | 4.5  | 4.3  | 4.3  | 4.3  | 4.5  | 4.5  | 4.3  | 4.9   | 4.4   | 4.5   |
| 110.               | 4.3  | 4.4  | 4.4  | 4.3  | 4.3  | 4.3  | 4.5  | 4.5  | 4.3  | 5.0   | 4.4   | 4.5   |
| 120.               | 4.3  | 4.4  | 4.4  | 4.3  | 4.3  | 4.3  | 4.5  | 4.4  | 4.3  | 5.1   | 4.3   | 4.5   |
| 130.               | 4.3  | 4.4  | 4.4  | 4.3  | 4.3  | 4.3  | 4.5  | 4.4  | 4.3  | 5.2   | 4.3   | 4.5   |
| 140.               | 4.3  | 4.4  | 4.4  | 4.3  | 4.3  | 4.3  | 4.5  | 4.3  | 4.4  | 5.2   | 4.3   | 4.6   |
| 150.               | 4.3  | 4.4  | 4.4  | 4.3  | 4.3  | 4.3  | 4.5  | 4.3  | 4.4  | 5.0   | 4.4   | 4.7   |
| 160.               | 4.3  | 4.5  | 4.4  | 4.3  | 4.3  | 4.3  | 4.6  | 4.3  | 4.4  | 4.9   | 4.5   | 4.8   |
| 170.               | 4.3  | 4.5  | 4.4  | 4.3  | 4.3  | 4.3  | 4.6  | 4.3  | 4.3  | 4.5   | 4.5   | 4.8   |
| 180.               | 4.3  | 4.4  | 4.4  | 4.3  | 4.5  | 4.3  | 4.8  | 4.4  | 4.4  | 4.4   | 4.6   | 4.7   |
| 190.               | 4.3  | 4.3  | 4.3  | 4.5  | 4.5  | 4.3  | 4.8  | 4.4  | 4.4  | 4.3   | 4.5   | 4.6   |
| 200.               | 4.3  | 4.3  | 4.3  | 4.5  | 4.5  | 4.3  | 4.9  | 4.4  | 4.4  | 4.3   | 4.5   | 4.5   |
| 210.               | 4.3  | 4.3  | 4.3  | 4.5  | 4.4  | 4.3  | 4.9  | 4.4  | 4.5  | 4.3   | 4.5   | 4.5   |
| 220.               | 4.3  | 4.3  | 4.3  | 4.5  | 4.4  | 4.3  | 5.0  | 4.3  | 4.6  | 4.3   | 4.5   | 4.5   |
| 230.               | 4.3  | 4.3  | 4.3  | 4.5  | 4.4  | 4.3  | 5.0  | 4.3  | 4.9  | 4.3   | 4.5   | 4.5   |
| 240.               | 4.3  | 4.3  | 4.3  | 4.5  | 4.4  | 4.3  | 5.0  | 4.4  | 4.8  | 4.3   | 4.5   | 4.5   |
| 250.               | 4.3  | 4.3  | 4.3  | 4.6  | 4.4  | 4.3  | 4.8  | 4.4  | 4.8  | 4.3   | 4.6   | 4.5   |
| 260.               | 4.3  | 4.3  | 4.3  | 4.5  | 4.4  | 4.3  | 4.6  | 4.6  | 4.7  | 4.3   | 4.5   | 4.5   |
| 270.               | 4.3  | 4.4  | 4.3  | 4.6  | 4.5  | 4.3  | 4.6  | 4.5  | 4.6  | 4.3   | 4.5   | 4.4   |
| 280.               | 4.4  | 4.4  | 4.3  | 4.7  | 4.5  | 4.5  | 4.3  | 4.5  | 4.5  | 4.3   | 4.4   | 4.4   |
| 290.               | 4.4  | 4.4  | 4.3  | 4.7  | 4.4  | 4.5  | 4.3  | 4.4  | 4.5  | 4.3   | 4.3   | 4.3   |
| 300.               | 4.4  | 4.4  | 4.3  | 4.8  | 4.4  | 4.5  | 4.3  | 4.4  | 4.5  | 4.3   | 4.3   | 4.3   |
| 310.               | 4.4  | 4.4  | 4.3  | 4.8  | 4.4  | 4.6  | 4.3  | 4.4  | 4.5  | 4.3   | 4.3   | 4.3   |
| 320.               | 4.4  | 4.4  | 4.3  | 4.8  | 4.3  | 4.7  | 4.3  | 4.4  | 4.5  | 4.3   | 4.3   | 4.3   |
| 330.               | 4.4  | 4.4  | 4.3  | 4.8  | 4.3  | 4.6  | 4.3  | 4.4  | 4.5  | 4.3   | 4.3   | 4.3   |
| 340.               | 4.4  | 4.4  | 4.3  | 4.7  | 4.4  | 4.6  | 4.3  | 4.5  | 4.5  | 4.3   | 4.3   | 4.3   |
| 350.               | 4.6  | 4.4  | 4.3  | 4.6  | 4.4  | 4.6  | 4.3  | 4.4  | 4.4  | 4.3   | 4.3   | 4.3   |
| 360.               | 4.6  | 4.4  | 4.4  | 4.4  | 4.4  | 4.6  | 4.3  | 4.4  | 4.4  | 4.4   | 4.4   | 4.3   |
| MAX                | 4.9  | 4.5  | 4.6  | 4.8  | 4.5  | 4.7  | 5.0  | 4.6  | 4.9  | 5.2   | 4.6   | 4.8   |
| DEGR.              | 30   | 10   | 40   | 300  | 60   | 320  | 220  | 260  | 230  | 130   | 180   | 160   |

THE HIGHEST CONCENTRATION OF 5.20 PPM OCCURRED AT RECEPTOR REC10.





JOB: FederalStation2030MitigatedBuildPM

RUN: FederalStation2030MitigatedBuildPM

DATE : 4/15/11  
 TIME : 13:13:43

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S      VD = .0 CM/S      Z0 = 175. CM  
 U = 1.0 M/S      CLAS = 4 (D)      ATIM = 60. MINUTES      MIXH = 1000. M      AMB = 4.3 PPM

LINK VARIABLES

| LINK DESCRIPTION     | *<br>* X1 | LINK COORDINATES (FT)<br>Y1 | X2    | Y2     | *<br>* | LENGTH<br>(FT) | BRG TYPE<br>(DEG) | VPH  | EF<br>(G/MI) | H<br>(FT) | W<br>(FT) | V/C  | QUEUE<br>(VEH) |
|----------------------|-----------|-----------------------------|-------|--------|--------|----------------|-------------------|------|--------------|-----------|-----------|------|----------------|
| 1. Station EB in     | * .0      | 418.0                       | 200.0 | 418.0  | * *    | 200.           | 90. AG            | 139. | 8.3          | .0        | 24.0      |      |                |
| 2. Station EB L      | * 200.0   | 424.0                       | 206.7 | 424.0  | * *    | 7.             | 90. AG            | 240. | 100.0        | .0        | 12.0      | .09  | .3             |
| 3. Station EB TR     | * 200.0   | 412.0                       | 225.3 | 412.0  | * *    | 25.            | 90. AG            | 240. | 100.0        | .0        | 12.0      | .32  | 1.3            |
| 4. Whisconier EB out | * 454.0   | 418.0                       | 848.0 | 418.0  | * *    | 394.           | 90. AG            | 139. | 8.3          | .0        | 24.0      |      |                |
| 5. Whisconier WB in  | * 848.0   | 442.0                       | 648.0 | 442.0  | * *    | 200.           | 270. AG           | 740. | 8.3          | .0        | 24.0      |      |                |
| 6. Whisconier WB LT  | * 648.0   | 436.0                       | 558.8 | 436.0  | * *    | 89.            | 270. AG           | 189. | 100.0        | .0        | 12.0      | .84  | 4.5            |
| 7. Whisconier WB R   | * 648.0   | 448.0                       | 599.5 | 448.0  | * *    | 49.            | 270. AG           | 143. | 100.0        | .0        | 12.0      | .48  | 2.5            |
| 8. Station WB out    | * 406.0   | 442.0                       | .0    | 442.0  | * *    | 406.           | 270. AG           | 740. | 8.3          | .0        | 24.0      |      |                |
| 9. Federal NB in     | * 442.0   | .0                          | 442.0 | 200.0  | * *    | 200.           | 360. AG           | 767. | 8.3          | .0        | 12.0      |      |                |
| 10. Federal NB LTR   | * 442.0   | 200.0                       | 442.0 | 1290.4 | * *    | 1090.          | 360. AG           | 177. | 100.0        | .0        | 12.0      | 1.12 | 55.4           |
| 11. Federal NB out   | * 442.0   | 454.0                       | 442.0 | 836.0  | * *    | 382.           | 360. AG           | 767. | 8.3          | .0        | 24.0      |      |                |
| 12. Federal SB in    | * 418.0   | 836.0                       | 418.0 | 636.0  | * *    | 200.           | 180. AG           | 735. | 8.3          | .0        | 24.0      |      |                |
| 13. Federal SB L     | * 424.0   | 636.0                       | 424.0 | 579.7  | * *    | 56.            | 180. AG           | 166. | 100.0        | .0        | 12.0      | .47  | 2.9            |
| 14. Federal SB TR    | * 412.0   | 636.0                       | 412.0 | 579.9  | * *    | 56.            | 180. AG           | 154. | 100.0        | .0        | 12.0      | .51  | 2.9            |
| 15. Federal SB out   | * 424.0   | 404.0                       | 424.0 | .0     | * *    | 404.           | 180. AG           | 735. | 8.3          | .0        | 24.0      |      |                |

DATE : 4/15/11  
 TIME : 13:13:43

-----  
 ADDITIONAL QUEUE LINK PARAMETERS  
 -----

| LINK DESCRIPTION    | *<br>* | CYCLE<br>LENGTH<br>(SEC) | RED<br>TIME<br>(SEC) | CLEARANCE<br>LOST TIME<br>(SEC) | APPROACH<br>VOL<br>(VPH) | SATURATION<br>FLOW RATE<br>(VPH) | IDLE<br>EM FAC<br>(gm/hr) | SIGNAL<br>TYPE | ARRIVAL<br>RATE |
|---------------------|--------|--------------------------|----------------------|---------------------------------|--------------------------|----------------------------------|---------------------------|----------------|-----------------|
| 2. Station EB L     | *<br>* | 60                       | 42                   | 4.0                             | 29                       | 1689                             | 127.94                    | 3              | 3               |
| 3. Station EB TR    | *<br>* | 60                       | 42                   | 4.0                             | 110                      | 1709                             | 127.94                    | 3              | 3               |
| 6. Whisconier WB LT | *<br>* | 60                       | 33                   | 4.0                             | 385                      | 1316                             | 127.94                    | 3              | 3               |
| 7. Whisconier WB R  | *<br>* | 60                       | 25                   | 4.0                             | 355                      | 1515                             | 127.94                    | 3              | 3               |
| 10. Federal NB LTR  | *<br>* | 60                       | 31                   | 5.0                             | 767                      | 1867                             | 127.94                    | 3              | 3               |
| 13. Federal SB L    | *<br>* | 60                       | 29                   | 3.0                             | 355                      | 1727                             | 127.94                    | 3              | 3               |
| 14. Federal SB TR   | *<br>* | 60                       | 27                   | 5.0                             | 380                      | 1728                             | 127.94                    | 3              | 3               |

-----  
 RECEPTOR LOCATIONS  
 -----

| RECEPTOR          | *<br>* | X     | COORDINATES (FT)<br>Y | Z   | *<br>* |
|-------------------|--------|-------|-----------------------|-----|--------|
| 1. EB W Midblock  | *<br>* | 196.0 | 390.0                 | 6.0 | *<br>* |
| 2. SW Corner      | *<br>* | 394.0 | 390.0                 | 6.0 | *<br>* |
| 3. SB S Midblock  | *<br>* | 394.0 | 200.0                 | 6.0 | *<br>* |
| 4. NB S Midblock  | *<br>* | 464.0 | 200.0                 | 6.0 | *<br>* |
| 5. SE Corner      | *<br>* | 464.0 | 390.0                 | 6.0 | *<br>* |
| 6. EB E Midblock  | *<br>* | 648.0 | 390.0                 | 6.0 | *<br>* |
| 7. WB E Midblock  | *<br>* | 648.0 | 464.0                 | 6.0 | *<br>* |
| 8. NE Corner      | *<br>* | 464.0 | 464.0                 | 6.0 | *<br>* |
| 9. NB N Midblock  | *<br>* | 464.0 | 640.0                 | 6.0 | *<br>* |
| 10. SB N Midblock | *<br>* | 396.0 | 640.0                 | 6.0 | *<br>* |
| 11. NW Corner     | *<br>* | 396.0 | 464.0                 | 6.0 | *<br>* |
| 12. WB W Midblock | *<br>* | 196.0 | 464.0                 | 6.0 | *<br>* |

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

| WIND ANGLE (DEGR)* | REC1 | REC2 | REC3 | REC4 | REC5 | REC6 | REC7 | REC8 | REC9 | REC10 | REC11 | REC12 |
|--------------------|------|------|------|------|------|------|------|------|------|-------|-------|-------|
| 0.                 | 4.7  | 4.7  | 4.6  | 4.8  | 4.8  | 4.6  | 4.3  | 4.9  | 4.8  | 4.6   | 4.8   | 4.3   |
| 10.                | 4.8  | 4.8  | 4.7  | 4.5  | 4.6  | 4.5  | 4.3  | 4.6  | 4.6  | 4.9   | 4.9   | 4.3   |
| 20.                | 5.0  | 4.8  | 4.9  | 4.4  | 4.4  | 4.4  | 4.3  | 4.4  | 4.4  | 5.0   | 4.9   | 4.4   |
| 30.                | 5.0  | 4.7  | 4.8  | 4.3  | 4.3  | 4.4  | 4.3  | 4.3  | 4.3  | 4.9   | 4.7   | 4.4   |
| 40.                | 4.9  | 4.7  | 4.8  | 4.3  | 4.3  | 4.4  | 4.3  | 4.3  | 4.3  | 4.9   | 4.7   | 4.4   |
| 50.                | 4.8  | 4.6  | 4.8  | 4.3  | 4.4  | 4.4  | 4.3  | 4.3  | 4.3  | 4.9   | 4.7   | 4.4   |
| 60.                | 4.7  | 4.7  | 4.8  | 4.3  | 4.4  | 4.4  | 4.3  | 4.3  | 4.3  | 4.9   | 4.7   | 4.4   |
| 70.                | 4.6  | 4.7  | 4.7  | 4.3  | 4.4  | 4.4  | 4.3  | 4.3  | 4.3  | 4.9   | 4.7   | 4.4   |
| 80.                | 4.5  | 4.7  | 4.6  | 4.3  | 4.4  | 4.4  | 4.4  | 4.3  | 4.3  | 4.8   | 4.7   | 4.5   |
| 90.                | 4.4  | 4.7  | 4.5  | 4.3  | 4.4  | 4.3  | 4.4  | 4.4  | 4.3  | 5.0   | 4.8   | 4.5   |
| 100.               | 4.4  | 4.6  | 4.6  | 4.3  | 4.3  | 4.3  | 4.5  | 4.4  | 4.3  | 5.2   | 4.8   | 4.6   |
| 110.               | 4.4  | 4.7  | 4.6  | 4.3  | 4.3  | 4.3  | 4.5  | 4.4  | 4.3  | 5.3   | 4.7   | 4.6   |
| 120.               | 4.4  | 4.8  | 4.6  | 4.3  | 4.3  | 4.3  | 4.5  | 4.4  | 4.3  | 5.3   | 4.6   | 4.6   |
| 130.               | 4.3  | 4.8  | 4.6  | 4.3  | 4.3  | 4.3  | 4.5  | 4.3  | 4.3  | 5.4   | 4.6   | 4.6   |
| 140.               | 4.3  | 4.8  | 4.6  | 4.3  | 4.3  | 4.3  | 4.5  | 4.3  | 4.4  | 5.4   | 4.6   | 4.6   |
| 150.               | 4.3  | 4.8  | 4.6  | 4.3  | 4.3  | 4.3  | 4.5  | 4.3  | 4.4  | 5.4   | 4.8   | 4.6   |
| 160.               | 4.3  | 4.7  | 4.6  | 4.3  | 4.3  | 4.3  | 4.6  | 4.3  | 4.3  | 5.3   | 4.8   | 4.8   |
| 170.               | 4.3  | 4.6  | 4.5  | 4.3  | 4.4  | 4.3  | 4.6  | 4.4  | 4.6  | 5.1   | 4.7   | 4.8   |
| 180.               | 4.3  | 4.5  | 4.4  | 4.4  | 4.7  | 4.3  | 4.8  | 4.7  | 4.8  | 4.7   | 4.7   | 4.7   |
| 190.               | 4.3  | 4.3  | 4.3  | 4.6  | 4.8  | 4.3  | 5.0  | 4.9  | 5.1  | 4.5   | 4.6   | 4.6   |
| 200.               | 4.3  | 4.3  | 4.3  | 4.6  | 5.0  | 4.3  | 4.9  | 4.9  | 5.2  | 4.3   | 4.5   | 4.5   |
| 210.               | 4.3  | 4.3  | 4.3  | 4.6  | 5.0  | 4.3  | 5.1  | 4.9  | 5.2  | 4.3   | 4.5   | 4.5   |
| 220.               | 4.3  | 4.3  | 4.3  | 4.6  | 4.9  | 4.3  | 5.2  | 4.9  | 5.3  | 4.3   | 4.5   | 4.5   |
| 230.               | 4.3  | 4.3  | 4.3  | 4.6  | 4.8  | 4.4  | 5.2  | 4.7  | 5.3  | 4.3   | 4.5   | 4.5   |
| 240.               | 4.3  | 4.3  | 4.3  | 4.5  | 4.8  | 4.4  | 5.2  | 4.9  | 5.3  | 4.3   | 4.5   | 4.5   |
| 250.               | 4.3  | 4.3  | 4.3  | 4.6  | 4.8  | 4.4  | 5.0  | 4.9  | 5.3  | 4.3   | 4.6   | 4.5   |
| 260.               | 4.3  | 4.3  | 4.3  | 4.6  | 4.8  | 4.4  | 4.8  | 5.0  | 5.2  | 4.3   | 4.5   | 4.5   |
| 270.               | 4.3  | 4.4  | 4.3  | 4.7  | 4.9  | 4.4  | 4.7  | 5.0  | 5.2  | 4.3   | 4.5   | 4.4   |
| 280.               | 4.4  | 4.4  | 4.3  | 4.7  | 4.9  | 4.5  | 4.4  | 5.0  | 5.0  | 4.3   | 4.4   | 4.4   |
| 290.               | 4.4  | 4.4  | 4.3  | 4.7  | 4.9  | 4.5  | 4.4  | 4.9  | 5.0  | 4.3   | 4.3   | 4.3   |
| 300.               | 4.4  | 4.4  | 4.3  | 4.8  | 4.8  | 4.6  | 4.4  | 4.9  | 5.0  | 4.3   | 4.3   | 4.3   |
| 310.               | 4.4  | 4.4  | 4.3  | 4.8  | 4.8  | 4.8  | 4.4  | 4.9  | 5.0  | 4.3   | 4.3   | 4.3   |
| 320.               | 4.4  | 4.4  | 4.3  | 4.9  | 4.8  | 4.8  | 4.4  | 5.0  | 5.1  | 4.3   | 4.3   | 4.3   |
| 330.               | 4.4  | 4.4  | 4.3  | 4.9  | 4.9  | 4.8  | 4.4  | 5.1  | 5.1  | 4.3   | 4.3   | 4.3   |
| 340.               | 4.4  | 4.4  | 4.3  | 5.0  | 5.0  | 4.7  | 4.4  | 5.4  | 5.2  | 4.3   | 4.3   | 4.3   |
| 350.               | 4.5  | 4.5  | 4.4  | 5.0  | 5.1  | 4.7  | 4.4  | 5.3  | 5.2  | 4.5   | 4.4   | 4.3   |
| 360.               | 4.7  | 4.7  | 4.6  | 4.8  | 4.8  | 4.6  | 4.3  | 4.9  | 4.8  | 4.6   | 4.8   | 4.3   |
| MAX                | 5.0  | 4.8  | 4.9  | 5.0  | 5.1  | 4.8  | 5.2  | 5.4  | 5.3  | 5.4   | 4.9   | 4.8   |
| DEGR.              | 20   | 10   | 20   | 340  | 350  | 310  | 220  | 340  | 220  | 130   | 10    | 160   |

THE HIGHEST CONCENTRATION OF 5.40 PPM OCCURRED AT RECEPTOR REC10.



JOB: GristMillGlover2010ExistingAM

RUN: GristMillGlover2010ExistingAM

DATE : 4/ 7/11  
 TIME : 15: 8:43

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S      VD = .0 CM/S      Z0 = 175. CM  
 U = 1.0 M/S      CLAS = 4 (D)      ATIM = 60. MINUTES      MIXH = 1000. M      AMB = 4.3 PPM

LINK VARIABLES

| LINK DESCRIPTION     | *<br>*<br>* | X1    | LINK COORDINATES (FT)<br>Y1 | X2    | Y2    | *<br>*<br>* | LENGTH<br>(FT) | BRG TYPE<br>(DEG) | VPH   | EF<br>(G/MI) | H<br>(FT) | W<br>(FT) | V/C | QUEUE<br>(VEH) |
|----------------------|-------------|-------|-----------------------------|-------|-------|-------------|----------------|-------------------|-------|--------------|-----------|-----------|-----|----------------|
| 1. Grist Mill EB in  | *<br>*<br>* | .0    | 418.0                       | 200.0 | 418.0 | *<br>*<br>* | 200.           | 90. AG            | 2153. | 11.2         | .0        | 36.0      |     |                |
| 2. Grist Mill EB T   | *<br>*<br>* | 200.0 | 424.0                       | 379.3 | 424.0 | *<br>*<br>* | 179.           | 90. AG            | 313.  | 100.0        | .0        | 24.0      | .43 | 9.1            |
| 3. Grist Mill EB R   | *<br>*<br>* | 200.0 | 406.0                       | 249.9 | 406.0 | *<br>*<br>* | 50.            | 90. AG            | 102.  | 100.0        | .0        | 12.0      | .33 | 2.5            |
| 4. Grist Mill EB out | *<br>*<br>* | 454.0 | 412.0                       | 848.0 | 412.0 | *<br>*<br>* | 394.           | 90. AG            | 2153. | 11.2         | .0        | 24.0      |     |                |
| 5. Grist Mill WB in  | *<br>*<br>* | 848.0 | 442.0                       | 648.0 | 442.0 | *<br>*<br>* | 200.           | 270. AG           | 1324. | 11.2         | .0        | 36.0      |     |                |
| 6. Grist Mill WB L   | *<br>*<br>* | 648.0 | 430.0                       | 620.3 | 430.0 | *<br>*<br>* | 28.            | 270. AG           | 364.  | 100.0        | .0        | 12.0      | .20 | 1.4            |
| 7. Grist Mill WB T   | *<br>*<br>* | 648.0 | 448.0                       | 603.1 | 448.0 | *<br>*<br>* | 45.            | 270. AG           | 110.  | 100.0        | .0        | 24.0      | .23 | 2.3            |
| 8. Grist Mill WB out | *<br>*<br>* | 406.0 | 448.0                       | .0    | 448.0 | *<br>*<br>* | 406.           | 270. AG           | 1324. | 11.2         | .0        | 24.0      |     |                |
| 9. Glover NB in      | *<br>*<br>* | 442.0 | .0                          | 442.0 | 196.0 | *<br>*<br>* | 196.           | 360. AG           | 115.  | 11.2         | .0        | 24.0      |     |                |
| 10. Glover NB L      | *<br>*<br>* | 436.0 | 196.0                       | 436.0 | 242.5 | *<br>*<br>* | 47.            | 360. AG           | 411.  | 100.0        | .0        | 12.0      | .60 | 2.4            |
| 11. Glover NB LR     | *<br>*<br>* | 448.0 | 196.0                       | 448.0 | 217.3 | *<br>*<br>* | 21.            | 360. AG           | 411.  | 100.0        | .0        | 12.0      | .71 | 1.1            |
| 12. Glover SB out    | *<br>*<br>* | 418.0 | 400.0                       | 418.0 | .0    | *<br>*<br>* | 400.           | 180. AG           | 115.  | 11.2         | .0        | 24.0      |     |                |

DATE : 4/ 7/11  
 TIME : 15: 8:43

-----  
 ADDITIONAL QUEUE LINK PARAMETERS  
 -----

| LINK DESCRIPTION   | *<br>* | CYCLE<br>LENGTH<br>(SEC) | RED<br>TIME<br>(SEC) | CLEARANCE<br>LOST TIME<br>(SEC) | APPROACH<br>VOL<br>(VPH) | SATURATION<br>FLOW RATE<br>(VPH) | IDLE<br>EM FAC<br>(gm/hr) | SIGNAL<br>TYPE | ARRIVAL<br>RATE |
|--------------------|--------|--------------------------|----------------------|---------------------------------|--------------------------|----------------------------------|---------------------------|----------------|-----------------|
| 2. Grist Mill EB T | *      | 110                      | 37                   | 5.0                             | 1773                     | 3450                             | 173.64                    | 3              | 4               |
| 3. Grist Mill EB R | *      | 110                      | 24                   | 5.0                             | 380                      | 1584                             | 173.64                    | 3              | 4               |
| 6. Grist Mill WB L | *      | 110                      | 86                   | 3.0                             | 59                       | 1702                             | 173.64                    | 3              | 4               |
| 7. Grist Mill WB T | *      | 110                      | 13                   | 5.0                             | 1265                     | 3403                             | 173.64                    | 3              | 4               |
| 10. Glover NB L    | *      | 110                      | 97                   | 5.0                             | 85                       | 2610                             | 173.64                    | 3              | 3               |
| 11. Glover NB LR   | *      | 110                      | 97                   | 5.0                             | 30                       | 776                              | 173.64                    | 3              | 3               |

-----  
 RECEPTOR LOCATIONS  
 -----

| RECEPTOR          | *<br>* | X     | COORDINATES (FT)<br>Y | Z   | *<br>* |
|-------------------|--------|-------|-----------------------|-----|--------|
| 1. EB W Midblock  | *      | 196.0 | 390.0                 | 6.0 | *      |
| 2. SW Corner      | *      | 394.0 | 390.0                 | 6.0 | *      |
| 3. SB S Midblock  | *      | 394.0 | 200.0                 | 6.0 | *      |
| 4. NB S Midblock  | *      | 464.0 | 200.0                 | 6.0 | *      |
| 5. SE Corner      | *      | 464.0 | 390.0                 | 6.0 | *      |
| 6. EB E Midblock  | *      | 648.0 | 390.0                 | 6.0 | *      |
| 7. WB E Midblock  | *      | 648.0 | 470.0                 | 6.0 | *      |
| 8. NE Corner      | *      | 464.0 | 470.0                 | 6.0 | *      |
| 9. NW Corner      | *      | 396.0 | 470.0                 | 6.0 | *      |
| 10. WB W Midblock | *      | 196.0 | 470.0                 | 6.0 | *      |

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

| WIND ANGLE (DEGR) | REC1 | REC2 | REC3 | REC4 | REC5 | REC6 | REC7 | REC8 | REC9 | REC10 |
|-------------------|------|------|------|------|------|------|------|------|------|-------|
| 0.                | 5.3  | 4.6  | 4.5  | 4.4  | 4.9  | 5.5  | 4.3  | 4.3  | 4.3  | 4.3   |
| 10.               | 5.3  | 4.4  | 4.4  | 4.4  | 5.0  | 5.4  | 4.3  | 4.3  | 4.3  | 4.3   |
| 20.               | 5.4  | 4.4  | 4.4  | 4.5  | 5.0  | 5.4  | 4.3  | 4.3  | 4.3  | 4.3   |
| 30.               | 5.4  | 4.3  | 4.6  | 4.5  | 5.0  | 5.3  | 4.3  | 4.3  | 4.3  | 4.3   |
| 40.               | 5.7  | 4.3  | 4.8  | 4.6  | 5.1  | 5.4  | 4.3  | 4.3  | 4.3  | 4.3   |
| 50.               | 5.7  | 4.4  | 5.0  | 4.6  | 5.1  | 5.4  | 4.3  | 4.3  | 4.3  | 4.3   |
| 60.               | 5.7  | 4.5  | 5.1  | 4.5  | 5.2  | 5.5  | 4.3  | 4.3  | 4.3  | 4.3   |
| 70.               | 5.6  | 4.9  | 5.2  | 4.4  | 5.5  | 5.5  | 4.3  | 4.3  | 4.3  | 4.3   |
| 80.               | 5.4  | 5.0  | 5.1  | 4.3  | 5.4  | 5.3  | 4.4  | 4.5  | 4.4  | 4.5   |
| 90.               | 5.0  | 4.9  | 5.0  | 4.3  | 5.0  | 4.9  | 4.7  | 4.6  | 4.6  | 4.9   |
| 100.              | 4.5  | 4.6  | 4.7  | 4.3  | 4.6  | 4.5  | 5.0  | 4.8  | 4.8  | 5.4   |
| 110.              | 4.3  | 4.4  | 4.5  | 4.3  | 4.4  | 4.4  | 5.2  | 5.0  | 4.8  | 5.6   |
| 120.              | 4.3  | 4.3  | 4.3  | 4.3  | 4.3  | 4.3  | 5.2  | 4.8  | 4.7  | 5.6   |
| 130.              | 4.4  | 4.3  | 4.3  | 4.3  | 4.3  | 4.3  | 5.2  | 4.8  | 4.7  | 5.5   |
| 140.              | 4.3  | 4.3  | 4.3  | 4.3  | 4.3  | 4.3  | 5.2  | 4.7  | 4.6  | 5.5   |
| 150.              | 4.3  | 4.4  | 4.3  | 4.3  | 4.3  | 4.3  | 5.1  | 4.7  | 4.6  | 5.4   |
| 160.              | 4.3  | 4.4  | 4.3  | 4.3  | 4.3  | 4.3  | 5.2  | 4.7  | 4.5  | 5.4   |
| 170.              | 4.3  | 4.4  | 4.3  | 4.3  | 4.3  | 4.3  | 5.3  | 4.6  | 4.7  | 5.4   |
| 180.              | 4.3  | 4.4  | 4.3  | 4.3  | 4.4  | 4.3  | 5.4  | 4.7  | 4.9  | 5.2   |
| 190.              | 4.3  | 4.3  | 4.3  | 4.3  | 4.4  | 4.3  | 5.4  | 4.6  | 4.9  | 5.2   |
| 200.              | 4.3  | 4.3  | 4.3  | 4.3  | 4.4  | 4.3  | 5.5  | 4.4  | 5.0  | 5.2   |
| 210.              | 4.3  | 4.3  | 4.3  | 4.3  | 4.3  | 4.3  | 5.3  | 4.3  | 5.1  | 5.2   |
| 220.              | 4.3  | 4.3  | 4.3  | 4.3  | 4.3  | 4.3  | 5.2  | 4.4  | 5.4  | 5.3   |
| 230.              | 4.3  | 4.3  | 4.3  | 4.4  | 4.3  | 4.4  | 5.1  | 4.6  | 5.4  | 5.3   |
| 240.              | 4.3  | 4.3  | 4.3  | 4.6  | 4.3  | 4.3  | 5.0  | 4.8  | 5.7  | 5.4   |
| 250.              | 4.4  | 4.3  | 4.3  | 4.9  | 4.3  | 4.4  | 5.0  | 5.1  | 5.6  | 5.3   |
| 260.              | 4.5  | 4.5  | 4.3  | 5.3  | 4.5  | 4.6  | 4.9  | 5.2  | 5.5  | 5.1   |
| 270.              | 4.7  | 4.9  | 4.3  | 5.6  | 4.8  | 5.1  | 4.7  | 4.9  | 5.0  | 4.7   |
| 280.              | 5.1  | 5.3  | 4.3  | 5.9  | 5.0  | 5.4  | 4.5  | 4.6  | 4.6  | 4.4   |
| 290.              | 5.4  | 5.5  | 4.4  | 6.1  | 5.1  | 5.4  | 4.3  | 4.4  | 4.4  | 4.3   |
| 300.              | 5.5  | 5.4  | 4.4  | 6.3  | 4.9  | 5.2  | 4.3  | 4.3  | 4.3  | 4.3   |
| 310.              | 5.4  | 5.3  | 4.6  | 6.1  | 4.7  | 5.2  | 4.3  | 4.3  | 4.3  | 4.3   |
| 320.              | 5.4  | 5.2  | 4.6  | 5.8  | 4.6  | 5.4  | 4.3  | 4.3  | 4.3  | 4.3   |
| 330.              | 5.2  | 4.9  | 4.6  | 5.4  | 4.6  | 5.4  | 4.3  | 4.3  | 4.3  | 4.3   |
| 340.              | 5.1  | 4.8  | 4.6  | 4.9  | 4.7  | 5.5  | 4.3  | 4.3  | 4.3  | 4.3   |
| 350.              | 5.2  | 4.7  | 4.5  | 4.5  | 4.8  | 5.6  | 4.3  | 4.3  | 4.3  | 4.3   |
| 360.              | 5.3  | 4.6  | 4.5  | 4.4  | 4.9  | 5.5  | 4.3  | 4.3  | 4.3  | 4.3   |
| MAX               | 5.7  | 5.5  | 5.2  | 6.3  | 5.5  | 5.6  | 5.5  | 5.2  | 5.7  | 5.6   |
| DEGR.             | 40   | 290  | 70   | 300  | 70   | 350  | 200  | 260  | 240  | 110   |

THE HIGHEST CONCENTRATION OF 6.30 PPM OCCURRED AT RECEPTOR REC4 .





JOB: GristMillGlover2010ExistingPM

RUN: GristMillGlover2010ExistingPM

DATE : 4/ 7/11  
 TIME : 15:11:59

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S      VD = .0 CM/S      Z0 = 175. CM  
 U = 1.0 M/S      CLAS = 4 (D)      ATIM = 60. MINUTES      MIXH = 1000. M      AMB = 4.3 PPM

LINK VARIABLES

| LINK DESCRIPTION     | *<br>*<br>* | X1    | LINK COORDINATES (FT) |       | *<br>*<br>* | LENGTH<br>(FT) | BRG TYPE<br>(DEG) | VPH   | EF<br>(G/MI) | H<br>(FT) | W<br>(FT) | V/C | QUEUE<br>(VEH) |
|----------------------|-------------|-------|-----------------------|-------|-------------|----------------|-------------------|-------|--------------|-----------|-----------|-----|----------------|
|                      |             |       | Y1                    | X2    | Y2          |                |                   |       |              |           |           |     |                |
| 1. Grist Mill EB in  | *<br>*<br>* | .0    | 418.0                 | 200.0 | 418.0       | 200.           | 90. AG            | 1332. | 11.2         | .0        | 36.0      |     |                |
| 2. Grist Mill EB T   | *<br>*<br>* | 200.0 | 424.0                 | 353.3 | 424.0       | 153.           | 90. AG            | 410.  | 100.0        | .0        | 24.0      | .36 | 7.8            |
| 3. Grist Mill EB R   | *<br>*<br>* | 200.0 | 406.0                 | 206.3 | 406.0       | 6.             | 90. AG            | 93.   | 100.0        | .0        | 12.0      | .05 | .3             |
| 4. Grist Mill EB out | *<br>*<br>* | 454.0 | 412.0                 | 848.0 | 412.0       | 394.           | 90. AG            | 1332. | 11.2         | .0        | 24.0      |     |                |
| 5. Grist Mill WB in  | *<br>*<br>* | 848.0 | 442.0                 | 648.0 | 442.0       | 200.           | 270. AG           | 1404. | 11.2         | .0        | 36.0      |     |                |
| 6. Grist Mill WB L   | *<br>*<br>* | 648.0 | 430.0                 | 635.8 | 430.0       | 12.            | 270. AG           | 373.  | 100.0        | .0        | 12.0      | .11 | .6             |
| 7. Grist Mill WB T   | *<br>*<br>* | 648.0 | 448.0                 | 557.7 | 448.0       | 90.            | 270. AG           | 224.  | 100.0        | .0        | 24.0      | .29 | 4.6            |
| 8. Grist Mill WB out | *<br>*<br>* | 406.0 | 448.0                 | .0    | 448.0       | 406.           | 270. AG           | 1404. | 11.2         | .0        | 24.0      |     |                |
| 9. Glover NB in      | *<br>*<br>* | 442.0 | .0                    | 442.0 | 196.0       | 196.           | 360. AG           | 449.  | 11.2         | .0        | 24.0      |     |                |
| 10. Glover NB L      | *<br>*<br>* | 436.0 | 196.0                 | 436.0 | 347.2       | 151.           | 360. AG           | 354.  | 100.0        | .0        | 12.0      | .71 | 7.7            |
| 11. Glover NB LR     | *<br>*<br>* | 448.0 | 196.0                 | 448.0 | 260.7       | 65.            | 360. AG           | 354.  | 100.0        | .0        | 12.0      | .92 | 3.3            |
| 12. Glover SB out    | *<br>*<br>* | 418.0 | 400.0                 | 418.0 | .0          | 400.           | 180. AG           | 449.  | 11.2         | .0        | 24.0      |     |                |

DATE : 4/ 7/11  
 TIME : 15:11:59

-----  
 ADDITIONAL QUEUE LINK PARAMETERS  
 -----

| LINK DESCRIPTION   | *<br>*<br>*<br>* | CYCLE<br>LENGTH<br>(SEC) | RED<br>TIME<br>(SEC) | CLEARANCE<br>LOST TIME<br>(SEC) | APPROACH<br>VOL<br>(VPH) | SATURATION<br>FLOW RATE<br>(VPH) | IDLE<br>EM FAC<br>(gm/hr) | SIGNAL<br>TYPE | ARRIVAL<br>RATE |
|--------------------|------------------|--------------------------|----------------------|---------------------------------|--------------------------|----------------------------------|---------------------------|----------------|-----------------|
| 2. Grist Mill EB T | *                | 100                      | 44                   | 5.0                             | 1274                     | 3573                             | 173.64                    | 3              | 4               |
| 3. Grist Mill EB R | *                | 100                      | 20                   | 5.0                             | 58                       | 1599                             | 173.64                    | 3              | 4               |
| 6. Grist Mill WB L | *                | 100                      | 80                   | 3.0                             | 28                       | 1734                             | 173.64                    | 3              | 4               |
| 7. Grist Mill WB T | *                | 100                      | 24                   | 5.0                             | 1376                     | 3467                             | 173.64                    | 3              | 4               |
| 10. Glover NB L    | *                | 100                      | 76                   | 5.0                             | 361                      | 2987                             | 173.64                    | 3              | 3               |
| 11. Glover NB LR   | *                | 100                      | 76                   | 5.0                             | 88                       | 570                              | 173.64                    | 3              | 3               |

-----  
 RECEPTOR LOCATIONS  
 -----

| RECEPTOR          | *<br>*<br>*<br>* | X     | COORDINATES (FT)<br>Y | Z   | *<br>*<br>*<br>* |
|-------------------|------------------|-------|-----------------------|-----|------------------|
| 1. EB W Midblock  | *                | 196.0 | 390.0                 | 6.0 | *                |
| 2. SW Corner      | *                | 394.0 | 390.0                 | 6.0 | *                |
| 3. SB S Midblock  | *                | 394.0 | 200.0                 | 6.0 | *                |
| 4. NB S Midblock  | *                | 464.0 | 200.0                 | 6.0 | *                |
| 5. SE Corner      | *                | 464.0 | 390.0                 | 6.0 | *                |
| 6. EB E Midblock  | *                | 648.0 | 390.0                 | 6.0 | *                |
| 7. WB E Midblock  | *                | 648.0 | 470.0                 | 6.0 | *                |
| 8. NE Corner      | *                | 464.0 | 470.0                 | 6.0 | *                |
| 9. NW Corner      | *                | 396.0 | 470.0                 | 6.0 | *                |
| 10. WB W Midblock | *                | 196.0 | 470.0                 | 6.0 | *                |

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

| WIND ANGLE (DEGR) | REC1 | REC2 | REC3 | REC4 | REC5 | REC6 | REC7 | REC8 | REC9 | REC10 |
|-------------------|------|------|------|------|------|------|------|------|------|-------|
| 0.                | 5.2  | 4.5  | 4.7  | 5.0  | 4.7  | 5.3  | 4.3  | 4.3  | 4.3  | 4.3   |
| 10.               | 5.4  | 4.4  | 4.7  | 4.6  | 4.7  | 5.1  | 4.3  | 4.3  | 4.3  | 4.3   |
| 20.               | 5.4  | 4.4  | 5.1  | 4.5  | 4.7  | 5.1  | 4.3  | 4.3  | 4.3  | 4.3   |
| 30.               | 5.6  | 4.3  | 5.3  | 4.5  | 4.7  | 5.0  | 4.3  | 4.3  | 4.3  | 4.3   |
| 40.               | 5.7  | 4.3  | 5.5  | 4.6  | 4.8  | 5.1  | 4.3  | 4.3  | 4.3  | 4.3   |
| 50.               | 5.6  | 4.4  | 5.7  | 4.5  | 4.9  | 5.2  | 4.3  | 4.3  | 4.3  | 4.3   |
| 60.               | 5.7  | 4.7  | 5.6  | 4.5  | 5.1  | 5.2  | 4.3  | 4.3  | 4.3  | 4.3   |
| 70.               | 5.4  | 4.9  | 5.3  | 4.3  | 5.2  | 5.2  | 4.3  | 4.3  | 4.3  | 4.3   |
| 80.               | 5.2  | 5.0  | 5.2  | 4.3  | 5.1  | 5.0  | 4.4  | 4.5  | 4.4  | 4.4   |
| 90.               | 4.8  | 4.9  | 5.0  | 4.3  | 4.9  | 4.7  | 4.6  | 4.7  | 4.6  | 4.9   |
| 100.              | 4.6  | 4.6  | 4.9  | 4.3  | 4.5  | 4.4  | 4.9  | 4.8  | 4.7  | 5.3   |
| 110.              | 4.4  | 4.5  | 4.7  | 4.3  | 4.4  | 4.3  | 5.1  | 4.9  | 4.7  | 5.8   |
| 120.              | 4.5  | 4.5  | 4.5  | 4.3  | 4.3  | 4.3  | 5.2  | 4.7  | 4.5  | 5.8   |
| 130.              | 4.5  | 4.7  | 4.6  | 4.3  | 4.3  | 4.3  | 5.1  | 4.6  | 4.6  | 5.8   |
| 140.              | 4.3  | 4.9  | 4.6  | 4.3  | 4.3  | 4.3  | 5.1  | 4.6  | 4.5  | 5.7   |
| 150.              | 4.3  | 5.1  | 4.6  | 4.3  | 4.3  | 4.3  | 4.9  | 4.5  | 4.6  | 5.5   |
| 160.              | 4.3  | 5.1  | 4.6  | 4.3  | 4.3  | 4.3  | 5.1  | 4.5  | 5.0  | 5.5   |
| 170.              | 4.3  | 5.0  | 4.5  | 4.3  | 4.5  | 4.3  | 5.1  | 4.7  | 5.2  | 5.3   |
| 180.              | 4.3  | 4.7  | 4.4  | 4.4  | 4.9  | 4.3  | 5.2  | 4.9  | 5.1  | 5.2   |
| 190.              | 4.3  | 4.4  | 4.3  | 4.6  | 5.2  | 4.3  | 5.2  | 4.9  | 4.9  | 5.0   |
| 200.              | 4.3  | 4.3  | 4.3  | 4.6  | 5.1  | 4.3  | 5.3  | 4.7  | 4.9  | 5.1   |
| 210.              | 4.3  | 4.3  | 4.3  | 4.6  | 4.9  | 4.3  | 5.3  | 4.5  | 5.0  | 5.1   |
| 220.              | 4.3  | 4.3  | 4.3  | 4.6  | 4.7  | 4.5  | 5.6  | 4.3  | 5.2  | 5.1   |
| 230.              | 4.3  | 4.3  | 4.3  | 4.6  | 4.5  | 4.5  | 5.4  | 4.5  | 5.4  | 5.1   |
| 240.              | 4.3  | 4.3  | 4.3  | 4.8  | 4.4  | 4.6  | 5.4  | 4.8  | 5.6  | 5.2   |
| 250.              | 4.3  | 4.3  | 4.3  | 5.1  | 4.4  | 4.4  | 5.4  | 5.1  | 5.7  | 5.2   |
| 260.              | 4.4  | 4.5  | 4.3  | 5.3  | 4.5  | 4.6  | 5.1  | 5.2  | 5.5  | 5.0   |
| 270.              | 4.6  | 4.9  | 4.3  | 5.6  | 4.9  | 4.8  | 4.7  | 4.9  | 5.0  | 4.7   |
| 280.              | 4.9  | 5.3  | 4.3  | 5.8  | 5.1  | 5.0  | 4.6  | 4.6  | 4.6  | 4.4   |
| 290.              | 5.1  | 5.5  | 4.3  | 5.9  | 5.0  | 5.2  | 4.3  | 4.4  | 4.4  | 4.3   |
| 300.              | 5.2  | 5.3  | 4.5  | 6.4  | 4.8  | 5.1  | 4.3  | 4.3  | 4.3  | 4.3   |
| 310.              | 5.1  | 5.1  | 4.6  | 6.4  | 4.7  | 5.1  | 4.3  | 4.3  | 4.3  | 4.3   |
| 320.              | 5.1  | 4.9  | 4.7  | 6.6  | 4.5  | 5.2  | 4.3  | 4.3  | 4.3  | 4.3   |
| 330.              | 5.0  | 4.7  | 4.6  | 6.5  | 4.5  | 5.1  | 4.3  | 4.3  | 4.3  | 4.3   |
| 340.              | 5.0  | 4.5  | 4.6  | 6.2  | 4.5  | 5.2  | 4.3  | 4.3  | 4.3  | 4.3   |
| 350.              | 5.1  | 4.5  | 4.5  | 5.5  | 4.6  | 5.3  | 4.3  | 4.3  | 4.3  | 4.3   |
| 360.              | 5.2  | 4.5  | 4.7  | 5.0  | 4.7  | 5.3  | 4.3  | 4.3  | 4.3  | 4.3   |
| MAX               | 5.7  | 5.5  | 5.7  | 6.6  | 5.2  | 5.3  | 5.6  | 5.2  | 5.7  | 5.8   |
| DEGR.             | 40   | 290  | 50   | 320  | 70   | 0    | 220  | 260  | 250  | 110   |

THE HIGHEST CONCENTRATION OF 6.60 PPM OCCURRED AT RECEPTOR REC4 .

DATE : 4/ 7/11  
 TIME : 15:11:59

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING  
 THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

| LINK # | *<br>*<br>*<br>* | CO/LINK (PPM) |      |      |      |      |      |      |      |      |       |
|--------|------------------|---------------|------|------|------|------|------|------|------|------|-------|
|        |                  | REC1          | REC2 | REC3 | REC4 | REC5 | REC6 | REC7 | REC8 | REC9 | REC10 |
|        |                  | 40            | 290  | 50   | 320  | 70   | 0    | 220  | 260  | 250  | 110   |
| 1      | *                | .0            | .1   | .0   | .0   | .0   | .0   | .0   | .1   | .1   | .0    |
| 2      | *                | 1.0           | .8   | .0   | .2   | .0   | .0   | .0   | .4   | .7   | .7    |
| 3      | *                | .1            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    |
| 4      | *                | .0            | .0   | .1   | .0   | .6   | .4   | .3   | .0   | .0   | .1    |
| 5      | *                | .0            | .0   | .1   | .0   | .1   | .2   | .0   | .0   | .0   | .0    |
| 6      | *                | .0            | .0   | .0   | .0   | .0   | .2   | .1   | .0   | .0   | .0    |
| 7      | *                | .0            | .0   | .0   | .0   | .2   | .2   | .7   | .0   | .0   | .0    |
| 8      | *                | .3            | .3   | .0   | .1   | .0   | .0   | .0   | .4   | .6   | .6    |
| 9      | *                | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    |
| 10     | *                | .0            | .0   | .6   | .8   | .0   | .0   | .1   | .0   | .0   | .1    |
| 11     | *                | .0            | .0   | .4   | 1.1  | .0   | .0   | .1   | .0   | .0   | .0    |
| 12     | *                | .0            | .0   | .2   | .1   | .0   | .0   | .0   | .0   | .0   | .0    |

JOB: GristMillGlover2030NoBuildAM

RUN: GristMillGlover2030NoBuildAM

DATE : 4/15/11  
 TIME : 13:18:39

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S      VD = .0 CM/S      Z0 = 175. CM  
 U = 1.0 M/S      CLAS = 4 (D)      ATIM = 60. MINUTES      MIXH = 1000. M      AMB = 4.3 PPM

LINK VARIABLES

| LINK DESCRIPTION     | *<br>*<br>* | X1    | LINK COORDINATES (FT) |       | *<br>*<br>* | LENGTH<br>(FT) | BRG TYPE<br>(DEG) | VPH   | EF<br>(G/MI) | H<br>(FT) | W<br>(FT) | V/C | QUEUE<br>(VEH) |
|----------------------|-------------|-------|-----------------------|-------|-------------|----------------|-------------------|-------|--------------|-----------|-----------|-----|----------------|
|                      |             |       | Y1                    | X2    | Y2          |                |                   |       |              |           |           |     |                |
| 1. Grist Mill EB in  | *<br>*<br>* | .0    | 418.0                 | 200.0 | 418.0       | 200.           | 90. AG            | 2584. | 8.3          | .0        | 36.0      |     |                |
| 2. Grist Mill EB T   | *<br>*<br>* | 200.0 | 424.0                 | 415.3 | 424.0       | 215.           | 90. AG            | 231.  | 100.0        | .0        | 24.0      | .50 | 10.9           |
| 3. Grist Mill EB R   | *<br>*<br>* | 200.0 | 406.0                 | 259.8 | 406.0       | 60.            | 90. AG            | 75.   | 100.0        | .0        | 12.0      | .40 | 3.0            |
| 4. Grist Mill EB out | *<br>*<br>* | 454.0 | 412.0                 | 848.0 | 412.0       | 394.           | 90. AG            | 2584. | 8.3          | .0        | 24.0      |     |                |
| 5. Grist Mill WB in  | *<br>*<br>* | 848.0 | 442.0                 | 648.0 | 442.0       | 200.           | 270. AG           | 1589. | 8.3          | .0        | 36.0      |     |                |
| 6. Grist Mill WB L   | *<br>*<br>* | 648.0 | 430.0                 | 614.6 | 430.0       | 33.            | 270. AG           | 268.  | 100.0        | .0        | 12.0      | .24 | 1.7            |
| 7. Grist Mill WB T   | *<br>*<br>* | 648.0 | 448.0                 | 594.0 | 448.0       | 54.            | 270. AG           | 81.   | 100.0        | .0        | 24.0      | .27 | 2.7            |
| 8. Grist Mill WB out | *<br>*<br>* | 406.0 | 448.0                 | .0    | 448.0       | 406.           | 270. AG           | 1589. | 8.3          | .0        | 24.0      |     |                |
| 9. Glover NB in      | *<br>*<br>* | 442.0 | .0                    | 442.0 | 196.0       | 196.           | 360. AG           | 138.  | 8.3          | .0        | 24.0      |     |                |
| 10. Glover NB L      | *<br>*<br>* | 436.0 | 196.0                 | 436.0 | 256.5       | 60.            | 360. AG           | 303.  | 100.0        | .0        | 12.0      | .72 | 3.1            |
| 11. Glover NB LR     | *<br>*<br>* | 448.0 | 196.0                 | 448.0 | 229.3       | 33.            | 360. AG           | 303.  | 100.0        | .0        | 12.0      | .86 | 1.7            |
| 12. Glover SB out    | *<br>*<br>* | 418.0 | 400.0                 | 418.0 | .0          | 400.           | 180. AG           | 138.  | 8.3          | .0        | 24.0      |     |                |

DATE : 4/15/11  
 TIME : 13:18:39

-----  
 ADDITIONAL QUEUE LINK PARAMETERS  
 -----

| LINK DESCRIPTION   | *<br>* | CYCLE<br>LENGTH<br>(SEC) | RED<br>TIME<br>(SEC) | CLEARANCE<br>LOST TIME<br>(SEC) | APPROACH<br>VOL<br>(VPH) | SATURATION<br>FLOW RATE<br>(VPH) | IDLE<br>EM FAC<br>(gm/hr) | SIGNAL<br>TYPE | ARRIVAL<br>RATE |
|--------------------|--------|--------------------------|----------------------|---------------------------------|--------------------------|----------------------------------|---------------------------|----------------|-----------------|
| 2. Grist Mill EB T | *<br>* | 110                      | 37                   | 5.0                             | 2128                     | 3540                             | 127.94                    | 3              | 4               |
| 3. Grist Mill EB R | *<br>* | 110                      | 24                   | 5.0                             | 456                      | 1584                             | 127.94                    | 3              | 4               |
| 6. Grist Mill WB L | *<br>* | 110                      | 86                   | 3.0                             | 71                       | 1702                             | 127.94                    | 3              | 4               |
| 7. Grist Mill WB T | *<br>* | 110                      | 13                   | 5.0                             | 1518                     | 3403                             | 127.94                    | 3              | 4               |
| 10. Glover NB L    | *<br>* | 110                      | 97                   | 5.0                             | 102                      | 2610                             | 127.94                    | 3              | 3               |
| 11. Glover NB LR   | *<br>* | 110                      | 97                   | 5.0                             | 36                       | 776                              | 127.94                    | 3              | 3               |

-----  
 RECEPTOR LOCATIONS  
 -----

| RECEPTOR          | *<br>* | X     | COORDINATES (FT)<br>Y | Z   | *<br>* |
|-------------------|--------|-------|-----------------------|-----|--------|
| 1. EB W Midblock  | *<br>* | 196.0 | 390.0                 | 6.0 | *<br>* |
| 2. SW Corner      | *<br>* | 394.0 | 390.0                 | 6.0 | *<br>* |
| 3. SB S Midblock  | *<br>* | 394.0 | 200.0                 | 6.0 | *<br>* |
| 4. NB S Midblock  | *<br>* | 464.0 | 200.0                 | 6.0 | *<br>* |
| 5. SE Corner      | *<br>* | 464.0 | 390.0                 | 6.0 | *<br>* |
| 6. EB E Midblock  | *<br>* | 648.0 | 390.0                 | 6.0 | *<br>* |
| 7. WB E Midblock  | *<br>* | 648.0 | 470.0                 | 6.0 | *<br>* |
| 8. NE Corner      | *<br>* | 464.0 | 470.0                 | 6.0 | *<br>* |
| 9. NW Corner      | *<br>* | 396.0 | 470.0                 | 6.0 | *<br>* |
| 10. WB W Midblock | *<br>* | 196.0 | 470.0                 | 6.0 | *<br>* |

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

| WIND ANGLE (DEGR) | REC1 | REC2 | REC3 | REC4 | REC5 | REC6 | REC7 | REC8 | REC9 | REC10 |
|-------------------|------|------|------|------|------|------|------|------|------|-------|
| 0.                | 5.1  | 5.0  | 4.4  | 4.5  | 4.9  | 5.3  | 4.3  | 4.3  | 4.3  | 4.3   |
| 10.               | 5.2  | 4.9  | 4.5  | 4.4  | 4.9  | 5.2  | 4.3  | 4.3  | 4.3  | 4.3   |
| 20.               | 5.2  | 4.8  | 4.5  | 4.4  | 4.9  | 5.1  | 4.3  | 4.3  | 4.3  | 4.3   |
| 30.               | 5.3  | 4.6  | 4.6  | 4.5  | 4.9  | 5.2  | 4.3  | 4.3  | 4.3  | 4.3   |
| 40.               | 5.3  | 4.5  | 4.8  | 4.6  | 5.0  | 5.3  | 4.3  | 4.3  | 4.3  | 4.3   |
| 50.               | 5.3  | 4.5  | 5.0  | 4.5  | 5.0  | 5.3  | 4.3  | 4.3  | 4.3  | 4.3   |
| 60.               | 5.3  | 4.5  | 5.1  | 4.4  | 5.1  | 5.4  | 4.3  | 4.3  | 4.3  | 4.3   |
| 70.               | 5.4  | 4.8  | 5.1  | 4.3  | 5.4  | 5.3  | 4.3  | 4.3  | 4.3  | 4.3   |
| 80.               | 5.1  | 4.9  | 5.0  | 4.3  | 5.3  | 5.2  | 4.4  | 4.4  | 4.4  | 4.5   |
| 90.               | 4.9  | 4.9  | 4.8  | 4.3  | 5.0  | 4.8  | 4.6  | 4.6  | 4.6  | 4.8   |
| 100.              | 4.5  | 4.5  | 4.6  | 4.3  | 4.6  | 4.5  | 4.9  | 4.8  | 4.7  | 5.2   |
| 110.              | 4.3  | 4.4  | 4.5  | 4.3  | 4.4  | 4.4  | 5.1  | 4.8  | 4.7  | 5.3   |
| 120.              | 4.3  | 4.3  | 4.3  | 4.3  | 4.3  | 4.3  | 5.2  | 4.7  | 4.7  | 5.3   |
| 130.              | 4.3  | 4.3  | 4.3  | 4.3  | 4.3  | 4.3  | 5.1  | 4.7  | 4.6  | 5.3   |
| 140.              | 4.3  | 4.3  | 4.3  | 4.3  | 4.3  | 4.3  | 5.1  | 4.7  | 4.6  | 5.3   |
| 150.              | 4.3  | 4.4  | 4.3  | 4.3  | 4.3  | 4.3  | 5.1  | 4.7  | 4.8  | 5.2   |
| 160.              | 4.3  | 4.5  | 4.3  | 4.3  | 4.3  | 4.3  | 4.9  | 4.6  | 4.7  | 5.2   |
| 170.              | 4.3  | 4.4  | 4.3  | 4.3  | 4.3  | 4.3  | 5.1  | 4.6  | 5.0  | 5.3   |
| 180.              | 4.3  | 4.4  | 4.3  | 4.3  | 4.5  | 4.3  | 5.1  | 4.7  | 5.1  | 5.2   |
| 190.              | 4.3  | 4.3  | 4.3  | 4.3  | 4.5  | 4.3  | 5.2  | 4.6  | 5.1  | 5.1   |
| 200.              | 4.3  | 4.3  | 4.3  | 4.3  | 4.4  | 4.3  | 5.2  | 4.4  | 5.1  | 5.1   |
| 210.              | 4.3  | 4.3  | 4.3  | 4.3  | 4.3  | 4.3  | 5.2  | 4.4  | 5.1  | 5.1   |
| 220.              | 4.3  | 4.3  | 4.3  | 4.3  | 4.3  | 4.3  | 5.1  | 4.5  | 5.2  | 5.2   |
| 230.              | 4.3  | 4.3  | 4.3  | 4.4  | 4.3  | 4.4  | 5.0  | 4.7  | 5.3  | 5.3   |
| 240.              | 4.3  | 4.3  | 4.3  | 4.6  | 4.3  | 4.3  | 5.0  | 4.8  | 5.4  | 5.3   |
| 250.              | 4.4  | 4.3  | 4.3  | 4.7  | 4.3  | 4.4  | 4.9  | 5.1  | 5.3  | 5.2   |
| 260.              | 4.5  | 4.5  | 4.3  | 5.1  | 4.5  | 4.6  | 4.9  | 5.0  | 5.3  | 4.9   |
| 270.              | 4.7  | 4.8  | 4.3  | 5.3  | 4.8  | 5.0  | 4.7  | 4.9  | 4.9  | 4.7   |
| 280.              | 5.1  | 5.1  | 4.3  | 5.5  | 5.1  | 5.3  | 4.5  | 4.6  | 4.5  | 4.4   |
| 290.              | 5.3  | 5.3  | 4.3  | 5.7  | 5.1  | 5.3  | 4.3  | 4.3  | 4.4  | 4.3   |
| 300.              | 5.3  | 5.2  | 4.4  | 5.9  | 4.9  | 5.2  | 4.3  | 4.3  | 4.3  | 4.3   |
| 310.              | 5.2  | 5.1  | 4.5  | 6.0  | 4.8  | 5.2  | 4.3  | 4.3  | 4.3  | 4.3   |
| 320.              | 5.2  | 5.1  | 4.6  | 5.7  | 4.7  | 5.3  | 4.3  | 4.3  | 4.3  | 4.3   |
| 330.              | 5.1  | 5.0  | 4.5  | 5.5  | 4.5  | 5.3  | 4.3  | 4.3  | 4.3  | 4.3   |
| 340.              | 5.1  | 5.0  | 4.5  | 5.2  | 4.7  | 5.3  | 4.3  | 4.3  | 4.3  | 4.3   |
| 350.              | 5.1  | 5.0  | 4.5  | 4.7  | 4.8  | 5.4  | 4.3  | 4.3  | 4.3  | 4.3   |
| 360.              | 5.1  | 5.0  | 4.4  | 4.5  | 4.9  | 5.3  | 4.3  | 4.3  | 4.3  | 4.3   |
| MAX               | 5.4  | 5.3  | 5.1  | 6.0  | 5.4  | 5.4  | 5.2  | 5.1  | 5.4  | 5.3   |
| DEGR.             | 70   | 290  | 60   | 310  | 70   | 60   | 120  | 250  | 240  | 110   |

THE HIGHEST CONCENTRATION OF 6.00 PPM OCCURRED AT RECEPTOR REC4 .





JOB: GristMillGlover2030NoBuildPM

RUN: GristMillGlover2030NoBuildPM

DATE : 4/15/11  
 TIME : 13:20:37

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S      VD = .0 CM/S      Z0 = 175. CM  
 U = 1.0 M/S      CLAS = 4 (D)      ATIM = 60. MINUTES      MIXH = 1000. M      AMB = 4.3 PPM

LINK VARIABLES

| LINK DESCRIPTION     | *<br>*<br>* | X1    | LINK COORDINATES (FT) |       | *<br>*<br>* | LENGTH<br>(FT) | BRG TYPE<br>(DEG) | VPH   | EF<br>(G/MI) | H<br>(FT) | W<br>(FT) | V/C  | QUEUE<br>(VEH) |
|----------------------|-------------|-------|-----------------------|-------|-------------|----------------|-------------------|-------|--------------|-----------|-----------|------|----------------|
|                      |             |       | Y1                    | X2    | Y2          |                |                   |       |              |           |           |      |                |
| 1. Grist Mill EB in  | *<br>*<br>* | .0    | 418.0                 | 200.0 | 418.0       | 200.           | 90. AG            | 1599. | 8.3          | .0        | 36.0      |      |                |
| 2. Grist Mill EB T   | *<br>*<br>* | 200.0 | 424.0                 | 383.8 | 424.0       | 184.           | 90. AG            | 302.  | 100.0        | .0        | 24.0      | .44  | 9.3            |
| 3. Grist Mill EB R   | *<br>*<br>* | 200.0 | 406.0                 | 207.7 | 406.0       | 8.             | 90. AG            | 69.   | 100.0        | .0        | 12.0      | .06  | .4             |
| 4. Grist Mill EB out | *<br>*<br>* | 454.0 | 412.0                 | 848.0 | 412.0       | 394.           | 90. AG            | 1599. | 8.3          | .0        | 24.0      |      |                |
| 5. Grist Mill WB in  | *<br>*<br>* | 848.0 | 442.0                 | 648.0 | 442.0       | 200.           | 270. AG           | 1685. | 8.3          | .0        | 36.0      |      |                |
| 6. Grist Mill WB L   | *<br>*<br>* | 648.0 | 430.0                 | 633.1 | 430.0       | 15.            | 270. AG           | 275.  | 100.0        | .0        | 12.0      | .13  | .8             |
| 7. Grist Mill WB T   | *<br>*<br>* | 648.0 | 448.0                 | 539.7 | 448.0       | 108.           | 270. AG           | 165.  | 100.0        | .0        | 24.0      | .34  | 5.5            |
| 8. Grist Mill WB out | *<br>*<br>* | 406.0 | 448.0                 | .0    | 448.0       | 406.           | 270. AG           | 1685. | 8.3          | .0        | 24.0      |      |                |
| 9. Glover NB in      | *<br>*<br>* | 442.0 | .0                    | 442.0 | 196.0       | 196.           | 360. AG           | 539.  | 8.3          | .0        | 24.0      |      |                |
| 10. Glover NB L      | *<br>*<br>* | 436.0 | 196.0                 | 436.0 | 401.5       | 206.           | 360. AG           | 261.  | 100.0        | .0        | 12.0      | .86  | 10.4           |
| 11. Glover NB LR     | *<br>*<br>* | 448.0 | 196.0                 | 448.0 | 351.0       | 155.           | 360. AG           | 261.  | 100.0        | .0        | 12.0      | 1.06 | 7.9            |
| 12. Glover SB out    | *<br>*<br>* | 418.0 | 400.0                 | 418.0 | .0          | 400.           | 180. AG           | 539.  | 8.3          | .0        | 24.0      |      |                |

DATE : 4/15/11  
 TIME : 13:20:37

-----  
 ADDITIONAL QUEUE LINK PARAMETERS  
 -----

| LINK DESCRIPTION   | *<br>* | CYCLE<br>LENGTH<br>(SEC) | RED<br>TIME<br>(SEC) | CLEARANCE<br>LOST TIME<br>(SEC) | APPROACH<br>VOL<br>(VPH) | SATURATION<br>FLOW RATE<br>(VPH) | IDLE<br>EM FAC<br>(gm/hr) | SIGNAL<br>TYPE | ARRIVAL<br>RATE |
|--------------------|--------|--------------------------|----------------------|---------------------------------|--------------------------|----------------------------------|---------------------------|----------------|-----------------|
| 2. Grist Mill EB T | *<br>* | 100                      | 44                   | 5.0                             | 1529                     | 3573                             | 127.94                    | 3              | 4               |
| 3. Grist Mill EB R | *<br>* | 100                      | 20                   | 5.0                             | 70                       | 1599                             | 127.94                    | 3              | 4               |
| 6. Grist Mill WB L | *<br>* | 100                      | 80                   | 3.0                             | 34                       | 1734                             | 127.94                    | 3              | 4               |
| 7. Grist Mill WB T | *<br>* | 100                      | 24                   | 5.0                             | 1651                     | 3467                             | 127.94                    | 3              | 4               |
| 10. Glover NB L    | *<br>* | 100                      | 76                   | 5.0                             | 433                      | 2963                             | 127.94                    | 3              | 3               |
| 11. Glover NB LR   | *<br>* | 100                      | 76                   | 5.0                             | 106                      | 590                              | 127.94                    | 3              | 3               |

-----  
 RECEPTOR LOCATIONS  
 -----

| RECEPTOR          | *<br>* | X     | COORDINATES (FT)<br>Y | Z   | *<br>* |
|-------------------|--------|-------|-----------------------|-----|--------|
| 1. EB W Midblock  | *<br>* | 196.0 | 390.0                 | 6.0 | *<br>* |
| 2. SW Corner      | *<br>* | 394.0 | 390.0                 | 6.0 | *<br>* |
| 3. SB S Midblock  | *<br>* | 394.0 | 200.0                 | 6.0 | *<br>* |
| 4. NB S Midblock  | *<br>* | 464.0 | 200.0                 | 6.0 | *<br>* |
| 5. SE Corner      | *<br>* | 464.0 | 390.0                 | 6.0 | *<br>* |
| 6. EB E Midblock  | *<br>* | 648.0 | 390.0                 | 6.0 | *<br>* |
| 7. WB E Midblock  | *<br>* | 648.0 | 470.0                 | 6.0 | *<br>* |
| 8. NE Corner      | *<br>* | 464.0 | 470.0                 | 6.0 | *<br>* |
| 9. NW Corner      | *<br>* | 396.0 | 470.0                 | 6.0 | *<br>* |
| 10. WB W Midblock | *<br>* | 196.0 | 470.0                 | 6.0 | *<br>* |

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

| WIND ANGLE (DEGR) | REC1 | REC2 | REC3 | REC4 | REC5 | REC6 | REC7 | REC8 | REC9 | REC10 |
|-------------------|------|------|------|------|------|------|------|------|------|-------|
| 0.                | 5.0  | 4.6  | 4.7  | 5.2  | 4.6  | 5.1  | 4.3  | 4.3  | 4.3  | 4.3   |
| 10.               | 5.2  | 4.4  | 4.8  | 4.7  | 4.7  | 5.1  | 4.3  | 4.3  | 4.3  | 4.3   |
| 20.               | 5.2  | 4.4  | 5.2  | 4.6  | 4.7  | 5.0  | 4.3  | 4.3  | 4.3  | 4.3   |
| 30.               | 5.3  | 4.3  | 5.4  | 4.5  | 4.7  | 5.0  | 4.3  | 4.3  | 4.3  | 4.3   |
| 40.               | 5.3  | 4.3  | 5.5  | 4.5  | 4.8  | 5.0  | 4.3  | 4.3  | 4.3  | 4.3   |
| 50.               | 5.4  | 4.4  | 5.4  | 4.5  | 4.9  | 5.1  | 4.3  | 4.3  | 4.3  | 4.3   |
| 60.               | 5.3  | 4.6  | 5.3  | 4.4  | 5.0  | 5.1  | 4.3  | 4.3  | 4.3  | 4.3   |
| 70.               | 5.3  | 5.1  | 5.1  | 4.3  | 5.1  | 5.1  | 4.3  | 4.3  | 4.3  | 4.3   |
| 80.               | 5.1  | 5.1  | 5.0  | 4.3  | 5.0  | 4.9  | 4.4  | 4.5  | 4.4  | 4.4   |
| 90.               | 4.8  | 5.2  | 4.8  | 4.3  | 4.8  | 4.7  | 4.6  | 4.7  | 4.6  | 4.9   |
| 100.              | 4.7  | 5.0  | 4.8  | 4.3  | 4.5  | 4.4  | 4.8  | 4.8  | 4.7  | 5.3   |
| 110.              | 4.5  | 4.9  | 4.7  | 4.3  | 4.4  | 4.3  | 5.0  | 4.9  | 4.6  | 5.5   |
| 120.              | 4.5  | 4.9  | 4.5  | 4.3  | 4.3  | 4.3  | 5.0  | 4.7  | 4.5  | 5.6   |
| 130.              | 4.5  | 5.0  | 4.5  | 4.3  | 4.3  | 4.3  | 5.0  | 4.5  | 4.7  | 5.6   |
| 140.              | 4.3  | 5.2  | 4.5  | 4.3  | 4.3  | 4.3  | 4.9  | 4.5  | 4.7  | 5.5   |
| 150.              | 4.3  | 5.4  | 4.6  | 4.3  | 4.3  | 4.3  | 4.9  | 4.5  | 4.9  | 5.2   |
| 160.              | 4.3  | 5.2  | 4.6  | 4.3  | 4.4  | 4.3  | 4.9  | 4.5  | 5.1  | 5.1   |
| 170.              | 4.3  | 5.0  | 4.5  | 4.3  | 4.6  | 4.3  | 5.0  | 4.7  | 5.2  | 5.2   |
| 180.              | 4.3  | 4.6  | 4.4  | 4.4  | 5.0  | 4.3  | 5.1  | 5.1  | 5.2  | 5.1   |
| 190.              | 4.3  | 4.4  | 4.3  | 4.5  | 5.5  | 4.3  | 5.1  | 5.1  | 5.0  | 5.0   |
| 200.              | 4.3  | 4.3  | 4.3  | 4.6  | 5.5  | 4.3  | 5.2  | 4.9  | 5.0  | 5.0   |
| 210.              | 4.3  | 4.3  | 4.3  | 4.6  | 5.3  | 4.3  | 5.2  | 4.6  | 5.2  | 5.0   |
| 220.              | 4.3  | 4.3  | 4.3  | 4.5  | 5.1  | 4.4  | 5.3  | 4.5  | 5.3  | 5.0   |
| 230.              | 4.3  | 4.3  | 4.3  | 4.6  | 5.0  | 4.5  | 5.3  | 4.6  | 5.4  | 5.1   |
| 240.              | 4.3  | 4.3  | 4.3  | 4.7  | 4.9  | 4.5  | 5.3  | 4.8  | 5.4  | 5.1   |
| 250.              | 4.3  | 4.3  | 4.3  | 4.9  | 4.9  | 4.5  | 5.2  | 5.0  | 5.6  | 5.0   |
| 260.              | 4.4  | 4.5  | 4.3  | 5.1  | 5.0  | 4.7  | 5.0  | 5.2  | 5.3  | 4.9   |
| 270.              | 4.5  | 4.8  | 4.3  | 5.2  | 5.3  | 4.9  | 4.7  | 4.9  | 5.0  | 4.7   |
| 280.              | 4.8  | 5.2  | 4.3  | 5.4  | 5.5  | 4.9  | 4.6  | 4.6  | 4.5  | 4.4   |
| 290.              | 5.0  | 5.5  | 4.3  | 5.6  | 5.3  | 5.1  | 4.3  | 4.4  | 4.4  | 4.3   |
| 300.              | 5.0  | 5.4  | 4.4  | 5.8  | 5.0  | 5.0  | 4.3  | 4.3  | 4.3  | 4.3   |
| 310.              | 5.1  | 5.3  | 4.6  | 5.8  | 4.8  | 5.0  | 4.3  | 4.3  | 4.3  | 4.3   |
| 320.              | 4.9  | 5.1  | 4.5  | 6.1  | 4.5  | 5.1  | 4.3  | 4.3  | 4.3  | 4.3   |
| 330.              | 4.9  | 5.0  | 4.6  | 6.2  | 4.5  | 5.1  | 4.3  | 4.3  | 4.3  | 4.3   |
| 340.              | 4.8  | 4.9  | 4.6  | 6.1  | 4.5  | 5.1  | 4.3  | 4.3  | 4.3  | 4.3   |
| 350.              | 4.9  | 4.8  | 4.5  | 5.7  | 4.6  | 5.2  | 4.3  | 4.3  | 4.3  | 4.3   |
| 360.              | 5.0  | 4.6  | 4.7  | 5.2  | 4.6  | 5.1  | 4.3  | 4.3  | 4.3  | 4.3   |
| MAX               | 5.4  | 5.5  | 5.5  | 6.2  | 5.5  | 5.2  | 5.3  | 5.2  | 5.6  | 5.6   |
| DEGR.             | 50   | 290  | 40   | 330  | 190  | 350  | 220  | 260  | 250  | 120   |

THE HIGHEST CONCENTRATION OF 6.20 PPM OCCURRED AT RECEPTOR REC4 .

DATE : 4/15/11  
 TIME : 13:20:37

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING  
 THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

| LINK # | * | CO/LINK (PPM) |      |      |      |      |      |      |      |      |       |
|--------|---|---------------|------|------|------|------|------|------|------|------|-------|
|        |   | REC1          | REC2 | REC3 | REC4 | REC5 | REC6 | REC7 | REC8 | REC9 | REC10 |
|        | * | 50            | 290  | 40   | 330  | 190  | 350  | 220  | 260  | 250  | 120   |
| 1      | * | .0            | .1   | .0   | .0   | .0   | .0   | .0   | .1   | .1   | .0    |
| 2      | * | .8            | .8   | .0   | .2   | .0   | .0   | .0   | .4   | .6   | .6    |
| 3      | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    |
| 4      | * | .0            | .0   | .1   | .0   | .0   | .4   | .2   | .0   | .0   | .0    |
| 5      | * | .0            | .0   | .0   | .0   | .0   | .1   | .0   | .0   | .0   | .0    |
| 6      | * | .0            | .0   | .0   | .0   | .0   | .2   | .1   | .0   | .0   | .0    |
| 7      | * | .0            | .0   | .1   | .0   | .0   | .2   | .5   | .0   | .0   | .0    |
| 8      | * | .3            | .3   | .0   | .1   | .0   | .0   | .0   | .4   | .6   | .5    |
| 9      | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    |
| 10     | * | .0            | .0   | .5   | .6   | .5   | .0   | .1   | .0   | .0   | .1    |
| 11     | * | .0            | .0   | .4   | .9   | .6   | .0   | .1   | .0   | .0   | .1    |
| 12     | * | .0            | .0   | .1   | .1   | .1   | .0   | .0   | .0   | .0   | .0    |

JOB: GristMillGlover2030BuildAM

RUN: GristMillGlover2030BuildAM

DATE : 4/15/11  
 TIME : 13:22:41

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S      VD = .0 CM/S      Z0 = 175. CM  
 U = 1.0 M/S      CLAS = 4 (D)      ATIM = 60. MINUTES      MIXH = 1000. M      AMB = 4.3 PPM

LINK VARIABLES

| LINK DESCRIPTION     | *<br>*<br>* | x1    | LINK COORDINATES (FT) |       | *<br>*<br>* | LENGTH<br>(FT) | BRG TYPE<br>(DEG) | VPH   | EF<br>(G/MI) | H<br>(FT) | W<br>(FT) | V/C | QUEUE<br>(VEH) |
|----------------------|-------------|-------|-----------------------|-------|-------------|----------------|-------------------|-------|--------------|-----------|-----------|-----|----------------|
|                      |             |       | Y1                    | X2    | Y2          |                |                   |       |              |           |           |     |                |
| 1. Grist Mill EB in  | *<br>*<br>* | .0    | 418.0                 | 200.0 | 418.0       | 200.           | 90. AG            | 2585. | 8.3          | .0        | 36.0      |     |                |
| 2. Grist Mill EB T   | *<br>*<br>* | 200.0 | 424.0                 | 415.3 | 424.0       | 215.           | 90. AG            | 231.  | 100.0        | .0        | 24.0      | .50 | 10.9           |
| 3. Grist Mill EB R   | *<br>*<br>* | 200.0 | 406.0                 | 260.0 | 406.0       | 60.            | 90. AG            | 75.   | 100.0        | .0        | 12.0      | .40 | 3.0            |
| 4. Grist Mill EB out | *<br>*<br>* | 454.0 | 412.0                 | 848.0 | 412.0       | 394.           | 90. AG            | 2585. | 8.3          | .0        | 24.0      |     |                |
| 5. Grist Mill WB in  | *<br>*<br>* | 848.0 | 442.0                 | 648.0 | 442.0       | 200.           | 270. AG           | 1596. | 8.3          | .0        | 36.0      |     |                |
| 6. Grist Mill WB L   | *<br>*<br>* | 648.0 | 430.0                 | 611.3 | 430.0       | 37.            | 270. AG           | 268.  | 100.0        | .0        | 12.0      | .27 | 1.9            |
| 7. Grist Mill WB T   | *<br>*<br>* | 648.0 | 448.0                 | 594.0 | 448.0       | 54.            | 270. AG           | 81.   | 100.0        | .0        | 24.0      | .27 | 2.7            |
| 8. Grist Mill WB out | *<br>*<br>* | 406.0 | 448.0                 | .0    | 448.0       | 406.           | 270. AG           | 1596. | 8.3          | .0        | 24.0      |     |                |
| 9. Glover NB in      | *<br>*<br>* | 442.0 | .0                    | 442.0 | 196.0       | 196.           | 360. AG           | 138.  | 8.3          | .0        | 24.0      |     |                |
| 10. Glover NB L      | *<br>*<br>* | 436.0 | 196.0                 | 436.0 | 256.5       | 60.            | 360. AG           | 303.  | 100.0        | .0        | 12.0      | .72 | 3.1            |
| 11. Glover NB LR     | *<br>*<br>* | 448.0 | 196.0                 | 448.0 | 229.3       | 33.            | 360. AG           | 303.  | 100.0        | .0        | 12.0      | .86 | 1.7            |
| 12. Glover SB out    | *<br>*<br>* | 418.0 | 400.0                 | 418.0 | .0          | 400.           | 180. AG           | 138.  | 8.3          | .0        | 24.0      |     |                |

DATE : 4/15/11  
 TIME : 13:22:41

-----  
 ADDITIONAL QUEUE LINK PARAMETERS  
 -----

| LINK DESCRIPTION   | *<br>* | CYCLE<br>LENGTH<br>(SEC) | RED<br>TIME<br>(SEC) | CLEARANCE<br>LOST TIME<br>(SEC) | APPROACH<br>VOL<br>(VPH) | SATURATION<br>FLOW RATE<br>(VPH) | IDLE<br>EM FAC<br>(gm/hr) | SIGNAL<br>TYPE | ARRIVAL<br>RATE |
|--------------------|--------|--------------------------|----------------------|---------------------------------|--------------------------|----------------------------------|---------------------------|----------------|-----------------|
| 2. Grist Mill EB T | *      | 110                      | 37                   | 5.0                             | 2128                     | 3540                             | 127.94                    | 3              | 4               |
| 3. Grist Mill EB R | *      | 110                      | 24                   | 5.0                             | 457                      | 1584                             | 127.94                    | 3              | 4               |
| 6. Grist Mill WB L | *      | 110                      | 86                   | 3.0                             | 78                       | 1702                             | 127.94                    | 3              | 4               |
| 7. Grist Mill WB T | *      | 110                      | 13                   | 5.0                             | 1518                     | 3403                             | 127.94                    | 3              | 4               |
| 10. Glover NB L    | *      | 110                      | 97                   | 5.0                             | 102                      | 2610                             | 127.94                    | 3              | 3               |
| 11. Glover NB LR   | *      | 110                      | 97                   | 5.0                             | 36                       | 776                              | 127.94                    | 3              | 3               |

-----  
 RECEPTOR LOCATIONS  
 -----

| RECEPTOR          | *<br>* | X     | COORDINATES (FT)<br>Y | Z   | *<br>* |
|-------------------|--------|-------|-----------------------|-----|--------|
| 1. EB W Midblock  | *      | 196.0 | 390.0                 | 6.0 | *      |
| 2. SW Corner      | *      | 394.0 | 390.0                 | 6.0 | *      |
| 3. SB S Midblock  | *      | 394.0 | 200.0                 | 6.0 | *      |
| 4. NB S Midblock  | *      | 464.0 | 200.0                 | 6.0 | *      |
| 5. SE Corner      | *      | 464.0 | 390.0                 | 6.0 | *      |
| 6. EB E Midblock  | *      | 648.0 | 390.0                 | 6.0 | *      |
| 7. WB E Midblock  | *      | 648.0 | 470.0                 | 6.0 | *      |
| 8. NE Corner      | *      | 464.0 | 470.0                 | 6.0 | *      |
| 9. NW Corner      | *      | 396.0 | 470.0                 | 6.0 | *      |
| 10. WB W Midblock | *      | 196.0 | 470.0                 | 6.0 | *      |

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

| WIND ANGLE (DEGR) | REC1 | REC2 | REC3 | REC4 | REC5 | REC6 | REC7 | REC8 | REC9 | REC10 |
|-------------------|------|------|------|------|------|------|------|------|------|-------|
| 0.                | 5.1  | 5.0  | 4.4  | 4.5  | 4.9  | 5.3  | 4.3  | 4.3  | 4.3  | 4.3   |
| 10.               | 5.2  | 4.9  | 4.5  | 4.4  | 4.9  | 5.2  | 4.3  | 4.3  | 4.3  | 4.3   |
| 20.               | 5.2  | 4.8  | 4.5  | 4.4  | 4.9  | 5.1  | 4.3  | 4.3  | 4.3  | 4.3   |
| 30.               | 5.3  | 4.6  | 4.6  | 4.5  | 4.9  | 5.2  | 4.3  | 4.3  | 4.3  | 4.3   |
| 40.               | 5.3  | 4.5  | 4.8  | 4.6  | 5.0  | 5.3  | 4.3  | 4.3  | 4.3  | 4.3   |
| 50.               | 5.3  | 4.5  | 5.0  | 4.5  | 5.0  | 5.3  | 4.3  | 4.3  | 4.3  | 4.3   |
| 60.               | 5.3  | 4.5  | 5.1  | 4.4  | 5.1  | 5.4  | 4.3  | 4.3  | 4.3  | 4.3   |
| 70.               | 5.4  | 4.8  | 5.1  | 4.3  | 5.4  | 5.3  | 4.3  | 4.3  | 4.3  | 4.3   |
| 80.               | 5.1  | 4.9  | 5.0  | 4.3  | 5.3  | 5.2  | 4.4  | 4.4  | 4.4  | 4.5   |
| 90.               | 4.9  | 4.9  | 4.8  | 4.3  | 5.0  | 4.8  | 4.6  | 4.6  | 4.6  | 4.8   |
| 100.              | 4.5  | 4.5  | 4.6  | 4.3  | 4.6  | 4.5  | 4.9  | 4.8  | 4.7  | 5.2   |
| 110.              | 4.3  | 4.4  | 4.5  | 4.3  | 4.4  | 4.4  | 5.1  | 4.9  | 4.7  | 5.3   |
| 120.              | 4.3  | 4.3  | 4.3  | 4.3  | 4.3  | 4.3  | 5.2  | 4.7  | 4.7  | 5.3   |
| 130.              | 4.3  | 4.3  | 4.3  | 4.3  | 4.3  | 4.3  | 5.2  | 4.7  | 4.6  | 5.3   |
| 140.              | 4.3  | 4.3  | 4.3  | 4.3  | 4.3  | 4.3  | 5.1  | 4.7  | 4.6  | 5.3   |
| 150.              | 4.3  | 4.4  | 4.3  | 4.3  | 4.3  | 4.3  | 5.1  | 4.7  | 4.8  | 5.2   |
| 160.              | 4.3  | 4.5  | 4.3  | 4.3  | 4.3  | 4.3  | 4.9  | 4.6  | 4.7  | 5.2   |
| 170.              | 4.3  | 4.4  | 4.3  | 4.3  | 4.3  | 4.3  | 5.1  | 4.6  | 5.0  | 5.3   |
| 180.              | 4.3  | 4.4  | 4.3  | 4.3  | 4.5  | 4.3  | 5.1  | 4.7  | 5.1  | 5.2   |
| 190.              | 4.3  | 4.3  | 4.3  | 4.3  | 4.5  | 4.3  | 5.2  | 4.6  | 5.1  | 5.1   |
| 200.              | 4.3  | 4.3  | 4.3  | 4.3  | 4.4  | 4.3  | 5.2  | 4.4  | 5.1  | 5.1   |
| 210.              | 4.3  | 4.3  | 4.3  | 4.3  | 4.3  | 4.3  | 5.2  | 4.4  | 5.1  | 5.1   |
| 220.              | 4.3  | 4.3  | 4.3  | 4.3  | 4.3  | 4.3  | 5.2  | 4.5  | 5.2  | 5.2   |
| 230.              | 4.3  | 4.3  | 4.3  | 4.4  | 4.3  | 4.4  | 5.1  | 4.7  | 5.3  | 5.3   |
| 240.              | 4.3  | 4.3  | 4.3  | 4.6  | 4.3  | 4.3  | 5.0  | 4.8  | 5.4  | 5.3   |
| 250.              | 4.4  | 4.3  | 4.3  | 4.7  | 4.3  | 4.4  | 4.9  | 5.1  | 5.3  | 5.2   |
| 260.              | 4.5  | 4.5  | 4.3  | 5.1  | 4.5  | 4.6  | 4.9  | 5.0  | 5.3  | 4.9   |
| 270.              | 4.7  | 4.8  | 4.3  | 5.3  | 4.8  | 5.0  | 4.7  | 4.9  | 4.9  | 4.7   |
| 280.              | 5.1  | 5.1  | 4.3  | 5.5  | 5.1  | 5.3  | 4.5  | 4.6  | 4.5  | 4.4   |
| 290.              | 5.3  | 5.3  | 4.3  | 5.7  | 5.1  | 5.3  | 4.3  | 4.3  | 4.4  | 4.3   |
| 300.              | 5.3  | 5.2  | 4.4  | 5.9  | 4.9  | 5.2  | 4.3  | 4.3  | 4.3  | 4.3   |
| 310.              | 5.2  | 5.1  | 4.5  | 6.0  | 4.8  | 5.3  | 4.3  | 4.3  | 4.3  | 4.3   |
| 320.              | 5.2  | 5.1  | 4.6  | 5.7  | 4.7  | 5.4  | 4.3  | 4.3  | 4.3  | 4.3   |
| 330.              | 5.1  | 5.0  | 4.5  | 5.5  | 4.5  | 5.3  | 4.3  | 4.3  | 4.3  | 4.3   |
| 340.              | 5.1  | 5.0  | 4.5  | 5.2  | 4.7  | 5.3  | 4.3  | 4.3  | 4.3  | 4.3   |
| 350.              | 5.1  | 5.0  | 4.5  | 4.7  | 4.8  | 5.4  | 4.3  | 4.3  | 4.3  | 4.3   |
| 360.              | 5.1  | 5.0  | 4.4  | 4.5  | 4.9  | 5.3  | 4.3  | 4.3  | 4.3  | 4.3   |
| MAX               | 5.4  | 5.3  | 5.1  | 6.0  | 5.4  | 5.4  | 5.2  | 5.1  | 5.4  | 5.3   |
| DEGR.             | 70   | 290  | 60   | 310  | 70   | 60   | 120  | 250  | 240  | 110   |

THE HIGHEST CONCENTRATION OF 6.00 PPM OCCURRED AT RECEPTOR REC4 .





JOB: GristMillGlover2030BuildPM

RUN: GristMillGlover2030BuildPM

DATE : 4/15/11  
 TIME : 13:24:26

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S      VD = .0 CM/S      Z0 = 175. CM  
 U = 1.0 M/S      CLAS = 4 (D)      ATIM = 60. MINUTES      MIXH = 1000. M      AMB = 4.3 PPM

LINK VARIABLES

| LINK DESCRIPTION     | *<br>*<br>* | X1    | LINK COORDINATES (FT) |       | *<br>*<br>* | LENGTH<br>(FT) | BRG TYPE<br>(DEG) | VPH   | EF<br>(G/MI) | H<br>(FT) | W<br>(FT) | V/C  | QUEUE<br>(VEH) |
|----------------------|-------------|-------|-----------------------|-------|-------------|----------------|-------------------|-------|--------------|-----------|-----------|------|----------------|
|                      |             |       | Y1                    | X2    | Y2          |                |                   |       |              |           |           |      |                |
| 1. Grist Mill EB in  | *<br>*<br>* | .0    | 418.0                 | 200.0 | 418.0       | 200.           | 90. AG            | 1599. | 8.3          | .0        | 36.0      |      |                |
| 2. Grist Mill EB T   | *<br>*<br>* | 200.0 | 424.0                 | 383.8 | 424.0       | 184.           | 90. AG            | 302.  | 100.0        | .0        | 24.0      | .44  | 9.3            |
| 3. Grist Mill EB R   | *<br>*<br>* | 200.0 | 406.0                 | 207.7 | 406.0       | 8.             | 90. AG            | 69.   | 100.0        | .0        | 12.0      | .06  | .4             |
| 4. Grist Mill EB out | *<br>*<br>* | 454.0 | 412.0                 | 848.0 | 412.0       | 394.           | 90. AG            | 1599. | 8.3          | .0        | 24.0      |      |                |
| 5. Grist Mill WB in  | *<br>*<br>* | 848.0 | 442.0                 | 648.0 | 442.0       | 200.           | 270. AG           | 1685. | 8.3          | .0        | 36.0      |      |                |
| 6. Grist Mill WB L   | *<br>*<br>* | 648.0 | 430.0                 | 633.1 | 430.0       | 15.            | 270. AG           | 275.  | 100.0        | .0        | 12.0      | .13  | .8             |
| 7. Grist Mill WB T   | *<br>*<br>* | 648.0 | 448.0                 | 539.7 | 448.0       | 108.           | 270. AG           | 165.  | 100.0        | .0        | 24.0      | .34  | 5.5            |
| 8. Grist Mill WB out | *<br>*<br>* | 406.0 | 448.0                 | .0    | 448.0       | 406.           | 270. AG           | 1685. | 8.3          | .0        | 24.0      |      |                |
| 9. Glover NB in      | *<br>*<br>* | 442.0 | .0                    | 442.0 | 196.0       | 196.           | 360. AG           | 547.  | 8.3          | .0        | 24.0      |      |                |
| 10. Glover NB L      | *<br>*<br>* | 436.0 | 196.0                 | 436.0 | 405.8       | 210.           | 360. AG           | 261.  | 100.0        | .0        | 12.0      | .87  | 10.7           |
| 11. Glover NB LR     | *<br>*<br>* | 448.0 | 196.0                 | 448.0 | 375.7       | 180.           | 360. AG           | 261.  | 100.0        | .0        | 12.0      | 1.08 | 9.1            |
| 12. Glover SB out    | *<br>*<br>* | 418.0 | 400.0                 | 418.0 | .0          | 400.           | 180. AG           | 547.  | 8.3          | .0        | 24.0      |      |                |

DATE : 4/15/11  
 TIME : 13:24:26

-----  
 ADDITIONAL QUEUE LINK PARAMETERS  
 -----

| LINK DESCRIPTION   | *<br>* | CYCLE<br>LENGTH<br>(SEC) | RED<br>TIME<br>(SEC) | CLEARANCE<br>LOST TIME<br>(SEC) | APPROACH<br>VOL<br>(VPH) | SATURATION<br>FLOW RATE<br>(VPH) | IDLE<br>EM FAC<br>(gm/hr) | SIGNAL<br>TYPE | ARRIVAL<br>RATE |
|--------------------|--------|--------------------------|----------------------|---------------------------------|--------------------------|----------------------------------|---------------------------|----------------|-----------------|
| 2. Grist Mill EB T | *      | 100                      | 44                   | 5.0                             | 1529                     | 3573                             | 127.94                    | 3              | 4               |
| 3. Grist Mill EB R | *      | 100                      | 20                   | 5.0                             | 70                       | 1599                             | 127.94                    | 3              | 4               |
| 6. Grist Mill WB L | *      | 100                      | 80                   | 3.0                             | 34                       | 1734                             | 127.94                    | 3              | 4               |
| 7. Grist Mill WB T | *      | 100                      | 24                   | 5.0                             | 1651                     | 3467                             | 127.94                    | 3              | 4               |
| 10. Glover NB L    | *      | 100                      | 76                   | 5.0                             | 434                      | 2929                             | 127.94                    | 3              | 3               |
| 11. Glover NB LR   | *      | 100                      | 76                   | 5.0                             | 113                      | 621                              | 127.94                    | 3              | 3               |

-----  
 RECEPTOR LOCATIONS  
 -----

| RECEPTOR          | *<br>* | X     | COORDINATES (FT)<br>Y | Z   | *<br>* |
|-------------------|--------|-------|-----------------------|-----|--------|
| 1. EB W Midblock  | *      | 196.0 | 390.0                 | 6.0 | *      |
| 2. SW Corner      | *      | 394.0 | 390.0                 | 6.0 | *      |
| 3. SB S Midblock  | *      | 394.0 | 200.0                 | 6.0 | *      |
| 4. NB S Midblock  | *      | 464.0 | 200.0                 | 6.0 | *      |
| 5. SE Corner      | *      | 464.0 | 390.0                 | 6.0 | *      |
| 6. EB E Midblock  | *      | 648.0 | 390.0                 | 6.0 | *      |
| 7. WB E Midblock  | *      | 648.0 | 470.0                 | 6.0 | *      |
| 8. NE Corner      | *      | 464.0 | 470.0                 | 6.0 | *      |
| 9. NW Corner      | *      | 396.0 | 470.0                 | 6.0 | *      |
| 10. WB W Midblock | *      | 196.0 | 470.0                 | 6.0 | *      |

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

| WIND ANGLE (DEGR) | REC1 | REC2 | REC3 | REC4 | REC5 | REC6 | REC7 | REC8 | REC9 | REC10 |
|-------------------|------|------|------|------|------|------|------|------|------|-------|
| 0.                | 5.0  | 4.6  | 4.8  | 5.2  | 4.6  | 5.1  | 4.3  | 4.3  | 4.3  | 4.3   |
| 10.               | 5.2  | 4.4  | 4.9  | 4.8  | 4.7  | 5.1  | 4.3  | 4.3  | 4.3  | 4.3   |
| 20.               | 5.2  | 4.4  | 5.3  | 4.6  | 4.7  | 5.0  | 4.3  | 4.3  | 4.3  | 4.3   |
| 30.               | 5.3  | 4.3  | 5.5  | 4.5  | 4.7  | 5.0  | 4.3  | 4.3  | 4.3  | 4.3   |
| 40.               | 5.3  | 4.3  | 5.5  | 4.5  | 4.8  | 5.0  | 4.3  | 4.3  | 4.3  | 4.3   |
| 50.               | 5.4  | 4.5  | 5.4  | 4.5  | 4.9  | 5.1  | 4.3  | 4.3  | 4.3  | 4.3   |
| 60.               | 5.3  | 4.6  | 5.4  | 4.4  | 5.0  | 5.1  | 4.3  | 4.3  | 4.3  | 4.3   |
| 70.               | 5.3  | 5.1  | 5.1  | 4.3  | 5.1  | 5.1  | 4.3  | 4.3  | 4.3  | 4.3   |
| 80.               | 5.1  | 5.2  | 5.0  | 4.3  | 5.0  | 4.9  | 4.4  | 4.5  | 4.4  | 4.4   |
| 90.               | 4.9  | 5.4  | 4.8  | 4.3  | 4.8  | 4.7  | 4.6  | 4.7  | 4.6  | 4.9   |
| 100.              | 4.7  | 5.1  | 4.8  | 4.3  | 4.5  | 4.4  | 4.8  | 4.8  | 4.7  | 5.3   |
| 110.              | 4.5  | 5.0  | 4.7  | 4.3  | 4.4  | 4.3  | 5.0  | 4.9  | 4.6  | 5.6   |
| 120.              | 4.5  | 5.1  | 4.5  | 4.3  | 4.3  | 4.3  | 5.0  | 4.7  | 4.5  | 5.6   |
| 130.              | 4.5  | 5.1  | 4.5  | 4.3  | 4.3  | 4.3  | 5.0  | 4.5  | 4.7  | 5.6   |
| 140.              | 4.3  | 5.4  | 4.5  | 4.3  | 4.3  | 4.3  | 4.9  | 4.5  | 4.8  | 5.5   |
| 150.              | 4.3  | 5.4  | 4.6  | 4.3  | 4.3  | 4.3  | 4.9  | 4.5  | 5.0  | 5.2   |
| 160.              | 4.3  | 5.2  | 4.6  | 4.3  | 4.4  | 4.3  | 4.9  | 4.6  | 5.3  | 5.1   |
| 170.              | 4.3  | 5.0  | 4.5  | 4.3  | 4.7  | 4.3  | 5.0  | 4.8  | 5.2  | 5.2   |
| 180.              | 4.3  | 4.6  | 4.4  | 4.4  | 5.2  | 4.3  | 5.1  | 5.2  | 5.2  | 5.1   |
| 190.              | 4.3  | 4.4  | 4.3  | 4.5  | 5.7  | 4.3  | 5.1  | 5.2  | 5.0  | 5.0   |
| 200.              | 4.3  | 4.3  | 4.3  | 4.6  | 5.8  | 4.3  | 5.2  | 5.1  | 5.0  | 5.0   |
| 210.              | 4.3  | 4.3  | 4.3  | 4.6  | 5.7  | 4.3  | 5.2  | 4.7  | 5.2  | 5.0   |
| 220.              | 4.3  | 4.3  | 4.3  | 4.5  | 5.5  | 4.4  | 5.3  | 4.5  | 5.3  | 5.0   |
| 230.              | 4.3  | 4.3  | 4.3  | 4.6  | 5.2  | 4.5  | 5.3  | 4.6  | 5.4  | 5.1   |
| 240.              | 4.3  | 4.3  | 4.3  | 4.7  | 5.1  | 4.5  | 5.3  | 4.8  | 5.4  | 5.1   |
| 250.              | 4.3  | 4.3  | 4.3  | 4.9  | 5.0  | 4.5  | 5.3  | 5.0  | 5.6  | 5.0   |
| 260.              | 4.4  | 4.5  | 4.3  | 5.1  | 5.0  | 4.7  | 5.0  | 5.2  | 5.3  | 4.9   |
| 270.              | 4.5  | 4.8  | 4.3  | 5.2  | 5.4  | 5.0  | 4.7  | 4.9  | 5.0  | 4.7   |
| 280.              | 4.8  | 5.2  | 4.3  | 5.4  | 5.5  | 4.9  | 4.6  | 4.6  | 4.5  | 4.4   |
| 290.              | 5.0  | 5.5  | 4.3  | 5.6  | 5.4  | 5.1  | 4.3  | 4.4  | 4.4  | 4.3   |
| 300.              | 5.0  | 5.4  | 4.4  | 5.8  | 5.1  | 5.0  | 4.3  | 4.3  | 4.3  | 4.3   |
| 310.              | 5.1  | 5.3  | 4.6  | 5.8  | 4.9  | 5.0  | 4.3  | 4.3  | 4.3  | 4.3   |
| 320.              | 4.9  | 5.1  | 4.5  | 6.1  | 4.6  | 5.1  | 4.3  | 4.3  | 4.3  | 4.3   |
| 330.              | 4.9  | 5.0  | 4.6  | 6.2  | 4.5  | 5.1  | 4.3  | 4.3  | 4.3  | 4.3   |
| 340.              | 4.8  | 4.9  | 4.6  | 6.1  | 4.5  | 5.1  | 4.3  | 4.3  | 4.3  | 4.3   |
| 350.              | 4.9  | 4.8  | 4.5  | 5.7  | 4.6  | 5.2  | 4.3  | 4.3  | 4.3  | 4.3   |
| 360.              | 5.0  | 4.6  | 4.8  | 5.2  | 4.6  | 5.1  | 4.3  | 4.3  | 4.3  | 4.3   |
| MAX               | 5.4  | 5.5  | 5.5  | 6.2  | 5.8  | 5.2  | 5.3  | 5.2  | 5.6  | 5.6   |
| DEGR.             | 50   | 290  | 30   | 330  | 200  | 350  | 220  | 180  | 250  | 110   |

THE HIGHEST CONCENTRATION OF 6.20 PPM OCCURRED AT RECEPTOR REC4 .

DATE : 4/15/11  
 TIME : 13:24:26

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING  
 THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

| LINK # | * | CO/LINK (PPM) |      |      |      |      |      |      |      |      |       |
|--------|---|---------------|------|------|------|------|------|------|------|------|-------|
|        |   | REC1          | REC2 | REC3 | REC4 | REC5 | REC6 | REC7 | REC8 | REC9 | REC10 |
| *      | * | 50            | 290  | 30   | 330  | 200  | 350  | 220  | 180  | 250  | 110   |
| 1      | * | .0            | .1   | .0   | .0   | .0   | .0   | .0   | .0   | .1   | .0    |
| 2      | * | .8            | .8   | .0   | .2   | .0   | .0   | .0   | .0   | .6   | .5    |
| 3      | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    |
| 4      | * | .0            | .0   | .1   | .0   | .0   | .4   | .2   | .2   | .0   | .1    |
| 5      | * | .0            | .0   | .0   | .0   | .0   | .1   | .0   | .0   | .0   | .0    |
| 6      | * | .0            | .0   | .0   | .0   | .0   | .2   | .1   | .0   | .0   | .0    |
| 7      | * | .0            | .0   | .0   | .0   | .0   | .2   | .5   | .0   | .0   | .0    |
| 8      | * | .3            | .3   | .0   | .1   | .0   | .0   | .0   | .0   | .6   | .5    |
| 9      | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    |
| 10     | * | .0            | .0   | .5   | .6   | .6   | .0   | .1   | .3   | .0   | .1    |
| 11     | * | .0            | .0   | .4   | .9   | .8   | .0   | .1   | .3   | .0   | .1    |
| 12     | * | .0            | .0   | .2   | .1   | .1   | .0   | .0   | .1   | .0   | .0    |

JOB: GristMillGlover2030MitigatedBuildAM

RUN: GristMillGlover2030MitigatedBuildAM

DATE : 4/15/11  
 TIME : 13:25:57

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S      VD = .0 CM/S      Z0 = 175. CM  
 U = 1.0 M/S      CLAS = 4 (D)      ATIM = 60. MINUTES      MIXH = 1000. M      AMB = 4.3 PPM

LINK VARIABLES

| LINK DESCRIPTION     | *<br>*<br>* | X1    | LINK COORDINATES (FT) |       | *<br>*<br>* | LENGTH<br>(FT) | BRG TYPE<br>(DEG) | VPH   | EF<br>(G/MI) | H<br>(FT) | W<br>(FT) | V/C | QUEUE<br>(VEH) |
|----------------------|-------------|-------|-----------------------|-------|-------------|----------------|-------------------|-------|--------------|-----------|-----------|-----|----------------|
|                      |             |       | Y1                    | X2    | Y2          |                |                   |       |              |           |           |     |                |
| 1. Grist Mill EB in  | *<br>*<br>* | .0    | 418.0                 | 200.0 | 418.0       | 200.           | 90. AG            | 2585. | 8.3          | .0        | 36.0      |     |                |
| 2. Grist Mill EB T   | *<br>*<br>* | 200.0 | 424.0                 | 415.3 | 424.0       | 215.           | 90. AG            | 231.  | 100.0        | .0        | 24.0      | .50 | 10.9           |
| 3. Grist Mill EB R   | *<br>*<br>* | 200.0 | 406.0                 | 260.0 | 406.0       | 60.            | 90. AG            | 75.   | 100.0        | .0        | 12.0      | .40 | 3.0            |
| 4. Grist Mill EB out | *<br>*<br>* | 454.0 | 412.0                 | 848.0 | 412.0       | 394.           | 90. AG            | 2585. | 8.3          | .0        | 24.0      |     |                |
| 5. Grist Mill WB in  | *<br>*<br>* | 848.0 | 442.0                 | 648.0 | 442.0       | 200.           | 270. AG           | 1596. | 8.3          | .0        | 36.0      |     |                |
| 6. Grist Mill WB L   | *<br>*<br>* | 648.0 | 430.0                 | 611.3 | 430.0       | 37.            | 270. AG           | 268.  | 100.0        | .0        | 12.0      | .27 | 1.9            |
| 7. Grist Mill WB T   | *<br>*<br>* | 648.0 | 448.0                 | 594.0 | 448.0       | 54.            | 270. AG           | 81.   | 100.0        | .0        | 24.0      | .27 | 2.7            |
| 8. Grist Mill WB out | *<br>*<br>* | 406.0 | 448.0                 | .0    | 448.0       | 406.           | 270. AG           | 1596. | 8.3          | .0        | 24.0      |     |                |
| 9. Glover NB in      | *<br>*<br>* | 442.0 | .0                    | 442.0 | 196.0       | 196.           | 360. AG           | 138.  | 8.3          | .0        | 24.0      |     |                |
| 10. Glover NB L      | *<br>*<br>* | 436.0 | 196.0                 | 436.0 | 256.5       | 60.            | 360. AG           | 303.  | 100.0        | .0        | 12.0      | .72 | 3.1            |
| 11. Glover NB LR     | *<br>*<br>* | 448.0 | 196.0                 | 448.0 | 229.3       | 33.            | 360. AG           | 303.  | 100.0        | .0        | 12.0      | .86 | 1.7            |
| 12. Glover SB out    | *<br>*<br>* | 418.0 | 400.0                 | 418.0 | .0          | 400.           | 180. AG           | 138.  | 8.3          | .0        | 24.0      |     |                |

DATE : 4/15/11  
 TIME : 13:25:57

-----  
 ADDITIONAL QUEUE LINK PARAMETERS  
 -----

| LINK DESCRIPTION   | *<br>* | CYCLE<br>LENGTH<br>(SEC) | RED<br>TIME<br>(SEC) | CLEARANCE<br>LOST TIME<br>(SEC) | APPROACH<br>VOL<br>(VPH) | SATURATION<br>FLOW RATE<br>(VPH) | IDLE<br>EM FAC<br>(gm/hr) | SIGNAL<br>TYPE | ARRIVAL<br>RATE |
|--------------------|--------|--------------------------|----------------------|---------------------------------|--------------------------|----------------------------------|---------------------------|----------------|-----------------|
| 2. Grist Mill EB T | *      | 110                      | 37                   | 5.0                             | 2128                     | 3540                             | 127.94                    | 3              | 4               |
| 3. Grist Mill EB R | *      | 110                      | 24                   | 5.0                             | 457                      | 1584                             | 127.94                    | 3              | 4               |
| 6. Grist Mill WB L | *      | 110                      | 86                   | 3.0                             | 78                       | 1702                             | 127.94                    | 3              | 4               |
| 7. Grist Mill WB T | *      | 110                      | 13                   | 5.0                             | 1518                     | 3403                             | 127.94                    | 3              | 4               |
| 10. Glover NB L    | *      | 110                      | 97                   | 5.0                             | 102                      | 2610                             | 127.94                    | 3              | 3               |
| 11. Glover NB LR   | *      | 110                      | 97                   | 5.0                             | 36                       | 776                              | 127.94                    | 3              | 3               |

-----  
 RECEPTOR LOCATIONS  
 -----

| RECEPTOR          | *<br>* | X     | COORDINATES (FT)<br>Y | Z   | *<br>* |
|-------------------|--------|-------|-----------------------|-----|--------|
| 1. EB W Midblock  | *      | 196.0 | 390.0                 | 6.0 | *      |
| 2. SW Corner      | *      | 394.0 | 390.0                 | 6.0 | *      |
| 3. SB S Midblock  | *      | 394.0 | 200.0                 | 6.0 | *      |
| 4. NB S Midblock  | *      | 464.0 | 200.0                 | 6.0 | *      |
| 5. SE Corner      | *      | 464.0 | 390.0                 | 6.0 | *      |
| 6. EB E Midblock  | *      | 648.0 | 390.0                 | 6.0 | *      |
| 7. WB E Midblock  | *      | 648.0 | 470.0                 | 6.0 | *      |
| 8. NE Corner      | *      | 464.0 | 470.0                 | 6.0 | *      |
| 9. NW Corner      | *      | 396.0 | 470.0                 | 6.0 | *      |
| 10. WB W Midblock | *      | 196.0 | 470.0                 | 6.0 | *      |

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

| WIND ANGLE (DEGR) | REC1 | REC2 | REC3 | REC4 | REC5 | REC6 | REC7 | REC8 | REC9 | REC10 |
|-------------------|------|------|------|------|------|------|------|------|------|-------|
| 0.                | 5.1  | 5.0  | 4.4  | 4.5  | 4.9  | 5.3  | 4.3  | 4.3  | 4.3  | 4.3   |
| 10.               | 5.2  | 4.9  | 4.5  | 4.4  | 4.9  | 5.2  | 4.3  | 4.3  | 4.3  | 4.3   |
| 20.               | 5.2  | 4.8  | 4.5  | 4.4  | 4.9  | 5.1  | 4.3  | 4.3  | 4.3  | 4.3   |
| 30.               | 5.3  | 4.6  | 4.6  | 4.5  | 4.9  | 5.2  | 4.3  | 4.3  | 4.3  | 4.3   |
| 40.               | 5.3  | 4.5  | 4.8  | 4.6  | 5.0  | 5.3  | 4.3  | 4.3  | 4.3  | 4.3   |
| 50.               | 5.3  | 4.5  | 5.0  | 4.5  | 5.0  | 5.3  | 4.3  | 4.3  | 4.3  | 4.3   |
| 60.               | 5.3  | 4.5  | 5.1  | 4.4  | 5.1  | 5.4  | 4.3  | 4.3  | 4.3  | 4.3   |
| 70.               | 5.4  | 4.8  | 5.1  | 4.3  | 5.4  | 5.3  | 4.3  | 4.3  | 4.3  | 4.3   |
| 80.               | 5.1  | 4.9  | 5.0  | 4.3  | 5.3  | 5.2  | 4.4  | 4.4  | 4.4  | 4.5   |
| 90.               | 4.9  | 4.9  | 4.8  | 4.3  | 5.0  | 4.8  | 4.6  | 4.6  | 4.6  | 4.8   |
| 100.              | 4.5  | 4.5  | 4.6  | 4.3  | 4.6  | 4.5  | 4.9  | 4.8  | 4.7  | 5.2   |
| 110.              | 4.3  | 4.4  | 4.5  | 4.3  | 4.4  | 4.4  | 5.1  | 4.9  | 4.7  | 5.3   |
| 120.              | 4.3  | 4.3  | 4.3  | 4.3  | 4.3  | 4.3  | 5.2  | 4.7  | 4.7  | 5.3   |
| 130.              | 4.3  | 4.3  | 4.3  | 4.3  | 4.3  | 4.3  | 5.2  | 4.7  | 4.6  | 5.3   |
| 140.              | 4.3  | 4.3  | 4.3  | 4.3  | 4.3  | 4.3  | 5.1  | 4.7  | 4.6  | 5.3   |
| 150.              | 4.3  | 4.4  | 4.3  | 4.3  | 4.3  | 4.3  | 5.1  | 4.7  | 4.8  | 5.2   |
| 160.              | 4.3  | 4.5  | 4.3  | 4.3  | 4.3  | 4.3  | 4.9  | 4.6  | 4.7  | 5.2   |
| 170.              | 4.3  | 4.4  | 4.3  | 4.3  | 4.3  | 4.3  | 5.1  | 4.6  | 5.0  | 5.3   |
| 180.              | 4.3  | 4.4  | 4.3  | 4.3  | 4.5  | 4.3  | 5.1  | 4.7  | 5.1  | 5.2   |
| 190.              | 4.3  | 4.3  | 4.3  | 4.3  | 4.5  | 4.3  | 5.2  | 4.6  | 5.1  | 5.1   |
| 200.              | 4.3  | 4.3  | 4.3  | 4.3  | 4.4  | 4.3  | 5.2  | 4.4  | 5.1  | 5.1   |
| 210.              | 4.3  | 4.3  | 4.3  | 4.3  | 4.3  | 4.3  | 5.2  | 4.4  | 5.1  | 5.1   |
| 220.              | 4.3  | 4.3  | 4.3  | 4.3  | 4.3  | 4.3  | 5.2  | 4.5  | 5.2  | 5.2   |
| 230.              | 4.3  | 4.3  | 4.3  | 4.4  | 4.3  | 4.4  | 5.1  | 4.7  | 5.3  | 5.3   |
| 240.              | 4.3  | 4.3  | 4.3  | 4.6  | 4.3  | 4.3  | 5.0  | 4.8  | 5.4  | 5.3   |
| 250.              | 4.4  | 4.3  | 4.3  | 4.7  | 4.3  | 4.4  | 4.9  | 5.1  | 5.3  | 5.2   |
| 260.              | 4.5  | 4.5  | 4.3  | 5.1  | 4.5  | 4.6  | 4.9  | 5.0  | 5.3  | 4.9   |
| 270.              | 4.7  | 4.8  | 4.3  | 5.3  | 4.8  | 5.0  | 4.7  | 4.9  | 4.9  | 4.7   |
| 280.              | 5.1  | 5.1  | 4.3  | 5.5  | 5.1  | 5.3  | 4.5  | 4.6  | 4.5  | 4.4   |
| 290.              | 5.3  | 5.3  | 4.3  | 5.7  | 5.1  | 5.3  | 4.3  | 4.3  | 4.4  | 4.3   |
| 300.              | 5.3  | 5.2  | 4.4  | 5.9  | 4.9  | 5.2  | 4.3  | 4.3  | 4.3  | 4.3   |
| 310.              | 5.2  | 5.1  | 4.5  | 6.0  | 4.8  | 5.3  | 4.3  | 4.3  | 4.3  | 4.3   |
| 320.              | 5.2  | 5.1  | 4.6  | 5.7  | 4.7  | 5.4  | 4.3  | 4.3  | 4.3  | 4.3   |
| 330.              | 5.1  | 5.0  | 4.5  | 5.5  | 4.5  | 5.3  | 4.3  | 4.3  | 4.3  | 4.3   |
| 340.              | 5.1  | 5.0  | 4.5  | 5.2  | 4.7  | 5.3  | 4.3  | 4.3  | 4.3  | 4.3   |
| 350.              | 5.1  | 5.0  | 4.5  | 4.7  | 4.8  | 5.4  | 4.3  | 4.3  | 4.3  | 4.3   |
| 360.              | 5.1  | 5.0  | 4.4  | 4.5  | 4.9  | 5.3  | 4.3  | 4.3  | 4.3  | 4.3   |
| MAX               | 5.4  | 5.3  | 5.1  | 6.0  | 5.4  | 5.4  | 5.2  | 5.1  | 5.4  | 5.3   |
| DEGR.             | 70   | 290  | 60   | 310  | 70   | 60   | 120  | 250  | 240  | 110   |

THE HIGHEST CONCENTRATION OF 6.00 PPM OCCURRED AT RECEPTOR REC4 .





JOB: GristMillGlover2030MitigatedBuildPM

RUN: GristMillGlover2030MitigatedBuildPM

DATE : 4/15/11  
 TIME : 13:27:59

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S      VD = .0 CM/S      Z0 = 175. CM  
 U = 1.0 M/S      CLAS = 4 (D)      ATIM = 60. MINUTES      MIXH = 1000. M      AMB = 4.3 PPM

LINK VARIABLES

| LINK DESCRIPTION     | *<br>*<br>* | X1    | LINK COORDINATES (FT) |       | *<br>*<br>* | LENGTH<br>(FT) | BRG TYPE<br>(DEG) | VPH   | EF<br>(G/MI) | H<br>(FT) | W<br>(FT) | V/C  | QUEUE<br>(VEH) |
|----------------------|-------------|-------|-----------------------|-------|-------------|----------------|-------------------|-------|--------------|-----------|-----------|------|----------------|
|                      |             |       | Y1                    | X2    | Y2          |                |                   |       |              |           |           |      |                |
| 1. Grist Mill EB in  | *<br>*<br>* | .0    | 418.0                 | 200.0 | 418.0       | 200.           | 90. AG            | 1599. | 8.3          | .0        | 36.0      |      |                |
| 2. Grist Mill EB T   | *<br>*<br>* | 200.0 | 424.0                 | 383.8 | 424.0       | 184.           | 90. AG            | 302.  | 100.0        | .0        | 24.0      | .44  | 9.3            |
| 3. Grist Mill EB R   | *<br>*<br>* | 200.0 | 406.0                 | 207.7 | 406.0       | 8.             | 90. AG            | 69.   | 100.0        | .0        | 12.0      | .06  | .4             |
| 4. Grist Mill EB out | *<br>*<br>* | 454.0 | 412.0                 | 848.0 | 412.0       | 394.           | 90. AG            | 1599. | 8.3          | .0        | 24.0      |      |                |
| 5. Grist Mill WB in  | *<br>*<br>* | 848.0 | 442.0                 | 648.0 | 442.0       | 200.           | 270. AG           | 1685. | 8.3          | .0        | 36.0      |      |                |
| 6. Grist Mill WB L   | *<br>*<br>* | 648.0 | 430.0                 | 632.9 | 430.0       | 15.            | 270. AG           | 278.  | 100.0        | .0        | 12.0      | .14  | .8             |
| 7. Grist Mill WB T   | *<br>*<br>* | 648.0 | 448.0                 | 535.2 | 448.0       | 113.           | 270. AG           | 172.  | 100.0        | .0        | 24.0      | .35  | 5.7            |
| 8. Grist Mill WB out | *<br>*<br>* | 406.0 | 448.0                 | .0    | 448.0       | 406.           | 270. AG           | 1685. | 8.3          | .0        | 24.0      |      |                |
| 9. Glover NB in      | *<br>*<br>* | 442.0 | .0                    | 442.0 | 196.0       | 196.           | 360. AG           | 547.  | 8.3          | .0        | 24.0      |      |                |
| 10. Glover NB L      | *<br>*<br>* | 436.0 | 196.0                 | 436.0 | 389.9       | 194.           | 360. AG           | 257.  | 100.0        | .0        | 12.0      | .82  | 9.9            |
| 11. Glover NB LR     | *<br>*<br>* | 448.0 | 196.0                 | 448.0 | 314.5       | 119.           | 360. AG           | 257.  | 100.0        | .0        | 12.0      | 1.02 | 6.0            |
| 12. Glover SB out    | *<br>*<br>* | 418.0 | 400.0                 | 418.0 | .0          | 400.           | 180. AG           | 547.  | 8.3          | .0        | 24.0      |      |                |

DATE : 4/15/11  
 TIME : 13:27:59

-----  
 ADDITIONAL QUEUE LINK PARAMETERS  
 -----

| LINK DESCRIPTION   | *<br>* | CYCLE<br>LENGTH<br>(SEC) | RED<br>TIME<br>(SEC) | CLEARANCE<br>LOST TIME<br>(SEC) | APPROACH<br>VOL<br>(VPH) | SATURATION<br>FLOW RATE<br>(VPH) | IDLE<br>EM FAC<br>(gm/hr) | SIGNAL<br>TYPE | ARRIVAL<br>RATE |
|--------------------|--------|--------------------------|----------------------|---------------------------------|--------------------------|----------------------------------|---------------------------|----------------|-----------------|
| 2. Grist Mill EB T | *      | 100                      | 44                   | 5.0                             | 1529                     | 3573                             | 127.94                    | 3              | 4               |
| 3. Grist Mill EB R | *      | 100                      | 20                   | 5.0                             | 70                       | 1599                             | 127.94                    | 3              | 4               |
| 6. Grist Mill WB L | *      | 100                      | 81                   | 3.0                             | 34                       | 1734                             | 127.94                    | 3              | 4               |
| 7. Grist Mill WB T | *      | 100                      | 25                   | 5.0                             | 1651                     | 3467                             | 127.94                    | 3              | 4               |
| 10. Glover NB L    | *      | 100                      | 75                   | 5.0                             | 434                      | 2929                             | 127.94                    | 3              | 3               |
| 11. Glover NB LR   | *      | 100                      | 75                   | 5.0                             | 113                      | 621                              | 127.94                    | 3              | 3               |

-----  
 RECEPTOR LOCATIONS  
 -----

| RECEPTOR          | *<br>* | X     | COORDINATES (FT)<br>Y | Z   | *<br>* |
|-------------------|--------|-------|-----------------------|-----|--------|
| 1. EB W Midblock  | *      | 196.0 | 390.0                 | 6.0 | *      |
| 2. SW Corner      | *      | 394.0 | 390.0                 | 6.0 | *      |
| 3. SB S Midblock  | *      | 394.0 | 200.0                 | 6.0 | *      |
| 4. NB S Midblock  | *      | 464.0 | 200.0                 | 6.0 | *      |
| 5. SE Corner      | *      | 464.0 | 390.0                 | 6.0 | *      |
| 6. EB E Midblock  | *      | 648.0 | 390.0                 | 6.0 | *      |
| 7. WB E Midblock  | *      | 648.0 | 470.0                 | 6.0 | *      |
| 8. NE Corner      | *      | 464.0 | 470.0                 | 6.0 | *      |
| 9. NW Corner      | *      | 396.0 | 470.0                 | 6.0 | *      |
| 10. WB W Midblock | *      | 196.0 | 470.0                 | 6.0 | *      |

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

| WIND ANGLE (DEGR) | REC1 | REC2 | REC3 | REC4 | REC5 | REC6 | REC7 | REC8 | REC9 | REC10 |
|-------------------|------|------|------|------|------|------|------|------|------|-------|
| 0.                | 5.0  | 4.6  | 4.7  | 5.1  | 4.6  | 5.1  | 4.3  | 4.3  | 4.3  | 4.3   |
| 10.               | 5.2  | 4.4  | 4.8  | 4.7  | 4.7  | 5.1  | 4.3  | 4.3  | 4.3  | 4.3   |
| 20.               | 5.2  | 4.4  | 5.2  | 4.6  | 4.7  | 5.1  | 4.3  | 4.3  | 4.3  | 4.3   |
| 30.               | 5.3  | 4.3  | 5.4  | 4.5  | 4.7  | 5.0  | 4.3  | 4.3  | 4.3  | 4.3   |
| 40.               | 5.3  | 4.3  | 5.4  | 4.5  | 4.8  | 5.0  | 4.3  | 4.3  | 4.3  | 4.3   |
| 50.               | 5.4  | 4.4  | 5.3  | 4.5  | 4.9  | 5.1  | 4.3  | 4.3  | 4.3  | 4.3   |
| 60.               | 5.3  | 4.5  | 5.3  | 4.4  | 5.0  | 5.1  | 4.3  | 4.3  | 4.3  | 4.3   |
| 70.               | 5.3  | 4.9  | 5.1  | 4.3  | 5.1  | 5.1  | 4.3  | 4.3  | 4.3  | 4.3   |
| 80.               | 5.1  | 5.0  | 5.0  | 4.3  | 5.0  | 4.9  | 4.4  | 4.5  | 4.4  | 4.4   |
| 90.               | 4.8  | 5.1  | 4.8  | 4.3  | 4.8  | 4.7  | 4.6  | 4.7  | 4.6  | 4.9   |
| 100.              | 4.6  | 4.9  | 4.8  | 4.3  | 4.5  | 4.4  | 4.8  | 4.8  | 4.7  | 5.3   |
| 110.              | 4.5  | 4.7  | 4.7  | 4.3  | 4.4  | 4.3  | 5.0  | 4.9  | 4.6  | 5.5   |
| 120.              | 4.5  | 4.8  | 4.5  | 4.3  | 4.3  | 4.3  | 5.0  | 4.7  | 4.5  | 5.6   |
| 130.              | 4.5  | 4.9  | 4.5  | 4.3  | 4.3  | 4.3  | 5.0  | 4.5  | 4.6  | 5.6   |
| 140.              | 4.3  | 5.1  | 4.5  | 4.3  | 4.3  | 4.3  | 4.9  | 4.5  | 4.6  | 5.5   |
| 150.              | 4.3  | 5.2  | 4.6  | 4.3  | 4.3  | 4.3  | 4.9  | 4.5  | 4.8  | 5.2   |
| 160.              | 4.3  | 5.1  | 4.6  | 4.3  | 4.3  | 4.3  | 5.0  | 4.5  | 5.0  | 5.1   |
| 170.              | 4.3  | 5.0  | 4.5  | 4.3  | 4.5  | 4.3  | 5.1  | 4.7  | 5.1  | 5.2   |
| 180.              | 4.3  | 4.6  | 4.4  | 4.4  | 4.9  | 4.3  | 5.1  | 5.0  | 5.2  | 5.1   |
| 190.              | 4.3  | 4.4  | 4.3  | 4.5  | 5.2  | 4.3  | 5.1  | 4.9  | 5.0  | 5.0   |
| 200.              | 4.3  | 4.3  | 4.3  | 4.6  | 5.2  | 4.3  | 5.2  | 4.9  | 5.0  | 5.0   |
| 210.              | 4.3  | 4.3  | 4.3  | 4.6  | 5.1  | 4.3  | 5.2  | 4.6  | 5.2  | 5.0   |
| 220.              | 4.3  | 4.3  | 4.3  | 4.5  | 5.0  | 4.4  | 5.3  | 4.5  | 5.3  | 5.0   |
| 230.              | 4.3  | 4.3  | 4.3  | 4.6  | 4.9  | 4.5  | 5.3  | 4.6  | 5.4  | 5.1   |
| 240.              | 4.3  | 4.3  | 4.3  | 4.7  | 4.9  | 4.5  | 5.2  | 4.8  | 5.4  | 5.1   |
| 250.              | 4.3  | 4.3  | 4.3  | 4.9  | 4.8  | 4.5  | 5.3  | 5.0  | 5.6  | 5.0   |
| 260.              | 4.4  | 4.5  | 4.3  | 5.1  | 4.8  | 4.6  | 5.0  | 5.2  | 5.3  | 4.9   |
| 270.              | 4.5  | 4.8  | 4.3  | 5.2  | 5.1  | 4.9  | 4.7  | 4.9  | 5.0  | 4.7   |
| 280.              | 4.8  | 5.2  | 4.3  | 5.4  | 5.2  | 4.9  | 4.6  | 4.6  | 4.5  | 4.4   |
| 290.              | 5.0  | 5.5  | 4.3  | 5.6  | 5.1  | 5.1  | 4.3  | 4.4  | 4.4  | 4.3   |
| 300.              | 5.0  | 5.4  | 4.4  | 5.8  | 4.8  | 5.0  | 4.3  | 4.3  | 4.3  | 4.3   |
| 310.              | 5.1  | 5.3  | 4.6  | 5.8  | 4.7  | 5.1  | 4.3  | 4.3  | 4.3  | 4.3   |
| 320.              | 4.9  | 5.1  | 4.5  | 6.1  | 4.5  | 5.1  | 4.3  | 4.3  | 4.3  | 4.3   |
| 330.              | 4.9  | 5.0  | 4.6  | 6.1  | 4.5  | 5.1  | 4.3  | 4.3  | 4.3  | 4.3   |
| 340.              | 4.8  | 4.9  | 4.6  | 6.0  | 4.5  | 5.1  | 4.3  | 4.3  | 4.3  | 4.3   |
| 350.              | 4.9  | 4.8  | 4.5  | 5.6  | 4.6  | 5.2  | 4.3  | 4.3  | 4.3  | 4.3   |
| 360.              | 5.0  | 4.6  | 4.7  | 5.1  | 4.6  | 5.1  | 4.3  | 4.3  | 4.3  | 4.3   |
| MAX               | 5.4  | 5.5  | 5.4  | 6.1  | 5.2  | 5.2  | 5.3  | 5.2  | 5.6  | 5.6   |
| DEGR.             | 50   | 290  | 30   | 320  | 190  | 350  | 220  | 260  | 250  | 120   |

THE HIGHEST CONCENTRATION OF 6.10 PPM OCCURRED AT RECEPTOR REC4 .

DATE : 4/15/11  
 TIME : 13:27:59

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING  
 THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

| LINK # | * | CO/LINK (PPM) |      |      |      |      |      |      |      |      |       |
|--------|---|---------------|------|------|------|------|------|------|------|------|-------|
|        |   | REC1          | REC2 | REC3 | REC4 | REC5 | REC6 | REC7 | REC8 | REC9 | REC10 |
|        | * | 50            | 290  | 30   | 320  | 190  | 350  | 220  | 260  | 250  | 120   |
| 1      | * | .0            | .1   | .0   | .0   | .0   | .0   | .0   | .1   | .1   | .0    |
| 2      | * | .8            | .8   | .0   | .2   | .0   | .0   | .0   | .4   | .6   | .6    |
| 3      | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    |
| 4      | * | .0            | .0   | .1   | .0   | .0   | .4   | .2   | .0   | .0   | .0    |
| 5      | * | .0            | .0   | .0   | .0   | .0   | .1   | .0   | .0   | .0   | .0    |
| 6      | * | .0            | .0   | .0   | .0   | .0   | .2   | .1   | .0   | .0   | .0    |
| 7      | * | .0            | .0   | .0   | .0   | .0   | .2   | .5   | .0   | .0   | .0    |
| 8      | * | .3            | .3   | .0   | .1   | .0   | .0   | .0   | .4   | .6   | .5    |
| 9      | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    |
| 10     | * | .0            | .0   | .5   | .6   | .5   | .0   | .1   | .0   | .0   | .1    |
| 11     | * | .0            | .0   | .3   | .8   | .3   | .0   | .1   | .0   | .0   | .1    |
| 12     | * | .0            | .0   | .2   | .1   | .1   | .0   | .0   | .0   | .0   | .0    |

JOB: Route7Bridge2010ExistingAM

RUN: Route7Bridge2010ExistingAM

DATE : 4/ 7/11  
 TIME : 21:32:46

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S      VD = .0 CM/S      Z0 = 175. CM  
 U = 1.0 M/S      CLAS = 4 (D)      ATIM = 60. MINUTES      MIXH = 1000. M      AMB = 4.3 PPM

LINK VARIABLES

| LINK DESCRIPTION    | *<br>* X1 | LINK COORDINATES (FT)<br>Y1 | X2    | Y2    | *<br>* | LENGTH<br>(FT) | BRG TYPE<br>(DEG) | VPH   | EF<br>(G/MI) | H<br>(FT) | W<br>(FT) | V/C | QUEUE<br>(VEH) |
|---------------------|-----------|-----------------------------|-------|-------|--------|----------------|-------------------|-------|--------------|-----------|-----------|-----|----------------|
| 1. Fort Hill EB in  | * .0      | 418.0                       | 200.0 | 418.0 | * *    | 200.           | 90. AG            | 98.   | 11.2         | .0        | 24.0      |     |                |
| 2. Fort Hill EB LT  | * 200.0   | 424.0                       | 242.2 | 424.0 | * *    | 42.            | 90. AG            | 411.  | 100.0        | .0        | 12.0      | .70 | 2.1            |
| 3. Fort Hill EB R   | * 200.0   | 412.0                       | 214.3 | 412.0 | * *    | 14.            | 90. AG            | 381.  | 100.0        | .0        | 12.0      | .16 | .7             |
| 4. Bridge EB out    | * 480.0   | 410.0                       | 848.0 | 410.0 | * *    | 368.           | 90. AG            | 98.   | 11.2         | .0        | 24.0      |     |                |
| 5. Bridge WB in     | * 848.0   | 446.0                       | 648.0 | 446.0 | * *    | 200.           | 270. AG           | 1253. | 11.2         | .0        | 48.0      |     |                |
| 6. Bridge WB L      | * 648.0   | 434.0                       | 444.6 | 434.0 | * *    | 203.           | 270. AG           | 584.  | 100.0        | .0        | 24.0      | .49 | 10.3           |
| 7. Bridge WB T      | * 648.0   | 452.0                       | 619.3 | 452.0 | * *    | 29.            | 270. AG           | 292.  | 100.0        | .0        | 12.0      | .13 | 1.5            |
| 8. Bridge WB R      | * 648.0   | 464.0                       | 611.0 | 464.0 | * *    | 37.            | 270. AG           | 292.  | 100.0        | .0        | 12.0      | .17 | 1.9            |
| 9. Fort Hill WB out | * 406.0   | 442.0                       | .0    | 442.0 | * *    | 406.           | 270. AG           | 1253. | 11.2         | .0        | 24.0      |     |                |
| 10. Route 7 NB in   | * 456.0   | .0                          | 456.0 | 200.0 | * *    | 200.           | 360. AG           | 672.  | 11.2         | .0        | 48.0      |     |                |
| 11. Route 7 NB L    | * 438.0   | 200.0                       | 438.0 | 216.4 | * *    | 16.            | 360. AG           | 423.  | 100.0        | .0        | 12.0      | .42 | .8             |
| 12. Route 7 NB T    | * 456.0   | 200.0                       | 456.0 | 241.9 | * *    | 42.            | 360. AG           | 601.  | 100.0        | .0        | 24.0      | .11 | 2.1            |
| 13. Route 7 NB R    | * 474.0   | 200.0                       | 474.0 | 368.6 | * *    | 169.           | 360. AG           | 301.  | 100.0        | .0        | 12.0      | .77 | 8.6            |
| 14. Route 7 NB out  | * 454.0   | 470.0                       | 454.0 | 836.0 | * *    | 366.           | 360. AG           | 672.  | 11.2         | .0        | 24.0      |     |                |
| 15. Route 7 SB in   | * 430.0   | 836.0                       | 430.0 | 636.0 | * *    | 200.           | 180. AG           | 622.  | 11.2         | .0        | 24.0      |     |                |
| 16. Route 7 SB L    | * 436.0   | 636.0                       | 436.0 | 553.7 | * *    | 82.            | 180. AG           | 394.  | 100.0        | .0        | 12.0      | .76 | 4.2            |
| 17. Route 7 SB TR   | * 424.0   | 636.0                       | 424.0 | 468.4 | * *    | 168.           | 180. AG           | 271.  | 100.0        | .0        | 12.0      | .75 | 8.5            |
| 18. Route 7 SB out  | * 420.0   | 396.0                       | 420.0 | .0    | * *    | 396.           | 180. AG           | 622.  | 11.2         | .0        | 24.0      |     |                |

DATE : 4/ 7/11  
 TIME : 21:32:46

-----  
 ADDITIONAL QUEUE LINK PARAMETERS  
 -----

| LINK DESCRIPTION   | *<br>* | CYCLE<br>LENGTH<br>(SEC) | RED<br>TIME<br>(SEC) | CLEARANCE<br>LOST TIME<br>(SEC) | APPROACH<br>VOL<br>(VPH) | SATURATION<br>FLOW RATE<br>(VPH) | IDLE<br>EM FAC<br>(gm/hr) | SIGNAL<br>TYPE | ARRIVAL<br>RATE |
|--------------------|--------|--------------------------|----------------------|---------------------------------|--------------------------|----------------------------------|---------------------------|----------------|-----------------|
| 2. Fort Hill EB LT | *      | 110                      | 97                   | 5.0                             | 69                       | 1800                             | 173.64                    | 3              | 3               |
| 3. Fort Hill EB R  | *      | 110                      | 90                   | 5.0                             | 29                       | 1537                             | 173.64                    | 3              | 3               |
| 6. Bridge WB L     | *      | 110                      | 69                   | 5.0                             | 1079                     | 3570                             | 173.64                    | 3              | 3               |
| 7. Bridge WB T     | *      | 110                      | 69                   | 5.0                             | 76                       | 1845                             | 173.64                    | 3              | 3               |
| 8. Bridge WB R     | *      | 110                      | 69                   | 5.0                             | 98                       | 1900                             | 173.64                    | 3              | 3               |
| 11. Route 7 NB L   | *      | 110                      | 100                  | 3.0                             | 30                       | 1601                             | 173.64                    | 3              | 3               |
| 12. Route 7 NB T   | *      | 110                      | 71                   | 5.0                             | 217                      | 3310                             | 173.64                    | 3              | 3               |
| 13. Route 7 NB R   | *      | 110                      | 71                   | 5.0                             | 425                      | 1900                             | 173.64                    | 3              | 3               |
| 16. Route 7 SB L   | *      | 110                      | 93                   | 3.0                             | 143                      | 1718                             | 173.64                    | 3              | 3               |
| 17. Route 7 SB TR  | *      | 110                      | 64                   | 5.0                             | 479                      | 1809                             | 173.64                    | 3              | 3               |

-----  
 RECEPTOR LOCATIONS  
 -----

| RECEPTOR          | *<br>* | COORDINATES (FT) |       |     | *<br>* |
|-------------------|--------|------------------|-------|-----|--------|
|                   |        | X                | Y     | Z   |        |
| 1. EB W Midblock  | *      | 196.0            | 384.0 | 6.0 | *      |
| 2. SW Corner      | *      | 394.0            | 384.0 | 6.0 | *      |
| 3. SB S Midblock  | *      | 394.0            | 200.0 | 6.0 | *      |
| 4. NB S Midblock  | *      | 490.0            | 200.0 | 6.0 | *      |
| 5. SE Corner      | *      | 490.0            | 384.0 | 6.0 | *      |
| 6. EB E Midblock  | *      | 648.0            | 384.0 | 6.0 | *      |
| 7. WB E Midblock  | *      | 648.0            | 482.0 | 6.0 | *      |
| 8. NE Corner      | *      | 490.0            | 482.0 | 6.0 | *      |
| 9. NB N Midblock  | *      | 476.0            | 640.0 | 6.0 | *      |
| 10. SB N Midblock | *      | 400.0            | 640.0 | 6.0 | *      |
| 11. NW Corner     | *      | 400.0            | 464.0 | 6.0 | *      |
| 12. WB W Midblock | *      | 196.0            | 464.0 | 6.0 | *      |

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

| WIND ANGLE (DEGR) | REC1 | REC2 | REC3 | REC4 | REC5 | REC6 | REC7 | REC8 | REC9 | REC10 | REC11 | REC12 |
|-------------------|------|------|------|------|------|------|------|------|------|-------|-------|-------|
| 0.                | 4.9  | 4.9  | 4.8  | 5.4  | 5.6  | 5.1  | 4.3  | 4.5  | 4.5  | 4.4   | 5.0   | 4.3   |
| 10.               | 5.2  | 4.9  | 5.1  | 5.0  | 5.3  | 5.0  | 4.3  | 4.3  | 4.4  | 4.6   | 5.3   | 4.3   |
| 20.               | 5.4  | 5.0  | 4.9  | 4.7  | 5.3  | 4.7  | 4.3  | 4.3  | 4.3  | 4.6   | 5.5   | 4.3   |
| 30.               | 5.3  | 4.9  | 5.1  | 4.6  | 5.4  | 4.6  | 4.3  | 4.3  | 4.3  | 4.6   | 5.4   | 4.3   |
| 40.               | 5.5  | 4.9  | 5.3  | 4.5  | 5.4  | 4.6  | 4.3  | 4.3  | 4.3  | 4.6   | 5.2   | 4.3   |
| 50.               | 5.3  | 5.0  | 5.6  | 4.4  | 5.5  | 4.6  | 4.3  | 4.3  | 4.3  | 4.6   | 5.0   | 4.5   |
| 60.               | 5.1  | 5.4  | 5.8  | 4.3  | 5.7  | 4.6  | 4.3  | 4.3  | 4.3  | 4.6   | 4.9   | 4.5   |
| 70.               | 4.9  | 5.5  | 5.8  | 4.3  | 5.4  | 4.5  | 4.3  | 4.3  | 4.3  | 4.6   | 4.9   | 4.5   |
| 80.               | 4.7  | 5.3  | 5.6  | 4.3  | 4.9  | 4.4  | 4.4  | 4.4  | 4.3  | 4.7   | 5.1   | 4.7   |
| 90.               | 4.7  | 5.1  | 5.5  | 4.3  | 4.6  | 4.4  | 4.5  | 4.7  | 4.3  | 4.9   | 5.4   | 5.0   |
| 100.              | 4.5  | 4.7  | 5.2  | 4.3  | 4.3  | 4.3  | 4.7  | 5.1  | 4.3  | 5.2   | 5.8   | 5.1   |
| 110.              | 4.5  | 4.7  | 4.8  | 4.3  | 4.3  | 4.3  | 4.8  | 5.5  | 4.3  | 5.4   | 5.6   | 5.2   |
| 120.              | 4.5  | 4.8  | 4.6  | 4.3  | 4.3  | 4.3  | 4.8  | 5.4  | 4.4  | 5.7   | 5.3   | 5.1   |
| 130.              | 4.4  | 4.8  | 4.7  | 4.3  | 4.3  | 4.3  | 4.7  | 5.5  | 4.5  | 6.0   | 5.0   | 5.4   |
| 140.              | 4.3  | 4.9  | 4.7  | 4.3  | 4.3  | 4.3  | 4.7  | 5.4  | 4.6  | 6.2   | 4.9   | 5.3   |
| 150.              | 4.3  | 5.0  | 4.7  | 4.3  | 4.3  | 4.3  | 4.7  | 5.4  | 4.6  | 6.1   | 4.8   | 5.3   |
| 160.              | 4.3  | 5.0  | 4.6  | 4.3  | 4.4  | 4.3  | 4.9  | 5.4  | 4.7  | 5.9   | 4.9   | 5.4   |
| 170.              | 4.3  | 4.8  | 4.6  | 4.4  | 4.7  | 4.3  | 5.3  | 5.6  | 4.9  | 5.5   | 5.0   | 5.3   |
| 180.              | 4.3  | 4.6  | 4.4  | 4.4  | 5.1  | 4.3  | 5.7  | 5.8  | 4.9  | 5.1   | 4.9   | 5.0   |
| 190.              | 4.3  | 4.4  | 4.3  | 4.5  | 5.6  | 4.3  | 6.1  | 5.9  | 5.2  | 4.5   | 4.8   | 4.9   |
| 200.              | 4.3  | 4.3  | 4.3  | 4.7  | 5.5  | 4.3  | 6.3  | 5.7  | 5.4  | 4.4   | 4.7   | 4.7   |
| 210.              | 4.3  | 4.3  | 4.3  | 4.7  | 5.3  | 4.3  | 6.7  | 5.4  | 5.6  | 4.4   | 4.7   | 4.7   |
| 220.              | 4.3  | 4.3  | 4.3  | 4.6  | 5.0  | 4.5  | 6.6  | 5.1  | 5.7  | 4.5   | 4.7   | 4.7   |
| 230.              | 4.3  | 4.3  | 4.3  | 4.6  | 4.8  | 4.5  | 6.5  | 4.8  | 5.6  | 4.4   | 4.8   | 4.8   |
| 240.              | 4.3  | 4.3  | 4.3  | 4.7  | 4.6  | 4.6  | 6.3  | 4.6  | 5.6  | 4.4   | 4.8   | 4.8   |
| 250.              | 4.3  | 4.3  | 4.3  | 5.0  | 4.5  | 4.5  | 5.8  | 4.8  | 5.4  | 4.3   | 5.0   | 4.8   |
| 260.              | 4.3  | 4.3  | 4.3  | 5.2  | 4.4  | 4.5  | 5.3  | 5.0  | 5.2  | 4.3   | 4.9   | 4.7   |
| 270.              | 4.3  | 4.5  | 4.3  | 5.8  | 4.5  | 4.8  | 4.9  | 4.8  | 4.9  | 4.3   | 4.8   | 4.6   |
| 280.              | 4.4  | 4.6  | 4.3  | 6.2  | 4.6  | 5.0  | 4.7  | 4.9  | 4.8  | 4.3   | 4.5   | 4.4   |
| 290.              | 4.5  | 4.7  | 4.3  | 6.5  | 4.6  | 5.5  | 4.6  | 4.8  | 4.6  | 4.3   | 4.4   | 4.3   |
| 300.              | 4.5  | 4.7  | 4.3  | 6.6  | 4.7  | 5.6  | 4.6  | 4.8  | 4.6  | 4.3   | 4.3   | 4.3   |
| 310.              | 4.6  | 4.6  | 4.4  | 6.4  | 4.9  | 5.8  | 4.6  | 4.9  | 4.6  | 4.3   | 4.3   | 4.3   |
| 320.              | 4.5  | 4.5  | 4.5  | 6.4  | 5.1  | 5.8  | 4.4  | 5.0  | 4.7  | 4.3   | 4.3   | 4.3   |
| 330.              | 4.5  | 4.5  | 4.4  | 6.0  | 5.5  | 5.5  | 4.3  | 5.1  | 4.7  | 4.3   | 4.3   | 4.3   |
| 340.              | 4.5  | 4.5  | 4.4  | 5.9  | 5.7  | 5.6  | 4.3  | 5.1  | 4.7  | 4.3   | 4.3   | 4.3   |
| 350.              | 4.7  | 4.6  | 4.4  | 5.8  | 5.7  | 5.6  | 4.3  | 4.9  | 4.6  | 4.3   | 4.5   | 4.3   |
| 360.              | 4.9  | 4.9  | 4.8  | 5.4  | 5.6  | 5.1  | 4.3  | 4.5  | 4.5  | 4.4   | 5.0   | 4.3   |
| MAX               | 5.5  | 5.5  | 5.8  | 6.6  | 5.7  | 5.8  | 6.7  | 5.9  | 5.7  | 6.2   | 5.8   | 5.4   |
| DEGR.             | 40   | 70   | 60   | 300  | 60   | 310  | 210  | 190  | 220  | 140   | 100   | 130   |

THE HIGHEST CONCENTRATION OF 6.70 PPM OCCURRED AT RECEPTOR REC7 .



DATE : 4/ 7/11  
 TIME : 21:32:46

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING  
 THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

| LINK # | * | CO/LINK (PPM) |      |      |      |      |      |      |      |      |       |       |       |
|--------|---|---------------|------|------|------|------|------|------|------|------|-------|-------|-------|
|        |   | REC1          | REC2 | REC3 | REC4 | REC5 | REC6 | REC7 | REC8 | REC9 | REC10 | REC11 | REC12 |
| *      | * | 40            | 70   | 60   | 300  | 60   | 310  | 210  | 190  | 220  | 140   | 100   | 130   |
| 1      | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 2      | * | .5            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .4    |
| 3      | * | .3            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 4      | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 5      | * | .0            | .1   | .1   | .0   | .1   | .0   | .0   | .0   | .0   | .0    | .1    | .0    |
| 6      | * | .0            | 1.0  | .1   | .0   | 1.1  | 1.2  | 1.1  | 1.1  | .0   | .4    | 1.3   | .0    |
| 7      | * | .0            | .0   | .0   | .0   | .1   | .0   | .4   | .0   | .0   | .0    | .0    | .0    |
| 8      | * | .0            | .0   | .0   | .0   | .1   | .0   | .7   | .0   | .0   | .0    | .0    | .0    |
| 9      | * | .2            | .0   | .0   | .1   | .0   | .0   | .0   | .0   | .1   | .0    | .0    | .5    |
| 10     | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 11     | * | .0            | .0   | .2   | .1   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 12     | * | .0            | .0   | .6   | 1.2  | .0   | .0   | .1   | .1   | .0   | .0    | .0    | .1    |
| 13     | * | .0            | .0   | .3   | .8   | .0   | .0   | .1   | .3   | .0   | .0    | .0    | .1    |
| 14     | * | .0            | .0   | .0   | .0   | .0   | .1   | .0   | .0   | .3   | .1    | .0    | .0    |
| 15     | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 16     | * | .1            | .0   | .0   | .0   | .0   | .1   | .0   | .0   | .6   | .7    | .0    | .0    |
| 17     | * | .1            | .0   | .0   | .0   | .0   | .1   | .0   | .0   | .4   | .7    | .1    | .0    |
| 18     | * | .0            | .1   | .2   | .1   | .0   | .0   | .0   | .1   | .0   | .0    | .0    | .0    |

JOB: Route7Bridge2010ExistingdPM

RUN: Route7Bridge2010ExistingdPM

DATE : 4/ 7/11  
 TIME : 21:50:36

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S      VD = .0 CM/S      Z0 = 175. CM  
 U = 1.0 M/S      CLAS = 4 (D)      ATIM = 60. MINUTES      MIXH = 1000. M      AMB = 4.3 PPM

LINK VARIABLES

| LINK DESCRIPTION    | *<br>* X1 | LINK COORDINATES (FT)<br>Y1 | X2    | Y2     | *<br>* | LENGTH<br>(FT) | BRG TYPE<br>(DEG) | VPH   | EF<br>(G/MI) | H<br>(FT) | W<br>(FT) | V/C  | QUEUE<br>(VEH) |
|---------------------|-----------|-----------------------------|-------|--------|--------|----------------|-------------------|-------|--------------|-----------|-----------|------|----------------|
| 1. Fort Hill EB in  | * .0      | 418.0                       | 200.0 | 418.0  | * *    | 200.           | 90. AG            | 363.  | 11.2         | .0        | 24.0      |      |                |
| 2. Fort Hill EB LT  | * 200.0   | 424.0                       | 476.0 | 424.0  | * *    | 276.           | 90. AG            | 369.  | 100.0        | .0        | 12.0      | 1.01 | 14.0           |
| 3. Fort Hill EB R   | * 200.0   | 412.0                       | 221.6 | 412.0  | * *    | 22.            | 90. AG            | 283.  | 100.0        | .0        | 12.0      | .10  | 1.1            |
| 4. Bridge EB out    | * 480.0   | 410.0                       | 848.0 | 410.0  | * *    | 368.           | 90. AG            | 363.  | 11.2         | .0        | 24.0      |      |                |
| 5. Bridge WB in     | * 848.0   | 446.0                       | 648.0 | 446.0  | * *    | 200.           | 270. AG           | 1103. | 11.2         | .0        | 48.0      |      |                |
| 6. Bridge WB L      | * 648.0   | 434.0                       | 458.5 | 434.0  | * *    | 189.           | 270. AG           | 699.  | 100.0        | .0        | 24.0      | .53  | 9.6            |
| 7. Bridge WB T      | * 648.0   | 452.0                       | 557.4 | 452.0  | * *    | 91.            | 270. AG           | 349.  | 100.0        | .0        | 12.0      | .51  | 4.6            |
| 8. Bridge WB R      | * 648.0   | 464.0                       | 574.7 | 464.0  | * *    | 73.            | 270. AG           | 349.  | 100.0        | .0        | 12.0      | .41  | 3.7            |
| 9. Fort Hill WB out | * 406.0   | 442.0                       | .0    | 442.0  | * *    | 406.           | 270. AG           | 1103. | 11.2         | .0        | 24.0      |      |                |
| 10. Route 7 NB in   | * 456.0   | .0                          | 456.0 | 200.0  | * *    | 200.           | 360. AG           | 1495. | 11.2         | .0        | 48.0      |      |                |
| 11. Route 7 NB L    | * 438.0   | 200.0                       | 438.0 | 375.6  | * *    | 176.           | 360. AG           | 392.  | 100.0        | .0        | 12.0      | .99  | 8.9            |
| 12. Route 7 NB T    | * 456.0   | 200.0                       | 456.0 | 316.9  | * *    | 117.           | 360. AG           | 629.  | 100.0        | .0        | 24.0      | .28  | 5.9            |
| 13. Route 7 NB R    | * 474.0   | 200.0                       | 474.0 | 3295.3 | * *    | 3095.          | 360. AG           | 314.  | 100.0        | .0        | 12.0      | 1.52 | 157.2          |
| 14. Route 7 NB out  | * 454.0   | 470.0                       | 454.0 | 836.0  | * *    | 366.           | 360. AG           | 1495. | 11.2         | .0        | 24.0      |      |                |
| 15. Route 7 SB in   | * 430.0   | 836.0                       | 430.0 | 636.0  | * *    | 200.           | 180. AG           | 678.  | 11.2         | .0        | 24.0      |      |                |
| 16. Route 7 SB L    | * 436.0   | 636.0                       | 436.0 | 483.7  | * *    | 152.           | 180. AG           | 365.  | 100.0        | .0        | 12.0      | .84  | 7.7            |
| 17. Route 7 SB TR   | * 424.0   | 636.0                       | 424.0 | 466.5  | * *    | 170.           | 180. AG           | 287.  | 100.0        | .0        | 12.0      | .69  | 8.6            |
| 18. Route 7 SB out  | * 420.0   | 396.0                       | 420.0 | .0     | * *    | 396.           | 180. AG           | 678.  | 11.2         | .0        | 24.0      |      |                |

DATE : 4/ 7/11  
 TIME : 21:50:36

-----  
 ADDITIONAL QUEUE LINK PARAMETERS  
 -----

| LINK DESCRIPTION   | *<br>* | CYCLE<br>LENGTH<br>(SEC) | RED<br>TIME<br>(SEC) | CLEARANCE<br>LOST TIME<br>(SEC) | APPROACH<br>VOL<br>(VPH) | SATURATION<br>FLOW RATE<br>(VPH) | IDLE<br>EM FAC<br>(gm/hr) | SIGNAL<br>TYPE | ARRIVAL<br>RATE |
|--------------------|--------|--------------------------|----------------------|---------------------------------|--------------------------|----------------------------------|---------------------------|----------------|-----------------|
| 2. Fort Hill EB LT | *      | 120                      | 95                   | 5.0                             | 309                      | 2044                             | 173.64                    | 3              | 3               |
| 3. Fort Hill EB R  | *      | 120                      | 73                   | 5.0                             | 54                       | 1599                             | 173.64                    | 3              | 3               |
| 6. Bridge WB L     | *      | 120                      | 90                   | 5.0                             | 770                      | 3813                             | 173.64                    | 3              | 3               |
| 7. Bridge WB T     | *      | 120                      | 90                   | 5.0                             | 184                      | 1881                             | 173.64                    | 3              | 3               |
| 8. Bridge WB R     | *      | 120                      | 90                   | 5.0                             | 149                      | 1900                             | 173.64                    | 3              | 3               |
| 11. Route 7 NB L   | *      | 120                      | 101                  | 3.0                             | 198                      | 1711                             | 173.64                    | 3              | 3               |
| 12. Route 7 NB T   | *      | 120                      | 81                   | 5.0                             | 529                      | 3538                             | 173.64                    | 3              | 3               |
| 13. Route 7 NB R   | *      | 120                      | 81                   | 5.0                             | 769                      | 1900                             | 173.64                    | 3              | 3               |
| 16. Route 7 SB L   | *      | 120                      | 94                   | 3.0                             | 259                      | 1769                             | 173.64                    | 3              | 3               |
| 17. Route 7 SB TR  | *      | 120                      | 74                   | 5.0                             | 419                      | 1860                             | 173.64                    | 3              | 3               |

-----  
 RECEPTOR LOCATIONS  
 -----

| RECEPTOR          | *<br>* | COORDINATES (FT) |       |     | *<br>* |
|-------------------|--------|------------------|-------|-----|--------|
|                   |        | X                | Y     | Z   |        |
| 1. EB W Midblock  | *      | 196.0            | 384.0 | 6.0 | *      |
| 2. SW corner      | *      | 394.0            | 384.0 | 6.0 | *      |
| 3. SB S Midblock  | *      | 394.0            | 200.0 | 6.0 | *      |
| 4. NB S Midblock  | *      | 490.0            | 200.0 | 6.0 | *      |
| 5. SE corner      | *      | 490.0            | 384.0 | 6.0 | *      |
| 6. EB E Midblock  | *      | 648.0            | 384.0 | 6.0 | *      |
| 7. WB E Midblock  | *      | 648.0            | 482.0 | 6.0 | *      |
| 8. NE corner      | *      | 490.0            | 482.0 | 6.0 | *      |
| 9. NB N Midblock  | *      | 476.0            | 640.0 | 6.0 | *      |
| 10. SB N Midblock | *      | 400.0            | 640.0 | 6.0 | *      |
| 11. NW corner     | *      | 400.0            | 464.0 | 6.0 | *      |
| 12. WB W Midblock | *      | 196.0            | 464.0 | 6.0 | *      |

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

| WIND ANGLE (DEGR)* | REC1 | REC2 | REC3 | REC4 | REC5 | REC6 | REC7 | REC8 | REC9 | REC10 | REC11 | REC12 |
|--------------------|------|------|------|------|------|------|------|------|------|-------|-------|-------|
| 0.                 | 5.1  | 6.0  | 5.6  | 6.6  | 7.3  | 5.7  | 4.5  | 5.8  | 7.7  | 4.9   | 5.4   | 4.4   |
| 10.                | 5.3  | 6.3  | 6.2  | 5.6  | 6.4  | 5.1  | 4.3  | 5.0  | 7.1  | 5.2   | 6.2   | 4.5   |
| 20.                | 5.5  | 6.4  | 6.7  | 5.1  | 5.8  | 4.7  | 4.3  | 4.5  | 6.0  | 5.3   | 6.4   | 4.5   |
| 30.                | 5.8  | 6.0  | 6.9  | 4.8  | 5.8  | 4.6  | 4.3  | 4.3  | 5.3  | 5.2   | 6.5   | 4.5   |
| 40.                | 5.9  | 5.9  | 7.1  | 4.6  | 6.0  | 4.7  | 4.3  | 4.3  | 4.9  | 5.2   | 6.3   | 4.6   |
| 50.                | 5.9  | 5.9  | 6.9  | 4.5  | 6.2  | 4.7  | 4.3  | 4.3  | 4.8  | 5.2   | 6.1   | 4.8   |
| 60.                | 5.9  | 6.3  | 6.5  | 4.3  | 6.3  | 4.7  | 4.3  | 4.3  | 4.7  | 5.2   | 5.9   | 4.8   |
| 70.                | 5.9  | 6.5  | 6.1  | 4.3  | 5.8  | 4.6  | 4.3  | 4.3  | 4.6  | 5.1   | 5.6   | 4.9   |
| 80.                | 5.4  | 6.3  | 5.9  | 4.3  | 5.3  | 4.5  | 4.4  | 4.7  | 4.6  | 5.3   | 5.9   | 5.1   |
| 90.                | 5.2  | 5.7  | 5.7  | 4.3  | 4.7  | 4.4  | 4.5  | 5.0  | 4.6  | 5.4   | 6.2   | 5.7   |
| 100.               | 4.8  | 5.2  | 5.3  | 4.3  | 4.3  | 4.3  | 4.6  | 5.6  | 4.6  | 5.6   | 6.5   | 5.6   |
| 110.               | 4.9  | 5.2  | 5.0  | 4.3  | 4.3  | 4.3  | 4.7  | 6.1  | 4.6  | 5.8   | 6.3   | 6.0   |
| 120.               | 4.9  | 5.4  | 4.8  | 4.3  | 4.3  | 4.3  | 4.8  | 6.0  | 4.8  | 6.5   | 6.1   | 6.0   |
| 130.               | 4.7  | 5.7  | 4.8  | 4.3  | 4.3  | 4.3  | 4.8  | 5.9  | 5.2  | 6.7   | 5.6   | 6.0   |
| 140.               | 4.4  | 6.1  | 4.9  | 4.3  | 4.3  | 4.3  | 4.8  | 5.8  | 5.4  | 7.0   | 5.7   | 5.9   |
| 150.               | 4.4  | 6.4  | 4.9  | 4.3  | 4.3  | 4.3  | 4.7  | 5.7  | 5.9  | 6.9   | 6.1   | 5.5   |
| 160.               | 4.3  | 6.1  | 4.8  | 4.3  | 4.4  | 4.3  | 5.0  | 5.8  | 6.5  | 6.8   | 6.3   | 5.3   |
| 170.               | 4.3  | 5.5  | 4.7  | 4.4  | 4.9  | 4.3  | 5.5  | 6.3  | 7.4  | 6.6   | 6.4   | 5.1   |
| 180.               | 4.3  | 4.9  | 4.5  | 4.6  | 5.7  | 4.3  | 5.9  | 7.2  | 8.6  | 5.6   | 6.1   | 5.0   |
| 190.               | 4.3  | 4.4  | 4.4  | 4.8  | 6.6  | 4.3  | 6.5  | 7.7  | 8.8  | 5.0   | 5.5   | 4.9   |
| 200.               | 4.3  | 4.3  | 4.3  | 5.0  | 7.0  | 4.4  | 6.9  | 7.5  | 8.5  | 4.6   | 5.2   | 4.8   |
| 210.               | 4.3  | 4.3  | 4.3  | 5.0  | 6.7  | 4.5  | 7.6  | 7.0  | 8.0  | 4.6   | 5.3   | 4.8   |
| 220.               | 4.3  | 4.3  | 4.3  | 4.9  | 6.3  | 4.8  | 8.0  | 6.5  | 7.6  | 4.5   | 5.3   | 4.8   |
| 230.               | 4.3  | 4.3  | 4.3  | 4.9  | 6.0  | 5.1  | 8.1  | 6.0  | 7.1  | 4.5   | 5.4   | 4.8   |
| 240.               | 4.3  | 4.3  | 4.3  | 4.9  | 5.8  | 5.1  | 7.8  | 6.1  | 7.0  | 4.4   | 5.5   | 4.9   |
| 250.               | 4.3  | 4.3  | 4.3  | 5.2  | 5.6  | 4.9  | 7.4  | 6.1  | 6.5  | 4.3   | 5.4   | 4.9   |
| 260.               | 4.3  | 4.4  | 4.3  | 5.5  | 5.6  | 5.0  | 6.7  | 6.1  | 6.2  | 4.3   | 5.2   | 4.7   |
| 270.               | 4.3  | 4.6  | 4.3  | 6.0  | 5.8  | 5.3  | 5.8  | 6.3  | 6.1  | 4.3   | 4.8   | 4.6   |
| 280.               | 4.5  | 4.9  | 4.3  | 6.5  | 6.1  | 5.7  | 5.2  | 6.2  | 5.9  | 4.3   | 4.6   | 4.4   |
| 290.               | 4.6  | 5.1  | 4.3  | 6.9  | 6.0  | 6.3  | 4.9  | 6.2  | 5.8  | 4.3   | 4.3   | 4.3   |
| 300.               | 4.6  | 5.2  | 4.3  | 7.3  | 6.2  | 6.6  | 4.8  | 6.4  | 5.9  | 4.3   | 4.3   | 4.3   |
| 310.               | 4.6  | 5.2  | 4.5  | 7.6  | 6.3  | 6.8  | 4.8  | 6.5  | 6.1  | 4.3   | 4.3   | 4.3   |
| 320.               | 4.6  | 5.1  | 4.5  | 7.9  | 6.7  | 6.8  | 4.6  | 6.5  | 6.4  | 4.3   | 4.3   | 4.3   |
| 330.               | 4.6  | 5.1  | 4.6  | 7.9  | 7.1  | 6.8  | 4.7  | 6.7  | 6.9  | 4.3   | 4.3   | 4.3   |
| 340.               | 4.6  | 5.1  | 4.6  | 7.8  | 7.8  | 6.6  | 4.6  | 6.6  | 7.3  | 4.3   | 4.3   | 4.3   |
| 350.               | 4.8  | 5.4  | 4.8  | 7.4  | 7.9  | 6.3  | 4.6  | 6.5  | 7.8  | 4.4   | 4.6   | 4.3   |
| 360.               | 5.1  | 6.0  | 5.6  | 6.6  | 7.3  | 5.7  | 4.5  | 5.8  | 7.7  | 4.9   | 5.4   | 4.4   |
| MAX                | 5.9  | 6.5  | 7.1  | 7.9  | 7.9  | 6.8  | 8.1  | 7.7  | 8.8  | 7.0   | 6.5   | 6.0   |
| DEGR.              | 40   | 70   | 40   | 320  | 350  | 310  | 230  | 190  | 190  | 140   | 30    | 120   |

THE HIGHEST CONCENTRATION OF 8.80 PPM OCCURRED AT RECEPTOR REC9 .

DATE : 4/ 7/11  
 TIME : 21:50:36

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING  
 THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

| LINK # | * | CO/LINK (PPM) |      |      |      |      |      |      |      |      |       |       |       |
|--------|---|---------------|------|------|------|------|------|------|------|------|-------|-------|-------|
|        |   | REC1          | REC2 | REC3 | REC4 | REC5 | REC6 | REC7 | REC8 | REC9 | REC10 | REC11 | REC12 |
| *      | * | 40            | 70   | 40   | 320  | 350  | 310  | 230  | 190  | 190  | 140   | 30    | 120   |
| 1      | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 2      | * | .6            | .3   | .0   | .2   | .2   | .0   | .0   | .2   | .2   | .0    | .0    | .7    |
| 3      | * | .3            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 4      | * | .0            | .1   | .0   | .0   | .1   | .1   | .1   | .0   | .0   | .0    | .0    | .0    |
| 5      | * | .0            | .1   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 6      | * | .0            | 1.1  | .4   | .0   | 1.1  | 1.4  | 1.4  | 1.2  | .2   | .4    | .0    | .0    |
| 7      | * | .0            | .1   | .1   | .0   | .0   | .3   | .7   | .0   | .0   | .1    | .0    | .0    |
| 8      | * | .0            | .1   | .1   | .0   | .0   | .1   | 1.0  | .0   | .0   | .1    | .0    | .0    |
| 9      | * | .2            | .0   | .0   | .1   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .5    |
| 10     | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .1   | .0   | .0    | .0    | .0    |
| 11     | * | .0            | .0   | .7   | .6   | .0   | .0   | .2   | .3   | .1   | .0    | .0    | .2    |
| 12     | * | .0            | .0   | .9   | 1.6  | .0   | .0   | .2   | .4   | .1   | .0    | .0    | .2    |
| 13     | * | .2            | .3   | .4   | 1.0  | 1.4  | .2   | .2   | 1.1  | 2.8  | .4    | .4    | .1    |
| 14     | * | .1            | .0   | .0   | .0   | .3   | .1   | .0   | .0   | .5   | .3    | .3    | .0    |
| 15     | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 16     | * | .1            | .0   | .0   | .0   | .3   | .2   | .0   | .0   | .3   | .7    | .7    | .0    |
| 17     | * | .1            | .0   | .0   | .0   | .2   | .1   | .0   | .0   | .2   | .7    | .8    | .0    |
| 18     | * | .0            | .1   | .2   | .1   | .0   | .0   | .0   | .1   | .1   | .0    | .0    | .0    |

JOB: Route7Bridge2030NoBuildAM

RUN: Route7Bridge2030NoBuildAM

DATE : 4/15/11  
 TIME : 13:36:16

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S      VD = .0 CM/S      Z0 = 175. CM  
 U = 1.0 M/S      CLAS = 4 (D)      ATIM = 60. MINUTES      MIXH = 1000. M      AMB = 4.3 PPM

LINK VARIABLES

| LINK DESCRIPTION    | *<br>* X1 | LINK COORDINATES (FT)<br>Y1 | X2    | Y2    | *<br>* | LENGTH<br>(FT) | BRG TYPE<br>(DEG) | VPH   | EF<br>(G/MI) | H<br>(FT) | W<br>(FT) | V/C | QUEUE<br>(VEH) |
|---------------------|-----------|-----------------------------|-------|-------|--------|----------------|-------------------|-------|--------------|-----------|-----------|-----|----------------|
| 1. Fort Hill EB in  | * .0      | 418.0                       | 200.0 | 418.0 | * *    | 200.           | 90. AG            | 132.  | 8.3          | .0        | 24.0      |     |                |
| 2. Fort Hill EB LT  | * 200.0   | 424.0                       | 284.5 | 424.0 | * *    | 84.            | 90. AG            | 303.  | 100.0        | .0        | 12.0      | .95 | 4.3            |
| 3. Fort Hill EB R   | * 200.0   | 412.0                       | 219.2 | 412.0 | * *    | 19.            | 90. AG            | 281.  | 100.0        | .0        | 12.0      | .22 | 1.0            |
| 4. Bridge EB out    | * 480.0   | 410.0                       | 848.0 | 410.0 | * *    | 368.           | 90. AG            | 132.  | 8.3          | .0        | 24.0      |     |                |
| 5. Bridge WB in     | * 848.0   | 446.0                       | 648.0 | 446.0 | * *    | 200.           | 270. AG           | 1530. | 8.3          | .0        | 48.0      |     |                |
| 6. Bridge WB L      | * 648.0   | 434.0                       | 400.9 | 434.0 | * *    | 247.           | 270. AG           | 431.  | 100.0        | .0        | 24.0      | .59 | 12.6           |
| 7. Bridge WB T      | * 648.0   | 452.0                       | 612.9 | 452.0 | * *    | 35.            | 270. AG           | 215.  | 100.0        | .0        | 12.0      | .16 | 1.8            |
| 8. Bridge WB R      | * 648.0   | 464.0                       | 600.1 | 464.0 | * *    | 48.            | 270. AG           | 215.  | 100.0        | .0        | 12.0      | .22 | 2.4            |
| 9. Fort Hill WB out | * 406.0   | 442.0                       | .0    | 442.0 | * *    | 406.           | 270. AG           | 1530. | 8.3          | .0        | 24.0      |     |                |
| 10. Route 7 NB in   | * 456.0   | .0                          | 456.0 | 200.0 | * *    | 200.           | 360. AG           | 811.  | 8.3          | .0        | 48.0      |     |                |
| 11. Route 7 NB L    | * 438.0   | 200.0                       | 438.0 | 220.9 | * *    | 21.            | 360. AG           | 312.  | 100.0        | .0        | 12.0      | .51 | 1.1            |
| 12. Route 7 NB T    | * 456.0   | 200.0                       | 456.0 | 250.5 | * *    | 50.            | 360. AG           | 443.  | 100.0        | .0        | 24.0      | .14 | 2.6            |
| 13. Route 7 NB R    | * 474.0   | 200.0                       | 474.0 | 454.7 | * *    | 255.           | 360. AG           | 222.  | 100.0        | .0        | 12.0      | .93 | 12.9           |
| 14. Route 7 NB out  | * 454.0   | 470.0                       | 454.0 | 836.0 | * *    | 366.           | 360. AG           | 811.  | 8.3          | .0        | 24.0      |     |                |
| 15. Route 7 SB in   | * 430.0   | 836.0                       | 430.0 | 636.0 | * *    | 200.           | 180. AG           | 749.  | 8.3          | .0        | 24.0      |     |                |
| 16. Route 7 SB L    | * 436.0   | 636.0                       | 436.0 | 507.6 | * *    | 128.           | 180. AG           | 290.  | 100.0        | .0        | 12.0      | .93 | 6.5            |
| 17. Route 7 SB TR   | * 424.0   | 636.0                       | 424.0 | 398.1 | * *    | 238.           | 180. AG           | 200.  | 100.0        | .0        | 12.0      | .90 | 12.1           |
| 18. Route 7 SB out  | * 420.0   | 396.0                       | 420.0 | .0    | * *    | 396.           | 180. AG           | 749.  | 8.3          | .0        | 24.0      |     |                |

DATE : 4/15/11  
 TIME : 13:36:16

-----  
 ADDITIONAL QUEUE LINK PARAMETERS  
 -----

| LINK DESCRIPTION   | *<br>* | CYCLE<br>LENGTH<br>(SEC) | RED<br>TIME<br>(SEC) | CLEARANCE<br>LOST TIME<br>(SEC) | APPROACH<br>VOL<br>(VPH) | SATURATION<br>FLOW RATE<br>(VPH) | IDLE<br>EM FAC<br>(gm/hr) | SIGNAL<br>TYPE | ARRIVAL<br>RATE |
|--------------------|--------|--------------------------|----------------------|---------------------------------|--------------------------|----------------------------------|---------------------------|----------------|-----------------|
| 2. Fort Hill EB LT | *      | 110                      | 97                   | 5.0                             | 93                       | 1799                             | 127.94                    | 3              | 3               |
| 3. Fort Hill EB R  | *      | 110                      | 90                   | 5.0                             | 39                       | 1537                             | 127.94                    | 3              | 3               |
| 6. Bridge WB L     | *      | 110                      | 69                   | 5.0                             | 1310                     | 3570                             | 127.94                    | 3              | 3               |
| 7. Bridge WB T     | *      | 110                      | 69                   | 5.0                             | 93                       | 1845                             | 127.94                    | 3              | 3               |
| 8. Bridge WB R     | *      | 110                      | 69                   | 5.0                             | 127                      | 1900                             | 127.94                    | 3              | 3               |
| 11. Route 7 NB L   | *      | 110                      | 100                  | 3.0                             | 37                       | 1601                             | 127.94                    | 3              | 3               |
| 12. Route 7 NB T   | *      | 110                      | 71                   | 5.0                             | 260                      | 3310                             | 127.94                    | 3              | 3               |
| 13. Route 7 NB R   | *      | 110                      | 71                   | 5.0                             | 514                      | 1900                             | 127.94                    | 3              | 3               |
| 16. Route 7 SB L   | *      | 110                      | 93                   | 3.0                             | 174                      | 1718                             | 127.94                    | 3              | 3               |
| 17. Route 7 SB TR  | *      | 110                      | 64                   | 5.0                             | 575                      | 1809                             | 127.94                    | 3              | 3               |

-----  
 RECEPTOR LOCATIONS  
 -----

| RECEPTOR          | *<br>* | X     | COORDINATES (FT)<br>Y | Z   | *<br>* |
|-------------------|--------|-------|-----------------------|-----|--------|
| 1. EB W Midblock  | *      | 196.0 | 384.0                 | 6.0 | *      |
| 2. SW Corner      | *      | 394.0 | 384.0                 | 6.0 | *      |
| 3. SB S Midblock  | *      | 394.0 | 200.0                 | 6.0 | *      |
| 4. NB S Midblock  | *      | 490.0 | 200.0                 | 6.0 | *      |
| 5. SE Corner      | *      | 490.0 | 384.0                 | 6.0 | *      |
| 6. EB E Midblock  | *      | 648.0 | 384.0                 | 6.0 | *      |
| 7. WB E Midblock  | *      | 648.0 | 482.0                 | 6.0 | *      |
| 8. NE Corner      | *      | 490.0 | 482.0                 | 6.0 | *      |
| 9. NB N Midblock  | *      | 476.0 | 640.0                 | 6.0 | *      |
| 10. SB N Midblock | *      | 400.0 | 640.0                 | 6.0 | *      |
| 11. NW Corner     | *      | 400.0 | 464.0                 | 6.0 | *      |
| 12. WB W Midblock | *      | 196.0 | 464.0                 | 6.0 | *      |

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

| WIND ANGLE (DEGR) | REC1 | REC2 | REC3 | REC4 | REC5 | REC6 | REC7 | REC8 | REC9 | REC10 | REC11 | REC12 |
|-------------------|------|------|------|------|------|------|------|------|------|-------|-------|-------|
| 0.                | 4.9  | 5.1  | 4.7  | 5.3  | 5.6  | 5.0  | 4.3  | 4.4  | 4.4  | 4.4   | 4.8   | 4.3   |
| 10.               | 5.1  | 5.5  | 5.0  | 4.9  | 5.2  | 4.9  | 4.3  | 4.3  | 4.4  | 4.5   | 5.1   | 4.3   |
| 20.               | 5.2  | 5.8  | 5.1  | 4.6  | 5.1  | 4.6  | 4.3  | 4.3  | 4.3  | 4.6   | 5.3   | 4.3   |
| 30.               | 5.3  | 5.7  | 5.1  | 4.5  | 5.1  | 4.6  | 4.3  | 4.3  | 4.3  | 4.6   | 5.3   | 4.3   |
| 40.               | 5.5  | 5.6  | 5.2  | 4.5  | 5.1  | 4.6  | 4.3  | 4.3  | 4.3  | 4.6   | 5.2   | 4.3   |
| 50.               | 5.4  | 5.6  | 5.4  | 4.4  | 5.2  | 4.6  | 4.3  | 4.3  | 4.3  | 4.6   | 5.0   | 4.4   |
| 60.               | 5.3  | 5.7  | 5.5  | 4.3  | 5.4  | 4.6  | 4.3  | 4.3  | 4.3  | 4.6   | 4.9   | 4.5   |
| 70.               | 5.1  | 5.6  | 5.5  | 4.3  | 5.1  | 4.5  | 4.3  | 4.3  | 4.3  | 4.5   | 4.9   | 4.5   |
| 80.               | 5.0  | 5.4  | 5.5  | 4.3  | 4.7  | 4.4  | 4.4  | 4.4  | 4.3  | 4.7   | 5.2   | 4.8   |
| 90.               | 4.7  | 5.0  | 5.2  | 4.3  | 4.5  | 4.3  | 4.5  | 4.6  | 4.3  | 4.8   | 5.6   | 5.0   |
| 100.              | 4.5  | 4.8  | 5.0  | 4.3  | 4.3  | 4.3  | 4.6  | 5.0  | 4.3  | 5.0   | 6.0   | 5.3   |
| 110.              | 4.4  | 4.7  | 4.8  | 4.3  | 4.3  | 4.3  | 4.7  | 5.3  | 4.3  | 5.1   | 6.2   | 5.4   |
| 120.              | 4.5  | 4.7  | 4.6  | 4.3  | 4.3  | 4.3  | 4.7  | 5.1  | 4.4  | 5.5   | 6.2   | 5.4   |
| 130.              | 4.4  | 4.7  | 4.6  | 4.3  | 4.3  | 4.3  | 4.7  | 5.2  | 4.5  | 5.5   | 6.2   | 5.4   |
| 140.              | 4.3  | 4.8  | 4.6  | 4.3  | 4.3  | 4.3  | 4.7  | 5.1  | 4.5  | 5.7   | 6.1   | 5.3   |
| 150.              | 4.3  | 4.8  | 4.6  | 4.3  | 4.3  | 4.3  | 4.6  | 5.1  | 4.5  | 5.8   | 6.2   | 5.3   |
| 160.              | 4.3  | 4.9  | 4.6  | 4.3  | 4.4  | 4.3  | 4.9  | 5.2  | 4.6  | 5.7   | 6.0   | 5.3   |
| 170.              | 4.3  | 4.8  | 4.6  | 4.3  | 4.6  | 4.3  | 5.0  | 5.4  | 4.8  | 5.5   | 5.7   | 5.2   |
| 180.              | 4.3  | 4.5  | 4.4  | 4.4  | 5.0  | 4.3  | 5.4  | 5.7  | 5.1  | 5.2   | 5.4   | 5.0   |
| 190.              | 4.3  | 4.4  | 4.3  | 4.5  | 5.4  | 4.3  | 5.7  | 5.9  | 5.3  | 4.6   | 5.0   | 4.9   |
| 200.              | 4.3  | 4.3  | 4.3  | 4.6  | 5.4  | 4.3  | 5.9  | 5.9  | 5.5  | 4.4   | 4.8   | 4.7   |
| 210.              | 4.3  | 4.3  | 4.3  | 4.6  | 5.3  | 4.3  | 6.1  | 5.7  | 5.5  | 4.5   | 4.7   | 4.7   |
| 220.              | 4.3  | 4.3  | 4.3  | 4.6  | 5.1  | 4.5  | 6.3  | 5.4  | 5.5  | 4.5   | 4.7   | 4.7   |
| 230.              | 4.3  | 4.3  | 4.3  | 4.6  | 5.0  | 4.5  | 6.1  | 5.4  | 5.5  | 4.4   | 4.7   | 4.7   |
| 240.              | 4.3  | 4.3  | 4.3  | 4.6  | 5.0  | 4.5  | 5.9  | 5.1  | 5.3  | 4.4   | 4.9   | 4.8   |
| 250.              | 4.3  | 4.3  | 4.3  | 4.8  | 5.0  | 4.4  | 5.9  | 5.2  | 5.1  | 4.3   | 5.0   | 4.8   |
| 260.              | 4.3  | 4.3  | 4.3  | 5.1  | 5.0  | 4.5  | 5.4  | 5.0  | 5.0  | 4.3   | 5.0   | 4.7   |
| 270.              | 4.3  | 4.5  | 4.3  | 5.5  | 5.3  | 4.8  | 4.9  | 4.9  | 4.9  | 4.3   | 4.7   | 4.6   |
| 280.              | 4.4  | 4.7  | 4.3  | 5.8  | 5.4  | 5.2  | 4.6  | 4.8  | 4.7  | 4.3   | 4.5   | 4.4   |
| 290.              | 4.5  | 4.7  | 4.3  | 6.0  | 5.7  | 5.4  | 4.5  | 4.7  | 4.6  | 4.3   | 4.3   | 4.3   |
| 300.              | 4.5  | 4.7  | 4.3  | 6.2  | 5.8  | 5.4  | 4.6  | 4.9  | 4.6  | 4.3   | 4.3   | 4.3   |
| 310.              | 4.5  | 4.5  | 4.4  | 6.2  | 5.9  | 5.4  | 4.5  | 5.0  | 4.6  | 4.3   | 4.3   | 4.3   |
| 320.              | 4.5  | 4.5  | 4.5  | 6.0  | 6.2  | 5.6  | 4.3  | 5.1  | 4.6  | 4.3   | 4.3   | 4.3   |
| 330.              | 4.5  | 4.5  | 4.5  | 6.0  | 6.3  | 5.3  | 4.3  | 5.1  | 4.7  | 4.3   | 4.3   | 4.3   |
| 340.              | 4.5  | 4.5  | 4.4  | 5.8  | 6.2  | 5.3  | 4.3  | 4.9  | 4.7  | 4.3   | 4.3   | 4.3   |
| 350.              | 4.7  | 4.7  | 4.6  | 5.5  | 5.9  | 5.2  | 4.3  | 4.8  | 4.6  | 4.3   | 4.5   | 4.3   |
| 360.              | 4.9  | 5.1  | 4.7  | 5.3  | 5.6  | 5.0  | 4.3  | 4.4  | 4.4  | 4.4   | 4.8   | 4.3   |
| MAX               | 5.5  | 5.8  | 5.5  | 6.2  | 6.3  | 5.6  | 6.3  | 5.9  | 5.5  | 5.8   | 6.2   | 5.4   |
| DEGR.             | 40   | 20   | 60   | 300  | 330  | 320  | 220  | 190  | 200  | 150   | 110   | 110   |

THE HIGHEST CONCENTRATION OF 6.30 PPM OCCURRED AT RECEPTOR REC7 .



DATE : 4/15/11  
 TIME : 13:36:16

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING  
 THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

| LINK # | * | CO/LINK (PPM) |      |      |      |      |      |      |      |      |       |       |       |
|--------|---|---------------|------|------|------|------|------|------|------|------|-------|-------|-------|
|        |   | REC1          | REC2 | REC3 | REC4 | REC5 | REC6 | REC7 | REC8 | REC9 | REC10 | REC11 | REC12 |
| *      | * | 40            | 20   | 60   | 300  | 330  | 320  | 220  | 190  | 200  | 150   | 110   | 110   |
| 1      | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 2      | * | .5            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .3    |
| 3      | * | .3            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 4      | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 5      | * | .0            | .0   | .1   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 6      | * | .0            | .6   | .0   | .0   | .8   | .8   | .9   | .8   | .2   | .3    | 1.3   | .2    |
| 7      | * | .0            | .0   | .0   | .0   | .0   | .1   | .3   | .0   | .0   | .0    | .0    | .0    |
| 8      | * | .0            | .0   | .0   | .0   | .0   | .1   | .6   | .0   | .0   | .0    | .0    | .0    |
| 9      | * | .2            | .1   | .0   | .1   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .5    |
| 10     | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 11     | * | .0            | .0   | .2   | .1   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 12     | * | .0            | .0   | .5   | 1.0  | .0   | .0   | .1   | .1   | .0   | .0    | .0    | .0    |
| 13     | * | .0            | .0   | .2   | .6   | .7   | .0   | .1   | .6   | .1   | .1    | .2    | .1    |
| 14     | * | .0            | .1   | .0   | .0   | .1   | .1   | .0   | .0   | .2   | .1    | .0    | .0    |
| 15     | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 16     | * | .1            | .2   | .0   | .0   | .1   | .1   | .0   | .0   | .4   | .5    | .0    | .0    |
| 17     | * | .1            | .5   | .0   | .0   | .3   | .1   | .0   | .0   | .3   | .5    | .4    | .0    |
| 18     | * | .0            | .0   | .2   | .1   | .0   | .0   | .0   | .1   | .0   | .0    | .0    | .0    |

JOB: Route7Bridge2030NoBuildPM

RUN: Route7Bridge2030NoBuildPM

DATE : 4/15/11  
 TIME : 13:38:38

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S      VD = .0 CM/S      Z0 = 175. CM  
 U = 1.0 M/S      CLAS = 4 (D)      ATIM = 60. MINUTES      MIXH = 1000. M      AMB = 4.3 PPM

LINK VARIABLES

| LINK DESCRIPTION    | *<br>* X1 | LINK COORDINATES (FT)<br>Y1 | X2     | Y2     | *<br>* LENGTH (FT) | BRG TYPE (DEG) | VPH   | EF (G/MI) | H (FT) | W (FT) | V/C  | QUEUE (VEH) |
|---------------------|-----------|-----------------------------|--------|--------|--------------------|----------------|-------|-----------|--------|--------|------|-------------|
| 1. Fort Hill EB in  | * .0      | 418.0                       | 200.0  | 418.0  | * 200.             | 90. AG         | 447.  | 8.3       | .0     | 24.0   |      |             |
| 2. Fort Hill EB LT  | * 200.0   | 424.0                       | 1220.8 | 424.0  | * 1021.            | 90. AG         | 272.  | 100.0     | .0     | 12.0   | 1.24 | 51.9        |
| 3. Fort Hill EB R   | * 200.0   | 412.0                       | 227.1  | 412.0  | * 27.              | 90. AG         | 209.  | 100.0     | .0     | 12.0   | .13  | 1.4         |
| 4. Bridge EB out    | * 480.0   | 410.0                       | 848.0  | 410.0  | * 368.             | 90. AG         | 447.  | 8.3       | .0     | 24.0   |      |             |
| 5. Bridge WB in     | * 848.0   | 446.0                       | 648.0  | 446.0  | * 200.             | 270. AG        | 1353. | 8.3       | .0     | 48.0   |      |             |
| 6. Bridge WB L      | * 648.0   | 434.0                       | 418.7  | 434.0  | * 229.             | 270. AG        | 515.  | 100.0     | .0     | 24.0   | .64  | 11.7        |
| 7. Bridge WB T      | * 648.0   | 452.0                       | 532.4  | 452.0  | * 116.             | 270. AG        | 257.  | 100.0     | .0     | 12.0   | .65  | 5.9         |
| 8. Bridge WB R      | * 648.0   | 464.0                       | 557.0  | 464.0  | * 91.              | 270. AG        | 257.  | 100.0     | .0     | 12.0   | .51  | 4.6         |
| 9. Fort Hill WB out | * 406.0   | 442.0                       | .0     | 442.0  | * 406.             | 270. AG        | 1353. | 8.3       | .0     | 24.0   |      |             |
| 10. Route 7 NB in   | * 456.0   | .0                          | 456.0  | 200.0  | * 200.             | 360. AG        | 1856. | 8.3       | .0     | 48.0   |      |             |
| 11. Route 7 NB L    | * 438.0   | 200.0                       | 438.0  | 1259.3 | * 1059.            | 360. AG        | 289.  | 100.0     | .0     | 12.0   | 1.41 | 53.8        |
| 12. Route 7 NB T    | * 456.0   | 200.0                       | 456.0  | 340.4  | * 140.             | 360. AG        | 463.  | 100.0     | .0     | 24.0   | .34  | 7.1         |
| 13. Route 7 NB R    | * 474.0   | 200.0                       | 474.0  | 5101.6 | * 4902.            | 360. AG        | 232.  | 100.0     | .0     | 12.0   | 1.86 | 249.0       |
| 14. Route 7 NB out  | * 454.0   | 470.0                       | 454.0  | 836.0  | * 366.             | 360. AG        | 1856. | 8.3       | .0     | 24.0   |      |             |
| 15. Route 7 SB in   | * 430.0   | 836.0                       | 430.0  | 636.0  | * 200.             | 180. AG        | 824.  | 8.3       | .0     | 24.0   |      |             |
| 16. Route 7 SB L    | * 436.0   | 636.0                       | 436.0  | 253.4  | * 383.             | 180. AG        | 269.  | 100.0     | .0     | 12.0   | 1.04 | 19.4        |
| 17. Route 7 SB TR   | * 424.0   | 636.0                       | 424.0  | 419.8  | * 216.             | 180. AG        | 212.  | 100.0     | .0     | 12.0   | .83  | 11.0        |
| 18. Route 7 SB out  | * 420.0   | 396.0                       | 420.0  | .0     | * 396.             | 180. AG        | 824.  | 8.3       | .0     | 24.0   |      |             |

DATE : 4/15/11  
 TIME : 13:38:38

-----  
 ADDITIONAL QUEUE LINK PARAMETERS  
 -----

| LINK DESCRIPTION   | *<br>* | CYCLE<br>LENGTH<br>(SEC) | RED<br>TIME<br>(SEC) | CLEARANCE<br>LOST TIME<br>(SEC) | APPROACH<br>VOL<br>(VPH) | SATURATION<br>FLOW RATE<br>(VPH) | IDLE<br>EM FAC<br>(gm/hr) | SIGNAL<br>TYPE | ARRIVAL<br>RATE |
|--------------------|--------|--------------------------|----------------------|---------------------------------|--------------------------|----------------------------------|---------------------------|----------------|-----------------|
| 2. Fort Hill EB LT | *      | 120                      | 95                   | 5.0                             | 379                      | 2044                             | 127.94                    | 3              | 3               |
| 3. Fort Hill EB R  | *      | 120                      | 73                   | 5.0                             | 68                       | 1599                             | 127.94                    | 3              | 3               |
| 6. Bridge WB L     | *      | 120                      | 90                   | 5.0                             | 933                      | 3813                             | 127.94                    | 3              | 3               |
| 7. Bridge WB T     | *      | 120                      | 90                   | 5.0                             | 235                      | 1881                             | 127.94                    | 3              | 3               |
| 8. Bridge WB R     | *      | 120                      | 90                   | 5.0                             | 185                      | 1900                             | 127.94                    | 3              | 3               |
| 11. Route 7 NB L   | *      | 120                      | 101                  | 3.0                             | 281                      | 1711                             | 127.94                    | 3              | 3               |
| 12. Route 7 NB T   | *      | 120                      | 81                   | 5.0                             | 634                      | 3538                             | 127.94                    | 3              | 3               |
| 13. Route 7 NB R   | *      | 120                      | 81                   | 5.0                             | 941                      | 1900                             | 127.94                    | 3              | 3               |
| 16. Route 7 SB L   | *      | 120                      | 94                   | 3.0                             | 322                      | 1769                             | 127.94                    | 3              | 3               |
| 17. Route 7 SB TR  | *      | 120                      | 74                   | 5.0                             | 502                      | 1860                             | 127.94                    | 3              | 3               |

-----  
 RECEPTOR LOCATIONS  
 -----

| RECEPTOR          | *<br>* | X     | COORDINATES (FT)<br>Y | Z   | *<br>* |
|-------------------|--------|-------|-----------------------|-----|--------|
| 1. EB W Midblock  | *      | 196.0 | 384.0                 | 6.0 | *      |
| 2. SW corner      | *      | 394.0 | 384.0                 | 6.0 | *      |
| 3. SB S Midblock  | *      | 394.0 | 200.0                 | 6.0 | *      |
| 4. NB S Midblock  | *      | 490.0 | 200.0                 | 6.0 | *      |
| 5. SE corner      | *      | 490.0 | 384.0                 | 6.0 | *      |
| 6. EB E Midblock  | *      | 648.0 | 384.0                 | 6.0 | *      |
| 7. WB E Midblock  | *      | 648.0 | 482.0                 | 6.0 | *      |
| 8. NE corner      | *      | 490.0 | 482.0                 | 6.0 | *      |
| 9. NB N Midblock  | *      | 476.0 | 640.0                 | 6.0 | *      |
| 10. SB N Midblock | *      | 400.0 | 640.0                 | 6.0 | *      |
| 11. NW corner     | *      | 400.0 | 464.0                 | 6.0 | *      |
| 12. WB W Midblock | *      | 196.0 | 464.0                 | 6.0 | *      |

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

| WIND ANGLE (DEGR)* | REC1 | REC2 | REC3 | REC4 | REC5 | REC6 | REC7 | REC8 | REC9 | REC10 | REC11 | REC12 |
|--------------------|------|------|------|------|------|------|------|------|------|-------|-------|-------|
| 0.                 | 5.0  | 6.0  | 5.8  | 6.7  | 7.3  | 5.8  | 4.4  | 5.7  | 7.3  | 5.2   | 5.6   | 4.4   |
| 10.                | 5.3  | 7.0  | 6.6  | 5.7  | 6.4  | 5.5  | 4.3  | 5.0  | 6.5  | 5.6   | 6.3   | 4.6   |
| 20.                | 5.4  | 7.2  | 7.1  | 5.1  | 5.9  | 5.1  | 4.3  | 4.4  | 5.5  | 5.7   | 6.7   | 4.6   |
| 30.                | 5.6  | 7.2  | 7.0  | 4.9  | 5.9  | 5.0  | 4.3  | 4.3  | 5.0  | 5.7   | 6.6   | 4.6   |
| 40.                | 5.9  | 7.2  | 6.9  | 4.7  | 6.2  | 5.1  | 4.3  | 4.3  | 4.8  | 5.7   | 6.5   | 4.7   |
| 50.                | 5.8  | 7.2  | 6.6  | 4.6  | 6.4  | 5.1  | 4.3  | 4.3  | 4.7  | 5.6   | 6.4   | 4.9   |
| 60.                | 5.9  | 7.5  | 6.1  | 4.5  | 6.4  | 5.1  | 4.3  | 4.3  | 4.6  | 5.6   | 6.3   | 4.9   |
| 70.                | 5.9  | 7.4  | 5.8  | 4.4  | 6.1  | 5.2  | 4.3  | 4.3  | 4.5  | 5.6   | 6.2   | 4.8   |
| 80.                | 5.8  | 7.1  | 5.7  | 4.4  | 5.6  | 5.0  | 4.5  | 4.6  | 4.5  | 5.7   | 6.8   | 5.3   |
| 90.                | 5.5  | 6.5  | 5.4  | 4.3  | 5.1  | 4.7  | 4.7  | 5.3  | 4.5  | 5.8   | 7.6   | 5.8   |
| 100.               | 5.0  | 5.8  | 5.1  | 4.3  | 4.5  | 4.4  | 5.0  | 5.9  | 4.6  | 6.1   | 8.3   | 6.0   |
| 110.               | 4.8  | 5.6  | 4.9  | 4.3  | 4.3  | 4.3  | 5.1  | 6.4  | 4.6  | 6.2   | 8.2   | 5.9   |
| 120.               | 4.8  | 5.8  | 4.8  | 4.3  | 4.3  | 4.3  | 5.2  | 6.2  | 4.9  | 6.8   | 8.0   | 5.9   |
| 130.               | 4.6  | 6.2  | 4.8  | 4.3  | 4.3  | 4.3  | 5.2  | 6.0  | 5.2  | 7.0   | 7.7   | 5.7   |
| 140.               | 4.4  | 6.3  | 4.8  | 4.3  | 4.3  | 4.3  | 5.1  | 5.9  | 5.4  | 7.2   | 7.4   | 5.6   |
| 150.               | 4.3  | 6.4  | 4.8  | 4.3  | 4.3  | 4.3  | 5.1  | 5.8  | 5.7  | 7.4   | 7.5   | 5.2   |
| 160.               | 4.3  | 5.9  | 4.8  | 4.3  | 4.4  | 4.3  | 5.3  | 5.6  | 6.2  | 7.1   | 7.2   | 5.1   |
| 170.               | 4.3  | 5.5  | 4.6  | 4.4  | 4.8  | 4.3  | 5.5  | 5.9  | 7.1  | 6.7   | 6.8   | 5.1   |
| 180.               | 4.3  | 4.9  | 4.5  | 4.6  | 5.4  | 4.3  | 5.9  | 6.7  | 8.1  | 5.8   | 5.8   | 4.9   |
| 190.               | 4.3  | 4.4  | 4.3  | 4.8  | 6.3  | 4.3  | 6.2  | 7.4  | 8.6  | 5.0   | 5.4   | 4.9   |
| 200.               | 4.3  | 4.3  | 4.3  | 4.9  | 6.7  | 4.4  | 6.5  | 7.6  | 8.4  | 4.5   | 5.0   | 4.7   |
| 210.               | 4.3  | 4.3  | 4.3  | 4.9  | 6.7  | 4.4  | 7.2  | 7.5  | 8.0  | 4.5   | 5.0   | 4.7   |
| 220.               | 4.3  | 4.3  | 4.3  | 4.9  | 6.4  | 4.6  | 7.5  | 7.4  | 7.4  | 4.5   | 5.2   | 4.8   |
| 230.               | 4.3  | 4.3  | 4.3  | 4.9  | 6.2  | 4.8  | 7.8  | 7.2  | 7.1  | 4.4   | 5.2   | 4.8   |
| 240.               | 4.3  | 4.3  | 4.3  | 4.8  | 5.9  | 4.9  | 7.6  | 7.0  | 6.8  | 4.4   | 5.2   | 4.8   |
| 250.               | 4.3  | 4.3  | 4.3  | 5.0  | 5.7  | 4.9  | 7.3  | 6.9  | 6.4  | 4.3   | 5.3   | 4.8   |
| 260.               | 4.3  | 4.3  | 4.3  | 5.3  | 5.8  | 5.0  | 6.8  | 6.6  | 6.2  | 4.3   | 5.0   | 4.7   |
| 270.               | 4.3  | 4.6  | 4.3  | 5.6  | 6.1  | 5.7  | 6.0  | 6.5  | 6.2  | 4.3   | 4.8   | 4.5   |
| 280.               | 4.5  | 4.8  | 4.3  | 5.9  | 6.3  | 6.2  | 5.2  | 6.2  | 6.1  | 4.3   | 4.4   | 4.4   |
| 290.               | 4.6  | 4.9  | 4.3  | 6.2  | 6.7  | 6.6  | 4.9  | 6.1  | 6.0  | 4.3   | 4.3   | 4.3   |
| 300.               | 4.6  | 5.0  | 4.3  | 6.6  | 6.8  | 7.1  | 5.0  | 6.3  | 6.1  | 4.3   | 4.3   | 4.3   |
| 310.               | 4.6  | 5.0  | 4.4  | 7.0  | 7.3  | 7.0  | 4.9  | 6.5  | 6.2  | 4.3   | 4.3   | 4.3   |
| 320.               | 4.6  | 5.0  | 4.5  | 7.3  | 7.6  | 7.1  | 4.8  | 6.6  | 6.5  | 4.3   | 4.3   | 4.3   |
| 330.               | 4.6  | 4.9  | 4.5  | 7.7  | 7.7  | 6.7  | 4.8  | 6.5  | 6.9  | 4.3   | 4.3   | 4.3   |
| 340.               | 4.6  | 4.9  | 4.5  | 7.6  | 7.9  | 6.6  | 4.7  | 6.6  | 7.3  | 4.3   | 4.3   | 4.3   |
| 350.               | 4.8  | 5.4  | 5.0  | 7.4  | 7.8  | 6.3  | 4.6  | 6.5  | 7.7  | 4.6   | 4.7   | 4.3   |
| 360.               | 5.0  | 6.0  | 5.8  | 6.7  | 7.3  | 5.8  | 4.4  | 5.7  | 7.3  | 5.2   | 5.6   | 4.4   |
| MAX                | 5.9  | 7.5  | 7.1  | 7.7  | 7.9  | 7.1  | 7.8  | 7.6  | 8.6  | 7.4   | 8.3   | 6.0   |
| DEGR.              | 40   | 60   | 20   | 330  | 340  | 300  | 230  | 200  | 190  | 150   | 100   | 100   |

THE HIGHEST CONCENTRATION OF 8.60 PPM OCCURRED AT RECEPTOR REC9 .

DATE : 4/15/11  
 TIME : 13:38:38

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING  
 THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

| LINK # | *<br>*<br>*<br>* | CO/LINK (PPM) |            |            |             |             |             |             |             |             |              |              |              |
|--------|------------------|---------------|------------|------------|-------------|-------------|-------------|-------------|-------------|-------------|--------------|--------------|--------------|
|        |                  | REC1<br>40    | REC2<br>60 | REC3<br>20 | REC4<br>330 | REC5<br>340 | REC6<br>300 | REC7<br>230 | REC8<br>200 | REC9<br>190 | REC10<br>150 | REC11<br>100 | REC12<br>100 |
| 1      | *                | .0            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .0           |
| 2      | *                | .5            | .6         | .2         | .2          | .4          | .5          | .4          | .3          | .2          | .2           | .6           | .6           |
| 3      | *                | .3            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .0           |
| 4      | *                | .0            | .0         | .0         | .0          | .1          | .1          | .1          | .0          | .0          | .0           | .1           | .0           |
| 5      | *                | .0            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .1           | .0           |
| 6      | *                | .0            | 1.1        | .3         | .1          | .9          | 1.1         | 1.1         | .9          | .2          | .4           | 1.3          | .3           |
| 7      | *                | .0            | .1         | .0         | .0          | .0          | .2          | .5          | .0          | .0          | .1           | .2           | .0           |
| 8      | *                | .0            | .1         | .0         | .0          | .0          | .1          | .7          | .0          | .0          | .0           | .1           | .0           |
| 9      | *                | .2            | .0         | .0         | .1          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .4           |
| 10     | *                | .0            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .0           |
| 11     | *                | .2            | .4         | .6         | .5          | .5          | .2          | .2          | .4          | .5          | .6           | .5           | .1           |
| 12     | *                | .0            | .0         | .4         | 1.2         | .0          | .0          | .2          | .3          | .1          | .0           | .0           | .0           |
| 13     | *                | .1            | .3         | .4         | .8          | .9          | .2          | .2          | .9          | 2.0         | .3           | .3           | .1           |
| 14     | *                | .1            | .0         | .1         | .0          | .2          | .1          | .0          | .0          | .5          | .3           | .0           | .0           |
| 15     | *                | .0            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .0           |
| 16     | *                | .1            | .4         | .5         | .4          | .4          | .2          | .1          | .4          | .5          | .6           | .4           | .1           |
| 17     | *                | .1            | .1         | .1         | .0          | .2          | .1          | .0          | .0          | .2          | .6           | .4           | .1           |
| 18     | *                | .0            | .1         | .2         | .1          | .0          | .0          | .0          | .1          | .1          | .0           | .0           | .0           |

JOB: Route7Bridge2030BuildAM

RUN: Route7Bridge2030BuildAM

DATE : 4/15/11  
 TIME : 13:40:52

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S      VD = .0 CM/S      Z0 = 175. CM  
 U = 1.0 M/S      CLAS = 4 (D)      ATIM = 60. MINUTES      MIXH = 1000. M      AMB = 4.3 PPM

LINK VARIABLES

| LINK DESCRIPTION    | *<br>* X1 | LINK COORDINATES (FT)<br>Y1 | X2    | Y2    | *<br>* LENGTH (FT) | BRG TYPE (DEG) | VPH   | EF (G/MI) | H (FT) | W (FT) | V/C  | QUEUE (VEH) |
|---------------------|-----------|-----------------------------|-------|-------|--------------------|----------------|-------|-----------|--------|--------|------|-------------|
| 1. Fort Hill EB in  | * .0      | 418.0                       | 200.0 | 418.0 | * 200.             | 90. AG         | 140.  | 8.3       | .0     | 24.0   |      |             |
| 2. Fort Hill EB LT  | * 200.0   | 424.0                       | 333.0 | 424.0 | * 133.             | 90. AG         | 303.  | 100.0     | .0     | 12.0   | 1.03 | 6.8         |
| 3. Fort Hill EB R   | * 200.0   | 412.0                       | 219.2 | 412.0 | * 19.              | 90. AG         | 281.  | 100.0     | .0     | 12.0   | .22  | 1.0         |
| 4. Bridge EB out    | * 480.0   | 410.0                       | 848.0 | 410.0 | * 368.             | 90. AG         | 140.  | 8.3       | .0     | 24.0   |      |             |
| 5. Bridge WB in     | * 848.0   | 446.0                       | 648.0 | 446.0 | * 200.             | 270. AG        | 1534. | 8.3       | .0     | 48.0   |      |             |
| 6. Bridge WB L      | * 648.0   | 434.0                       | 400.5 | 434.0 | * 248.             | 270. AG        | 431.  | 100.0     | .0     | 24.0   | .59  | 12.6        |
| 7. Bridge WB T      | * 648.0   | 452.0                       | 612.5 | 452.0 | * 35.              | 270. AG        | 215.  | 100.0     | .0     | 12.0   | .16  | 1.8         |
| 8. Bridge WB R      | * 648.0   | 464.0                       | 599.7 | 464.0 | * 48.              | 270. AG        | 215.  | 100.0     | .0     | 12.0   | .22  | 2.5         |
| 9. Fort Hill WB out | * 406.0   | 442.0                       | .0    | 442.0 | * 406.             | 270. AG        | 1534. | 8.3       | .0     | 24.0   |      |             |
| 10. Route 7 NB in   | * 456.0   | .0                          | 456.0 | 200.0 | * 200.             | 360. AG        | 867.  | 8.3       | .0     | 48.0   |      |             |
| 11. Route 7 NB L    | * 438.0   | 200.0                       | 438.0 | 220.9 | * 21.              | 360. AG        | 312.  | 100.0     | .0     | 12.0   | .51  | 1.1         |
| 12. Route 7 NB T    | * 456.0   | 200.0                       | 456.0 | 250.5 | * 50.              | 360. AG        | 443.  | 100.0     | .0     | 24.0   | .14  | 2.6         |
| 13. Route 7 NB R    | * 474.0   | 200.0                       | 474.0 | 716.5 | * 516.             | 360. AG        | 222.  | 100.0     | .0     | 12.0   | 1.03 | 26.2        |
| 14. Route 7 NB out  | * 454.0   | 470.0                       | 454.0 | 836.0 | * 366.             | 360. AG        | 867.  | 8.3       | .0     | 24.0   |      |             |
| 15. Route 7 SB in   | * 430.0   | 836.0                       | 430.0 | 636.0 | * 200.             | 180. AG        | 774.  | 8.3       | .0     | 24.0   |      |             |
| 16. Route 7 SB L    | * 436.0   | 636.0                       | 436.0 | 345.7 | * 290.             | 180. AG        | 290.  | 100.0     | .0     | 12.0   | 1.06 | 14.7        |
| 17. Route 7 SB TR   | * 424.0   | 636.0                       | 424.0 | 398.1 | * 238.             | 180. AG        | 200.  | 100.0     | .0     | 12.0   | .90  | 12.1        |
| 18. Route 7 SB out  | * 420.0   | 396.0                       | 420.0 | .0    | * 396.             | 180. AG        | 774.  | 8.3       | .0     | 24.0   |      |             |

DATE : 4/15/11  
 TIME : 13:40:52

-----  
 ADDITIONAL QUEUE LINK PARAMETERS  
 -----

| LINK DESCRIPTION   | *<br>* | CYCLE<br>LENGTH<br>(SEC) | RED<br>TIME<br>(SEC) | CLEARANCE<br>LOST TIME<br>(SEC) | APPROACH<br>VOL<br>(VPH) | SATURATION<br>FLOW RATE<br>(VPH) | IDLE<br>EM FAC<br>(gm/hr) | SIGNAL<br>TYPE | ARRIVAL<br>RATE |
|--------------------|--------|--------------------------|----------------------|---------------------------------|--------------------------|----------------------------------|---------------------------|----------------|-----------------|
| 2. Fort Hill EB LT | *      | 110                      | 97                   | 5.0                             | 101                      | 1801                             | 127.94                    | 3              | 3               |
| 3. Fort Hill EB R  | *      | 110                      | 90                   | 5.0                             | 39                       | 1537                             | 127.94                    | 3              | 3               |
| 6. Bridge WB L     | *      | 110                      | 69                   | 5.0                             | 1312                     | 3570                             | 127.94                    | 3              | 3               |
| 7. Bridge WB T     | *      | 110                      | 69                   | 5.0                             | 94                       | 1845                             | 127.94                    | 3              | 3               |
| 8. Bridge WB R     | *      | 110                      | 69                   | 5.0                             | 128                      | 1900                             | 127.94                    | 3              | 3               |
| 11. Route 7 NB L   | *      | 110                      | 100                  | 3.0                             | 37                       | 1601                             | 127.94                    | 3              | 3               |
| 12. Route 7 NB T   | *      | 110                      | 71                   | 5.0                             | 260                      | 3310                             | 127.94                    | 3              | 3               |
| 13. Route 7 NB R   | *      | 110                      | 71                   | 5.0                             | 570                      | 1900                             | 127.94                    | 3              | 3               |
| 16. Route 7 SB L   | *      | 110                      | 93                   | 3.0                             | 199                      | 1718                             | 127.94                    | 3              | 3               |
| 17. Route 7 SB TR  | *      | 110                      | 64                   | 5.0                             | 575                      | 1809                             | 127.94                    | 3              | 3               |

-----  
 RECEPTOR LOCATIONS  
 -----

| RECEPTOR          | *<br>* | COORDINATES (FT) |       |     | *<br>* |
|-------------------|--------|------------------|-------|-----|--------|
|                   |        | X                | Y     | Z   |        |
| 1. EB W Midblock  | *      | 196.0            | 384.0 | 6.0 | *      |
| 2. SW Corner      | *      | 394.0            | 384.0 | 6.0 | *      |
| 3. SB S Midblock  | *      | 394.0            | 200.0 | 6.0 | *      |
| 4. NB S Midblock  | *      | 490.0            | 200.0 | 6.0 | *      |
| 5. SE Corner      | *      | 490.0            | 384.0 | 6.0 | *      |
| 6. EB E Midblock  | *      | 648.0            | 384.0 | 6.0 | *      |
| 7. WB E Midblock  | *      | 648.0            | 482.0 | 6.0 | *      |
| 8. NE Corner      | *      | 490.0            | 482.0 | 6.0 | *      |
| 9. NB N Midblock  | *      | 476.0            | 640.0 | 6.0 | *      |
| 10. SB N Midblock | *      | 400.0            | 640.0 | 6.0 | *      |
| 11. NW Corner     | *      | 400.0            | 464.0 | 6.0 | *      |
| 12. WB W Midblock | *      | 196.0            | 464.0 | 6.0 | *      |

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

| WIND ANGLE (DEGR) | REC1 | REC2 | REC3 | REC4 | REC5 | REC6 | REC7 | REC8 | REC9 | REC10 | REC11 | REC12 |
|-------------------|------|------|------|------|------|------|------|------|------|-------|-------|-------|
| 0.                | 4.9  | 5.4  | 4.9  | 5.5  | 6.0  | 5.0  | 4.3  | 4.9  | 6.0  | 4.4   | 4.8   | 4.3   |
| 10.               | 5.1  | 5.8  | 5.4  | 5.0  | 5.4  | 4.9  | 4.3  | 4.6  | 5.8  | 4.5   | 5.4   | 4.3   |
| 20.               | 5.2  | 6.3  | 5.4  | 4.6  | 5.2  | 4.6  | 4.3  | 4.4  | 5.3  | 4.6   | 5.6   | 4.3   |
| 30.               | 5.3  | 6.4  | 5.3  | 4.5  | 5.1  | 4.6  | 4.3  | 4.3  | 5.0  | 4.6   | 5.8   | 4.3   |
| 40.               | 5.6  | 6.4  | 5.2  | 4.5  | 5.1  | 4.6  | 4.3  | 4.3  | 4.7  | 4.7   | 5.8   | 4.3   |
| 50.               | 5.5  | 6.2  | 5.4  | 4.4  | 5.2  | 4.6  | 4.3  | 4.3  | 4.6  | 4.8   | 5.7   | 4.5   |
| 60.               | 5.5  | 6.2  | 5.5  | 4.3  | 5.4  | 4.6  | 4.3  | 4.3  | 4.6  | 4.8   | 5.5   | 4.6   |
| 70.               | 5.4  | 6.0  | 5.5  | 4.3  | 5.1  | 4.5  | 4.3  | 4.3  | 4.5  | 4.7   | 5.6   | 4.6   |
| 80.               | 5.2  | 5.8  | 5.5  | 4.3  | 4.7  | 4.4  | 4.4  | 4.4  | 4.5  | 4.9   | 5.9   | 4.9   |
| 90.               | 4.9  | 5.5  | 5.2  | 4.3  | 4.5  | 4.3  | 4.5  | 4.6  | 4.5  | 5.0   | 6.2   | 5.4   |
| 100.              | 4.6  | 5.2  | 5.0  | 4.3  | 4.3  | 4.3  | 4.6  | 5.0  | 4.5  | 5.2   | 6.6   | 5.5   |
| 110.              | 4.4  | 5.1  | 4.8  | 4.3  | 4.3  | 4.3  | 4.7  | 5.3  | 4.5  | 5.3   | 6.7   | 5.6   |
| 120.              | 4.5  | 5.1  | 4.6  | 4.3  | 4.3  | 4.3  | 4.7  | 5.1  | 4.7  | 5.8   | 6.7   | 5.6   |
| 130.              | 4.4  | 5.0  | 4.6  | 4.3  | 4.3  | 4.3  | 4.7  | 5.2  | 4.8  | 5.8   | 6.7   | 5.4   |
| 140.              | 4.3  | 5.0  | 4.7  | 4.3  | 4.3  | 4.3  | 4.7  | 5.1  | 4.9  | 6.1   | 6.6   | 5.3   |
| 150.              | 4.3  | 4.9  | 4.6  | 4.3  | 4.3  | 4.3  | 4.6  | 5.1  | 5.2  | 6.1   | 6.7   | 5.3   |
| 160.              | 4.3  | 4.9  | 4.6  | 4.3  | 4.4  | 4.3  | 4.9  | 5.2  | 5.7  | 6.1   | 6.4   | 5.3   |
| 170.              | 4.3  | 4.8  | 4.6  | 4.4  | 4.6  | 4.3  | 5.0  | 5.4  | 6.5  | 5.8   | 6.0   | 5.2   |
| 180.              | 4.3  | 4.5  | 4.4  | 4.4  | 5.0  | 4.3  | 5.4  | 5.8  | 7.0  | 5.4   | 5.5   | 5.0   |
| 190.              | 4.3  | 4.4  | 4.3  | 4.5  | 5.4  | 4.3  | 5.7  | 6.2  | 7.4  | 4.7   | 5.0   | 4.9   |
| 200.              | 4.3  | 4.3  | 4.3  | 4.7  | 5.4  | 4.3  | 5.9  | 6.3  | 7.3  | 4.5   | 4.8   | 4.7   |
| 210.              | 4.3  | 4.3  | 4.3  | 4.7  | 5.3  | 4.3  | 6.1  | 6.4  | 7.0  | 4.5   | 4.7   | 4.7   |
| 220.              | 4.3  | 4.3  | 4.3  | 4.6  | 5.2  | 4.5  | 6.2  | 6.4  | 6.4  | 4.5   | 4.8   | 4.7   |
| 230.              | 4.3  | 4.3  | 4.3  | 4.6  | 5.2  | 4.5  | 6.2  | 6.3  | 6.3  | 4.5   | 4.9   | 4.7   |
| 240.              | 4.3  | 4.3  | 4.3  | 4.6  | 5.3  | 4.5  | 6.0  | 6.2  | 6.1  | 4.4   | 5.1   | 4.8   |
| 250.              | 4.3  | 4.3  | 4.3  | 4.8  | 5.3  | 4.4  | 6.1  | 6.3  | 5.8  | 4.3   | 5.2   | 4.8   |
| 260.              | 4.3  | 4.3  | 4.3  | 5.1  | 5.5  | 4.6  | 5.7  | 6.1  | 5.6  | 4.3   | 5.1   | 4.7   |
| 270.              | 4.3  | 4.6  | 4.3  | 5.5  | 5.7  | 5.0  | 5.3  | 5.9  | 5.5  | 4.3   | 4.8   | 4.6   |
| 280.              | 4.4  | 4.8  | 4.3  | 5.8  | 5.9  | 5.5  | 4.8  | 5.8  | 5.3  | 4.3   | 4.6   | 4.4   |
| 290.              | 4.5  | 4.9  | 4.3  | 6.0  | 6.1  | 5.6  | 4.7  | 5.7  | 5.2  | 4.3   | 4.4   | 4.3   |
| 300.              | 4.5  | 4.9  | 4.3  | 6.2  | 6.3  | 5.6  | 4.7  | 5.7  | 5.3  | 4.3   | 4.3   | 4.3   |
| 310.              | 4.5  | 4.7  | 4.4  | 6.2  | 6.3  | 5.5  | 4.6  | 5.7  | 5.4  | 4.3   | 4.3   | 4.3   |
| 320.              | 4.5  | 4.6  | 4.5  | 6.1  | 6.5  | 5.7  | 4.5  | 5.8  | 5.5  | 4.3   | 4.3   | 4.3   |
| 330.              | 4.5  | 4.5  | 4.5  | 6.2  | 6.7  | 5.4  | 4.4  | 5.9  | 5.9  | 4.3   | 4.3   | 4.3   |
| 340.              | 4.5  | 4.5  | 4.5  | 6.0  | 6.6  | 5.4  | 4.3  | 5.8  | 6.1  | 4.3   | 4.3   | 4.3   |
| 350.              | 4.7  | 4.8  | 4.8  | 5.8  | 6.4  | 5.2  | 4.3  | 5.5  | 6.2  | 4.3   | 4.5   | 4.3   |
| 360.              | 4.9  | 5.4  | 4.9  | 5.5  | 6.0  | 5.0  | 4.3  | 4.9  | 6.0  | 4.4   | 4.8   | 4.3   |
| MAX               | 5.6  | 6.4  | 5.5  | 6.2  | 6.7  | 5.7  | 6.2  | 6.4  | 7.4  | 6.1   | 6.7   | 5.6   |
| DEGR.             | 40   | 40   | 60   | 300  | 330  | 320  | 220  | 210  | 190  | 140   | 110   | 110   |

THE HIGHEST CONCENTRATION OF 7.40 PPM OCCURRED AT RECEPTOR REC9 .



DATE : 4/15/11  
 TIME : 13:40:52

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING  
 THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

| LINK # | * | CO/LINK (PPM) |      |      |      |      |      |      |      |      |       |       |       |
|--------|---|---------------|------|------|------|------|------|------|------|------|-------|-------|-------|
|        |   | REC1          | REC2 | REC3 | REC4 | REC5 | REC6 | REC7 | REC8 | REC9 | REC10 | REC11 | REC12 |
| *      | * | 40            | 40   | 60   | 300  | 330  | 320  | 220  | 210  | 190  | 140   | 110   | 110   |
| 1      | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 2      | * | .5            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .4    |
| 3      | * | .3            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 4      | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 5      | * | .0            | .0   | .1   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 6      | * | .0            | .8   | .0   | .0   | .8   | .8   | .9   | .8   | .2   | .3    | 1.3   | .2    |
| 7      | * | .0            | .0   | .0   | .0   | .0   | .1   | .3   | .0   | .0   | .0    | .0    | .0    |
| 8      | * | .0            | .0   | .0   | .0   | .0   | .1   | .5   | .0   | .0   | .0    | .0    | .0    |
| 9      | * | .2            | .0   | .0   | .1   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .5    |
| 10     | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 11     | * | .0            | .0   | .2   | .1   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 12     | * | .0            | .0   | .5   | 1.0  | .0   | .0   | .1   | .0   | .0   | .0    | .0    | .0    |
| 13     | * | .1            | .3   | .2   | .6   | .8   | .1   | .1   | .8   | 2.0  | .3    | .2    | .1    |
| 14     | * | .0            | .1   | .0   | .0   | .1   | .1   | .0   | .0   | .2   | .1    | .0    | .0    |
| 15     | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 16     | * | .1            | .5   | .0   | .0   | .4   | .1   | .0   | .3   | .4   | .6    | .5    | .1    |
| 17     | * | .1            | .4   | .0   | .0   | .3   | .1   | .0   | .1   | .2   | .5    | .4    | .0    |
| 18     | * | .0            | .0   | .2   | .1   | .0   | .0   | .0   | .1   | .1   | .0    | .0    | .0    |

JOB: Route7Bridge2030BuildPM

RUN: Route7Bridge2030BuildPM

DATE : 4/15/11  
 TIME : 13:43: 4

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S      VD = .0 CM/S      Z0 = 175. CM  
 U = 1.0 M/S      CLAS = 4 (D)      ATIM = 60. MINUTES      MIXH = 1000. M      AMB = 4.3 PPM

LINK VARIABLES

| LINK DESCRIPTION    | *<br>* X1 | LINK COORDINATES (FT)<br>Y1 | X2     | Y2     | *<br>* LENGTH (FT) | BRG TYPE (DEG) | VPH   | EF (G/MI) | H (FT) | W (FT) | V/C  | QUEUE (VEH) |
|---------------------|-----------|-----------------------------|--------|--------|--------------------|----------------|-------|-----------|--------|--------|------|-------------|
| 1. Fort Hill EB in  | * .0      | 418.0                       | 200.0  | 418.0  | * 200.             | 90. AG         | 447.  | 8.3       | .0     | 24.0   |      |             |
| 2. Fort Hill EB LT  | * 200.0   | 424.0                       | 1220.8 | 424.0  | * 1021.            | 90. AG         | 272.  | 100.0     | .0     | 12.0   | 1.24 | 51.9        |
| 3. Fort Hill EB R   | * 200.0   | 412.0                       | 227.1  | 412.0  | * 27.              | 90. AG         | 209.  | 100.0     | .0     | 12.0   | .13  | 1.4         |
| 4. Bridge EB out    | * 480.0   | 410.0                       | 848.0  | 410.0  | * 368.             | 90. AG         | 447.  | 8.3       | .0     | 24.0   |      |             |
| 5. Bridge WB in     | * 848.0   | 446.0                       | 648.0  | 446.0  | * 200.             | 270. AG        | 1442. | 8.3       | .0     | 48.0   |      |             |
| 6. Bridge WB L      | * 648.0   | 434.0                       | 404.4  | 434.0  | * 244.             | 270. AG        | 515.  | 100.0     | .0     | 24.0   | .68  | 12.4        |
| 7. Bridge WB T      | * 648.0   | 452.0                       | 528.4  | 452.0  | * 120.             | 270. AG        | 257.  | 100.0     | .0     | 12.0   | .68  | 6.1         |
| 8. Bridge WB R      | * 648.0   | 464.0                       | 545.1  | 464.0  | * 103.             | 270. AG        | 257.  | 100.0     | .0     | 12.0   | .57  | 5.2         |
| 9. Fort Hill WB out | * 406.0   | 442.0                       | .0     | 442.0  | * 406.             | 270. AG        | 1442. | 8.3       | .0     | 24.0   |      |             |
| 10. Route 7 NB in   | * 456.0   | .0                          | 456.0  | 200.0  | * 200.             | 360. AG        | 1822. | 8.3       | .0     | 48.0   |      |             |
| 11. Route 7 NB L    | * 438.0   | 200.0                       | 438.0  | 861.9  | * 662.             | 360. AG        | 289.  | 100.0     | .0     | 12.0   | 1.23 | 33.6        |
| 12. Route 7 NB T    | * 456.0   | 200.0                       | 456.0  | 340.4  | * 140.             | 360. AG        | 463.  | 100.0     | .0     | 24.0   | .34  | 7.1         |
| 13. Route 7 NB R    | * 474.0   | 200.0                       | 474.0  | 5133.1 | * 4933.            | 360. AG        | 232.  | 100.0     | .0     | 12.0   | 1.87 | 250.6       |
| 14. Route 7 NB out  | * 454.0   | 470.0                       | 454.0  | 836.0  | * 366.             | 360. AG        | 1822. | 8.3       | .0     | 24.0   |      |             |
| 15. Route 7 SB in   | * 430.0   | 836.0                       | 430.0  | 636.0  | * 200.             | 180. AG        | 825.  | 8.3       | .0     | 24.0   |      |             |
| 16. Route 7 SB L    | * 436.0   | 636.0                       | 436.0  | 242.8  | * 393.             | 180. AG        | 269.  | 100.0     | .0     | 12.0   | 1.05 | 20.0        |
| 17. Route 7 SB TR   | * 424.0   | 636.0                       | 424.0  | 419.8  | * 216.             | 180. AG        | 212.  | 100.0     | .0     | 12.0   | .83  | 11.0        |
| 18. Route 7 SB out  | * 420.0   | 396.0                       | 420.0  | .0     | * 396.             | 180. AG        | 825.  | 8.3       | .0     | 24.0   |      |             |

DATE : 4/15/11  
 TIME : 13:43: 4

-----  
 ADDITIONAL QUEUE LINK PARAMETERS  
 -----

| LINK DESCRIPTION   | *<br>* | CYCLE<br>LENGTH<br>(SEC) | RED<br>TIME<br>(SEC) | CLEARANCE<br>LOST TIME<br>(SEC) | APPROACH<br>VOL<br>(VPH) | SATURATION<br>FLOW RATE<br>(VPH) | IDLE<br>EM FAC<br>(gm/hr) | SIGNAL<br>TYPE | ARRIVAL<br>RATE |
|--------------------|--------|--------------------------|----------------------|---------------------------------|--------------------------|----------------------------------|---------------------------|----------------|-----------------|
| 2. Fort Hill EB LT | *      | 120                      | 95                   | 5.0                             | 379                      | 2044                             | 127.94                    | 3              | 3               |
| 3. Fort Hill EB R  | *      | 120                      | 73                   | 5.0                             | 68                       | 1599                             | 127.94                    | 3              | 3               |
| 6. Bridge WB L     | *      | 120                      | 90                   | 5.0                             | 990                      | 3813                             | 127.94                    | 3              | 3               |
| 7. Bridge WB T     | *      | 120                      | 90                   | 5.0                             | 243                      | 1881                             | 127.94                    | 3              | 3               |
| 8. Bridge WB R     | *      | 120                      | 90                   | 5.0                             | 209                      | 1900                             | 127.94                    | 3              | 3               |
| 11. Route 7 NB L   | *      | 120                      | 101                  | 3.0                             | 244                      | 1711                             | 127.94                    | 3              | 3               |
| 12. Route 7 NB T   | *      | 120                      | 81                   | 5.0                             | 634                      | 3538                             | 127.94                    | 3              | 3               |
| 13. Route 7 NB R   | *      | 120                      | 81                   | 5.0                             | 944                      | 1900                             | 127.94                    | 3              | 3               |
| 16. Route 7 SB L   | *      | 120                      | 94                   | 3.0                             | 323                      | 1769                             | 127.94                    | 3              | 3               |
| 17. Route 7 SB TR  | *      | 120                      | 74                   | 5.0                             | 502                      | 1860                             | 127.94                    | 3              | 3               |

-----  
 RECEPTOR LOCATIONS  
 -----

| RECEPTOR          | *<br>* | X     | COORDINATES (FT)<br>Y | Z   | *<br>* |
|-------------------|--------|-------|-----------------------|-----|--------|
| 1. EB W Midblock  | *      | 196.0 | 384.0                 | 6.0 | *      |
| 2. SW corner      | *      | 394.0 | 384.0                 | 6.0 | *      |
| 3. SB S Midblock  | *      | 394.0 | 200.0                 | 6.0 | *      |
| 4. NB S Midblock  | *      | 490.0 | 200.0                 | 6.0 | *      |
| 5. SE corner      | *      | 490.0 | 384.0                 | 6.0 | *      |
| 6. EB E Midblock  | *      | 648.0 | 384.0                 | 6.0 | *      |
| 7. WB E Midblock  | *      | 648.0 | 482.0                 | 6.0 | *      |
| 8. NE corner      | *      | 490.0 | 482.0                 | 6.0 | *      |
| 9. NB N Midblock  | *      | 476.0 | 640.0                 | 6.0 | *      |
| 10. SB N Midblock | *      | 400.0 | 640.0                 | 6.0 | *      |
| 11. NW corner     | *      | 400.0 | 464.0                 | 6.0 | *      |
| 12. WB W Midblock | *      | 196.0 | 464.0                 | 6.0 | *      |

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

| WIND ANGLE (DEGR) | REC1 | REC2 | REC3 | REC4 | REC5 | REC6 | REC7 | REC8 | REC9 | REC10 | REC11 | REC12 |
|-------------------|------|------|------|------|------|------|------|------|------|-------|-------|-------|
| 0.                | 5.0  | 6.1  | 5.8  | 6.6  | 7.2  | 5.8  | 4.4  | 5.6  | 7.1  | 5.0   | 5.5   | 4.4   |
| 10.               | 5.2  | 7.1  | 6.6  | 5.8  | 6.4  | 5.5  | 4.3  | 5.0  | 6.4  | 5.4   | 6.2   | 4.5   |
| 20.               | 5.4  | 7.5  | 7.1  | 5.1  | 5.9  | 5.1  | 4.3  | 4.4  | 5.5  | 5.6   | 6.6   | 4.5   |
| 30.               | 5.5  | 7.4  | 7.1  | 4.9  | 6.0  | 5.0  | 4.3  | 4.3  | 5.0  | 5.7   | 6.6   | 4.5   |
| 40.               | 5.9  | 7.3  | 7.0  | 4.7  | 6.3  | 5.1  | 4.3  | 4.3  | 4.8  | 5.6   | 6.5   | 4.6   |
| 50.               | 5.8  | 7.3  | 6.7  | 4.6  | 6.4  | 5.2  | 4.3  | 4.3  | 4.7  | 5.6   | 6.4   | 4.9   |
| 60.               | 5.9  | 7.5  | 6.2  | 4.5  | 6.4  | 5.1  | 4.3  | 4.3  | 4.6  | 5.6   | 6.3   | 4.9   |
| 70.               | 5.9  | 7.4  | 5.8  | 4.4  | 6.1  | 5.2  | 4.3  | 4.3  | 4.5  | 5.5   | 6.2   | 4.9   |
| 80.               | 5.9  | 7.1  | 5.7  | 4.4  | 5.6  | 5.0  | 4.5  | 4.7  | 4.5  | 5.7   | 6.8   | 5.3   |
| 90.               | 5.5  | 6.5  | 5.3  | 4.3  | 5.1  | 4.7  | 4.7  | 5.4  | 4.5  | 5.8   | 7.6   | 6.0   |
| 100.              | 5.0  | 5.8  | 5.1  | 4.3  | 4.5  | 4.4  | 5.0  | 6.1  | 4.6  | 6.1   | 8.3   | 6.1   |
| 110.              | 4.8  | 5.6  | 4.9  | 4.3  | 4.3  | 4.3  | 5.1  | 6.5  | 4.6  | 6.1   | 8.2   | 6.0   |
| 120.              | 4.8  | 5.8  | 4.8  | 4.3  | 4.3  | 4.3  | 5.2  | 6.4  | 4.9  | 6.8   | 8.1   | 5.9   |
| 130.              | 4.6  | 6.2  | 4.8  | 4.3  | 4.3  | 4.3  | 5.2  | 6.2  | 5.2  | 7.0   | 7.9   | 5.7   |
| 140.              | 4.4  | 6.3  | 4.8  | 4.3  | 4.3  | 4.3  | 5.1  | 5.9  | 5.4  | 7.2   | 7.8   | 5.6   |
| 150.              | 4.3  | 6.4  | 4.8  | 4.3  | 4.3  | 4.3  | 5.1  | 5.9  | 5.7  | 7.4   | 8.0   | 5.3   |
| 160.              | 4.3  | 5.9  | 4.7  | 4.3  | 4.4  | 4.3  | 5.3  | 5.6  | 6.2  | 7.1   | 7.8   | 5.1   |
| 170.              | 4.3  | 5.5  | 4.6  | 4.4  | 4.8  | 4.3  | 5.5  | 5.9  | 7.2  | 6.8   | 7.3   | 5.1   |
| 180.              | 4.3  | 4.9  | 4.5  | 4.6  | 5.4  | 4.3  | 5.9  | 6.7  | 8.1  | 5.9   | 6.2   | 4.9   |
| 190.              | 4.3  | 4.4  | 4.3  | 4.7  | 6.3  | 4.3  | 6.2  | 7.4  | 8.7  | 5.1   | 5.6   | 4.9   |
| 200.              | 4.3  | 4.3  | 4.3  | 4.9  | 6.7  | 4.4  | 6.5  | 7.6  | 8.5  | 4.5   | 5.1   | 4.7   |
| 210.              | 4.3  | 4.3  | 4.3  | 4.9  | 6.7  | 4.4  | 7.2  | 7.5  | 8.0  | 4.5   | 5.1   | 4.8   |
| 220.              | 4.3  | 4.3  | 4.3  | 4.9  | 6.4  | 4.6  | 7.5  | 7.4  | 7.4  | 4.5   | 5.2   | 4.8   |
| 230.              | 4.3  | 4.3  | 4.3  | 4.8  | 6.2  | 4.9  | 7.8  | 7.3  | 7.1  | 4.4   | 5.2   | 4.8   |
| 240.              | 4.3  | 4.3  | 4.3  | 4.8  | 5.9  | 4.9  | 7.7  | 7.1  | 6.7  | 4.4   | 5.3   | 4.8   |
| 250.              | 4.3  | 4.3  | 4.3  | 4.9  | 5.7  | 4.9  | 7.3  | 7.1  | 6.4  | 4.3   | 5.3   | 4.8   |
| 260.              | 4.3  | 4.3  | 4.3  | 5.3  | 5.8  | 5.0  | 6.8  | 6.6  | 6.2  | 4.3   | 5.1   | 4.7   |
| 270.              | 4.3  | 4.6  | 4.3  | 5.6  | 6.1  | 5.7  | 6.0  | 6.5  | 6.2  | 4.3   | 4.8   | 4.5   |
| 280.              | 4.5  | 4.8  | 4.3  | 5.9  | 6.3  | 6.3  | 5.2  | 6.2  | 6.1  | 4.3   | 4.5   | 4.4   |
| 290.              | 4.6  | 4.9  | 4.3  | 6.3  | 6.8  | 6.7  | 4.9  | 6.1  | 6.0  | 4.3   | 4.3   | 4.3   |
| 300.              | 4.6  | 5.0  | 4.3  | 6.6  | 7.0  | 7.1  | 5.0  | 6.3  | 6.0  | 4.3   | 4.3   | 4.3   |
| 310.              | 4.6  | 5.0  | 4.4  | 7.0  | 7.4  | 7.1  | 4.9  | 6.5  | 6.2  | 4.3   | 4.3   | 4.3   |
| 320.              | 4.6  | 5.0  | 4.5  | 7.3  | 7.7  | 7.1  | 4.8  | 6.6  | 6.4  | 4.3   | 4.3   | 4.3   |
| 330.              | 4.6  | 4.9  | 4.5  | 7.7  | 7.7  | 6.7  | 4.7  | 6.5  | 6.9  | 4.3   | 4.3   | 4.3   |
| 340.              | 4.6  | 4.9  | 4.5  | 7.7  | 7.9  | 6.5  | 4.6  | 6.6  | 7.2  | 4.3   | 4.3   | 4.3   |
| 350.              | 4.8  | 5.4  | 5.0  | 7.5  | 7.7  | 6.2  | 4.5  | 6.4  | 7.5  | 4.5   | 4.6   | 4.3   |
| 360.              | 5.0  | 6.1  | 5.8  | 6.6  | 7.2  | 5.8  | 4.4  | 5.6  | 7.1  | 5.0   | 5.5   | 4.4   |
| MAX               | 5.9  | 7.5  | 7.1  | 7.7  | 7.9  | 7.1  | 7.8  | 7.6  | 8.7  | 7.4   | 8.3   | 6.1   |
| DEGR.             | 40   | 20   | 20   | 330  | 340  | 300  | 230  | 200  | 190  | 150   | 100   | 100   |

THE HIGHEST CONCENTRATION OF 8.70 PPM OCCURRED AT RECEPTOR REC9 .

DATE : 4/15/11  
 TIME : 13:43: 4

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING  
 THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

| LINK # | *<br>*<br>*<br>* | CO/LINK (PPM) |            |            |             |             |             |             |             |             |              |              |              |
|--------|------------------|---------------|------------|------------|-------------|-------------|-------------|-------------|-------------|-------------|--------------|--------------|--------------|
|        |                  | REC1<br>40    | REC2<br>20 | REC3<br>20 | REC4<br>330 | REC5<br>340 | REC6<br>300 | REC7<br>230 | REC8<br>200 | REC9<br>190 | REC10<br>150 | REC11<br>100 | REC12<br>100 |
| 1      | *                | .0            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .0           |
| 2      | *                | .5            | .4         | .2         | .2          | .4          | .5          | .4          | .3          | .2          | .2           | .6           | .6           |
| 3      | *                | .3            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .0           |
| 4      | *                | .0            | .0         | .0         | .0          | .1          | .1          | .1          | .0          | .0          | .0           | .1           | .0           |
| 5      | *                | .0            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .1           | .0           |
| 6      | *                | .0            | .6         | .3         | .1          | .9          | 1.1         | 1.1         | .9          | .3          | .4           | 1.3          | .4           |
| 7      | *                | .0            | .0         | .0         | .0          | .0          | .2          | .5          | .0          | .0          | .1           | .2           | .0           |
| 8      | *                | .0            | .0         | .0         | .0          | .0          | .1          | .7          | .0          | .0          | .0           | .1           | .0           |
| 9      | *                | .2            | .1         | .0         | .1          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .4           |
| 10     | *                | .0            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .0           |
| 11     | *                | .2            | .6         | .6         | .5          | .5          | .2          | .2          | .4          | .5          | .6           | .5           | .1           |
| 12     | *                | .0            | .0         | .4         | 1.2         | .0          | .0          | .2          | .3          | .1          | .0           | .0           | .0           |
| 13     | *                | .1            | .4         | .4         | .8          | .9          | .2          | .2          | .9          | 2.0         | .3           | .3           | .1           |
| 14     | *                | .1            | .2         | .1         | .0          | .2          | .1          | .0          | .0          | .5          | .3           | .0           | .0           |
| 15     | *                | .0            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .0           |
| 16     | *                | .1            | .5         | .5         | .4          | .4          | .2          | .1          | .4          | .5          | .6           | .4           | .1           |
| 17     | *                | .1            | .4         | .1         | .0          | .2          | .1          | .0          | .0          | .2          | .6           | .4           | .1           |
| 18     | *                | .0            | .0         | .2         | .1          | .0          | .0          | .0          | .1          | .1          | .0           | .0           | .0           |

JOB: Route7Bridge2030MitigatedBuildAM

RUN: Route7Bridge2030MitigatedBuildAM

DATE : 4/15/11  
 TIME : 13:45: 4

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S      VD = .0 CM/S      Z0 = 175. CM  
 U = 1.0 M/S      CLAS = 4 (D)      ATIM = 60. MINUTES      MIXH = 1000. M      AMB = 4.3 PPM

LINK VARIABLES

| LINK DESCRIPTION    | *<br>* X1 | LINK COORDINATES (FT)<br>Y1 | X2    | Y2     | *<br>* LENGTH<br>(FT) | BRG TYPE<br>(DEG) | VPH   | EF<br>(G/MI) | H<br>(FT) | W<br>(FT) | V/C  | QUEUE<br>(VEH) |
|---------------------|-----------|-----------------------------|-------|--------|-----------------------|-------------------|-------|--------------|-----------|-----------|------|----------------|
| 1. Fort Hill EB in  | * .0      | 418.0                       | 200.0 | 418.0  | * 200.                | 90. AG            | 140.  | 8.3          | .0        | 24.0      |      |                |
| 2. Fort Hill EB LT  | * 200.0   | 424.0                       | 277.3 | 424.0  | * 77.                 | 90. AG            | 299.  | 100.0        | .0        | 12.0      | .89  | 3.9            |
| 3. Fort Hill EB R   | * 200.0   | 412.0                       | 219.0 | 412.0  | * 19.                 | 90. AG            | 278.  | 100.0        | .0        | 12.0      | .20  | 1.0            |
| 4. Bridge EB out    | * 480.0   | 410.0                       | 848.0 | 410.0  | * 368.                | 90. AG            | 140.  | 8.3          | .0        | 24.0      |      |                |
| 5. Bridge WB in     | * 848.0   | 446.0                       | 648.0 | 446.0  | * 200.                | 270. AG           | 1534. | 8.3          | .0        | 48.0      |      |                |
| 6. Bridge WB L      | * 648.0   | 434.0                       | 400.5 | 434.0  | * 248.                | 270. AG           | 431.  | 100.0        | .0        | 24.0      | .59  | 12.6           |
| 7. Bridge WB T      | * 648.0   | 452.0                       | 612.5 | 452.0  | * 35.                 | 270. AG           | 215.  | 100.0        | .0        | 12.0      | .16  | 1.8            |
| 8. Bridge WB R      | * 648.0   | 464.0                       | 601.1 | 464.0  | * 47.                 | 270. AG           | 209.  | 100.0        | .0        | 12.0      | .21  | 2.4            |
| 9. Fort Hill WB out | * 406.0   | 442.0                       | .0    | 442.0  | * 406.                | 270. AG           | 1534. | 8.3          | .0        | 24.0      |      |                |
| 10. Route 7 NB in   | * 456.0   | .0                          | 456.0 | 200.0  | * 200.                | 360. AG           | 867.  | 8.3          | .0        | 48.0      |      |                |
| 11. Route 7 NB L    | * 438.0   | 200.0                       | 438.0 | 220.9  | * 21.                 | 360. AG           | 312.  | 100.0        | .0        | 12.0      | .51  | 1.1            |
| 12. Route 7 NB T    | * 456.0   | 200.0                       | 456.0 | 252.6  | * 53.                 | 360. AG           | 462.  | 100.0        | .0        | 24.0      | .15  | 2.7            |
| 13. Route 7 NB R    | * 474.0   | 200.0                       | 474.0 | 1243.6 | * 1044.               | 360. AG           | 231.  | 100.0        | .0        | 12.0      | 1.14 | 53.0           |
| 14. Route 7 NB out  | * 454.0   | 470.0                       | 454.0 | 836.0  | * 366.                | 360. AG           | 867.  | 8.3          | .0        | 24.0      |      |                |
| 15. Route 7 SB in   | * 430.0   | 836.0                       | 430.0 | 636.0  | * 200.                | 180. AG           | 774.  | 8.3          | .0        | 24.0      |      |                |
| 16. Route 7 SB L    | * 436.0   | 636.0                       | 436.0 | 500.5  | * 135.                | 180. AG           | 284.  | 100.0        | .0        | 12.0      | .91  | 6.9            |
| 17. Route 7 SB TR   | * 424.0   | 636.0                       | 424.0 | 381.6  | * 254.                | 180. AG           | 203.  | 100.0        | .0        | 12.0      | .92  | 12.9           |
| 18. Route 7 SB out  | * 420.0   | 396.0                       | 420.0 | .0     | * 396.                | 180. AG           | 774.  | 8.3          | .0        | 24.0      |      |                |

DATE : 4/15/11  
 TIME : 13:45: 4

-----  
 ADDITIONAL QUEUE LINK PARAMETERS  
 -----

| LINK DESCRIPTION   | *<br>* | CYCLE<br>LENGTH<br>(SEC) | RED<br>TIME<br>(SEC) | CLEARANCE<br>LOST TIME<br>(SEC) | APPROACH<br>VOL<br>(VPH) | SATURATION<br>FLOW RATE<br>(VPH) | IDLE<br>EM FAC<br>(gm/hr) | SIGNAL<br>TYPE | ARRIVAL<br>RATE |
|--------------------|--------|--------------------------|----------------------|---------------------------------|--------------------------|----------------------------------|---------------------------|----------------|-----------------|
| 2. Fort Hill EB LT | *      | 110                      | 96                   | 5.0                             | 101                      | 1801                             | 127.94                    | 3              | 3               |
| 3. Fort Hill EB R  | *      | 110                      | 89                   | 5.0                             | 39                       | 1537                             | 127.94                    | 3              | 3               |
| 6. Bridge WB L     | *      | 110                      | 69                   | 5.0                             | 1312                     | 3570                             | 127.94                    | 3              | 3               |
| 7. Bridge WB T     | *      | 110                      | 69                   | 5.0                             | 94                       | 1845                             | 127.94                    | 3              | 3               |
| 8. Bridge WB R     | *      | 110                      | 67                   | 5.0                             | 128                      | 1900                             | 127.94                    | 3              | 3               |
| 11. Route 7 NB L   | *      | 110                      | 100                  | 3.0                             | 37                       | 1601                             | 127.94                    | 3              | 3               |
| 12. Route 7 NB T   | *      | 110                      | 74                   | 5.0                             | 260                      | 3310                             | 127.94                    | 3              | 3               |
| 13. Route 7 NB R   | *      | 110                      | 74                   | 5.0                             | 570                      | 1900                             | 127.94                    | 3              | 3               |
| 16. Route 7 SB L   | *      | 110                      | 91                   | 3.0                             | 199                      | 1718                             | 127.94                    | 3              | 3               |
| 17. Route 7 SB TR  | *      | 110                      | 65                   | 5.0                             | 575                      | 1809                             | 127.94                    | 3              | 3               |

-----  
 RECEPTOR LOCATIONS  
 -----

| RECEPTOR          | *<br>* | X     | COORDINATES (FT)<br>Y | Z   | *<br>* |
|-------------------|--------|-------|-----------------------|-----|--------|
| 1. EB W Midblock  | *      | 196.0 | 384.0                 | 6.0 | *      |
| 2. SW Corner      | *      | 394.0 | 384.0                 | 6.0 | *      |
| 3. SB S Midblock  | *      | 394.0 | 200.0                 | 6.0 | *      |
| 4. NB S Midblock  | *      | 490.0 | 200.0                 | 6.0 | *      |
| 5. SE Corner      | *      | 490.0 | 384.0                 | 6.0 | *      |
| 6. EB E Midblock  | *      | 648.0 | 384.0                 | 6.0 | *      |
| 7. WB E Midblock  | *      | 648.0 | 482.0                 | 6.0 | *      |
| 8. NE Corner      | *      | 490.0 | 482.0                 | 6.0 | *      |
| 9. NB N Midblock  | *      | 476.0 | 640.0                 | 6.0 | *      |
| 10. SB N Midblock | *      | 400.0 | 640.0                 | 6.0 | *      |
| 11. NW Corner     | *      | 400.0 | 464.0                 | 6.0 | *      |
| 12. WB W Midblock | *      | 196.0 | 464.0                 | 6.0 | *      |

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

| WIND ANGLE (DEGR) | REC1 | REC2 | REC3 | REC4 | REC5 | REC6 | REC7 | REC8 | REC9 | REC10 | REC11 | REC12 |
|-------------------|------|------|------|------|------|------|------|------|------|-------|-------|-------|
| 0.                | 4.9  | 5.4  | 4.9  | 5.6  | 6.1  | 5.0  | 4.3  | 5.1  | 6.6  | 4.5   | 5.0   | 4.3   |
| 10.               | 5.1  | 5.8  | 5.3  | 5.0  | 5.5  | 4.9  | 4.3  | 4.7  | 6.2  | 4.8   | 5.5   | 4.3   |
| 20.               | 5.3  | 6.1  | 5.2  | 4.6  | 5.2  | 4.6  | 4.3  | 4.4  | 5.5  | 4.9   | 5.7   | 4.4   |
| 30.               | 5.3  | 6.0  | 5.2  | 4.5  | 5.1  | 4.6  | 4.3  | 4.3  | 5.0  | 4.9   | 5.6   | 4.4   |
| 40.               | 5.6  | 5.9  | 5.2  | 4.5  | 5.1  | 4.6  | 4.3  | 4.3  | 4.8  | 4.9   | 5.5   | 4.4   |
| 50.               | 5.4  | 5.9  | 5.5  | 4.4  | 5.2  | 4.6  | 4.3  | 4.3  | 4.7  | 4.9   | 5.4   | 4.5   |
| 60.               | 5.4  | 5.9  | 5.5  | 4.3  | 5.4  | 4.6  | 4.3  | 4.3  | 4.6  | 4.9   | 5.2   | 4.6   |
| 70.               | 5.1  | 5.8  | 5.5  | 4.3  | 5.1  | 4.5  | 4.3  | 4.3  | 4.5  | 4.8   | 5.2   | 4.6   |
| 80.               | 5.0  | 5.6  | 5.5  | 4.3  | 4.7  | 4.4  | 4.4  | 4.4  | 4.5  | 5.0   | 5.5   | 4.9   |
| 90.               | 4.8  | 5.3  | 5.3  | 4.3  | 4.5  | 4.3  | 4.5  | 4.6  | 4.5  | 5.0   | 5.7   | 5.1   |
| 100.              | 4.5  | 4.9  | 5.0  | 4.3  | 4.3  | 4.3  | 4.6  | 5.0  | 4.5  | 5.3   | 6.2   | 5.3   |
| 110.              | 4.5  | 4.8  | 4.8  | 4.3  | 4.3  | 4.3  | 4.7  | 5.3  | 4.5  | 5.4   | 6.3   | 5.4   |
| 120.              | 4.5  | 4.7  | 4.6  | 4.3  | 4.3  | 4.3  | 4.7  | 5.1  | 4.7  | 5.8   | 6.3   | 5.4   |
| 130.              | 4.4  | 4.8  | 4.6  | 4.3  | 4.3  | 4.3  | 4.7  | 5.2  | 4.9  | 5.8   | 6.3   | 5.3   |
| 140.              | 4.3  | 4.8  | 4.7  | 4.3  | 4.3  | 4.3  | 4.7  | 5.1  | 5.0  | 6.0   | 6.2   | 5.4   |
| 150.              | 4.3  | 4.9  | 4.6  | 4.3  | 4.3  | 4.3  | 4.6  | 5.1  | 5.2  | 6.0   | 6.4   | 5.2   |
| 160.              | 4.3  | 4.9  | 4.6  | 4.3  | 4.4  | 4.3  | 4.9  | 5.2  | 5.8  | 6.0   | 6.1   | 5.3   |
| 170.              | 4.3  | 4.8  | 4.6  | 4.4  | 4.6  | 4.3  | 5.0  | 5.4  | 6.5  | 5.6   | 5.8   | 5.2   |
| 180.              | 4.3  | 4.5  | 4.4  | 4.4  | 5.0  | 4.3  | 5.4  | 5.8  | 7.0  | 5.2   | 5.4   | 5.0   |
| 190.              | 4.3  | 4.4  | 4.3  | 4.5  | 5.4  | 4.3  | 5.7  | 6.1  | 7.2  | 4.6   | 5.0   | 4.9   |
| 200.              | 4.3  | 4.3  | 4.3  | 4.7  | 5.4  | 4.3  | 5.8  | 6.2  | 7.2  | 4.4   | 4.8   | 4.7   |
| 210.              | 4.3  | 4.3  | 4.3  | 4.7  | 5.3  | 4.3  | 6.1  | 6.1  | 6.9  | 4.5   | 4.7   | 4.7   |
| 220.              | 4.3  | 4.3  | 4.3  | 4.6  | 5.1  | 4.5  | 6.2  | 6.1  | 6.4  | 4.5   | 4.7   | 4.7   |
| 230.              | 4.3  | 4.3  | 4.3  | 4.6  | 5.1  | 4.5  | 6.1  | 6.0  | 6.3  | 4.4   | 4.7   | 4.7   |
| 240.              | 4.3  | 4.3  | 4.3  | 4.6  | 5.0  | 4.5  | 6.0  | 5.7  | 6.0  | 4.4   | 4.9   | 4.8   |
| 250.              | 4.3  | 4.3  | 4.3  | 4.8  | 5.0  | 4.4  | 5.9  | 5.8  | 5.8  | 4.3   | 4.9   | 4.8   |
| 260.              | 4.3  | 4.3  | 4.3  | 5.1  | 5.1  | 4.5  | 5.4  | 5.6  | 5.6  | 4.3   | 4.9   | 4.7   |
| 270.              | 4.3  | 4.5  | 4.3  | 5.5  | 5.3  | 4.9  | 5.1  | 5.4  | 5.5  | 4.3   | 4.7   | 4.6   |
| 280.              | 4.4  | 4.7  | 4.3  | 5.8  | 5.5  | 5.2  | 4.7  | 5.5  | 5.3  | 4.3   | 4.5   | 4.4   |
| 290.              | 4.5  | 4.7  | 4.3  | 6.0  | 5.7  | 5.4  | 4.7  | 5.5  | 5.3  | 4.3   | 4.4   | 4.3   |
| 300.              | 4.5  | 4.7  | 4.3  | 6.2  | 5.8  | 5.6  | 4.8  | 5.6  | 5.3  | 4.3   | 4.3   | 4.3   |
| 310.              | 4.5  | 4.5  | 4.4  | 6.4  | 6.1  | 5.6  | 4.7  | 5.8  | 5.4  | 4.3   | 4.3   | 4.3   |
| 320.              | 4.5  | 4.5  | 4.5  | 6.0  | 6.2  | 5.8  | 4.6  | 5.8  | 5.6  | 4.3   | 4.3   | 4.3   |
| 330.              | 4.5  | 4.5  | 4.5  | 6.1  | 6.4  | 5.5  | 4.5  | 5.9  | 6.0  | 4.3   | 4.3   | 4.3   |
| 340.              | 4.5  | 4.5  | 4.4  | 6.0  | 6.5  | 5.4  | 4.5  | 5.9  | 6.4  | 4.3   | 4.3   | 4.3   |
| 350.              | 4.7  | 4.7  | 4.7  | 5.7  | 6.4  | 5.3  | 4.4  | 5.7  | 6.7  | 4.3   | 4.6   | 4.3   |
| 360.              | 4.9  | 5.4  | 4.9  | 5.6  | 6.1  | 5.0  | 4.3  | 5.1  | 6.6  | 4.5   | 5.0   | 4.3   |
| MAX               | 5.6  | 6.1  | 5.5  | 6.4  | 6.5  | 5.8  | 6.2  | 6.2  | 7.2  | 6.0   | 6.4   | 5.4   |
| DEGR.             | 40   | 20   | 50   | 310  | 340  | 320  | 220  | 200  | 190  | 140   | 150   | 110   |

THE HIGHEST CONCENTRATION OF 7.20 PPM OCCURRED AT RECEPTOR REC9 .



DATE : 4/15/11  
 TIME : 13:45: 4

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING  
 THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

| LINK # | * | CO/LINK (PPM) |      |      |      |      |      |      |      |      |       |       |       |
|--------|---|---------------|------|------|------|------|------|------|------|------|-------|-------|-------|
|        |   | REC1          | REC2 | REC3 | REC4 | REC5 | REC6 | REC7 | REC8 | REC9 | REC10 | REC11 | REC12 |
| *      | * | 40            | 20   | 50   | 310  | 340  | 320  | 220  | 200  | 190  | 140   | 150   | 110   |
| 1      | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 2      | * | .5            | .0   | .0   | .1   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .2    |
| 3      | * | .3            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 4      | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 5      | * | .0            | .0   | .1   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 6      | * | .0            | .6   | .1   | .0   | .8   | .8   | .9   | .8   | .2   | .3    | 1.0   | .2    |
| 7      | * | .0            | .0   | .0   | .0   | .0   | .1   | .3   | .0   | .0   | .0    | .0    | .0    |
| 8      | * | .0            | .0   | .0   | .0   | .0   | .1   | .5   | .0   | .0   | .0    | .0    | .0    |
| 9      | * | .2            | .1   | .0   | .1   | .0   | .0   | .0   | .0   | .0   | .0    | .1    | .5    |
| 10     | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 11     | * | .0            | .0   | .1   | .1   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 12     | * | .0            | .0   | .4   | 1.0  | .0   | .0   | .1   | .1   | .0   | .0    | .1    | .0    |
| 13     | * | .1            | .3   | .3   | .7   | .9   | .2   | .1   | .8   | 2.0  | .3    | .3    | .1    |
| 14     | * | .0            | .1   | .0   | .0   | .1   | .1   | .0   | .0   | .2   | .1    | .0    | .0    |
| 15     | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 16     | * | .1            | .2   | .0   | .0   | .2   | .1   | .0   | .0   | .2   | .5    | .0    | .0    |
| 17     | * | .1            | .5   | .0   | .0   | .2   | .1   | .0   | .1   | .2   | .5    | .5    | .1    |
| 18     | * | .0            | .0   | .2   | .1   | .0   | .0   | .0   | .1   | .1   | .0    | .1    | .0    |

JOB: Route7Bridge2030MitigatedBuildPM

RUN: Route7Bridge2030MitigatedBuildPM

DATE : 4/15/11  
 TIME : 13:47: 5

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S      VD = .0 CM/S      Z0 = 175. CM  
 U = 1.0 M/S      CLAS = 4 (D)      ATIM = 60. MINUTES      MIXH = 1000. M      AMB = 4.3 PPM

LINK VARIABLES

| LINK DESCRIPTION    | *<br>* X1 | LINK COORDINATES (FT)<br>Y1 | X2     | Y2     | *<br>* LENGTH (FT) | BRG TYPE (DEG) | VPH   | EF (G/MI) | H (FT) | W (FT) | V/C  | QUEUE (VEH) |
|---------------------|-----------|-----------------------------|--------|--------|--------------------|----------------|-------|-----------|--------|--------|------|-------------|
| 1. Fort Hill EB in  | * .0      | 418.0                       | 200.0  | 418.0  | * 200.             | 90. AG         | 447.  | 8.3       | .0     | 24.0   |      |             |
| 2. Fort Hill EB LT  | * 200.0   | 424.0                       | 1220.8 | 424.0  | * 1021.            | 90. AG         | 272.  | 100.0     | .0     | 12.0   | 1.24 | 51.9        |
| 3. Fort Hill EB R   | * 200.0   | 412.0                       | 227.1  | 412.0  | * 27.              | 90. AG         | 209.  | 100.0     | .0     | 12.0   | .13  | 1.4         |
| 4. Bridge EB out    | * 480.0   | 410.0                       | 848.0  | 410.0  | * 368.             | 90. AG         | 447.  | 8.3       | .0     | 24.0   |      |             |
| 5. Bridge WB in     | * 848.0   | 446.0                       | 648.0  | 446.0  | * 200.             | 270. AG        | 1442. | 8.3       | .0     | 48.0   |      |             |
| 6. Bridge WB L      | * 648.0   | 434.0                       | 412.5  | 434.0  | * 235.             | 270. AG        | 498.  | 100.0     | .0     | 24.0   | .60  | 12.0        |
| 7. Bridge WB T      | * 648.0   | 452.0                       | 532.4  | 452.0  | * 116.             | 270. AG        | 249.  | 100.0     | .0     | 12.0   | .60  | 5.9         |
| 8. Bridge WB R      | * 648.0   | 464.0                       | 548.6  | 464.0  | * 99.              | 270. AG        | 249.  | 100.0     | .0     | 12.0   | .51  | 5.1         |
| 9. Fort Hill WB out | * 406.0   | 442.0                       | .0     | 442.0  | * 406.             | 270. AG        | 1442. | 8.3       | .0     | 24.0   |      |             |
| 10. Route 7 NB in   | * 456.0   | .0                          | 456.0  | 200.0  | * 200.             | 360. AG        | 1822. | 8.3       | .0     | 48.0   |      |             |
| 11. Route 7 NB L    | * 438.0   | 200.0                       | 438.0  | 861.9  | * 662.             | 360. AG        | 289.  | 100.0     | .0     | 12.0   | 1.23 | 33.6        |
| 12. Route 7 NB T    | * 456.0   | 200.0                       | 456.0  | 342.1  | * 142.             | 360. AG        | 469.  | 100.0     | .0     | 24.0   | .35  | 7.2         |
| 13. Route 7 NB R    | * 474.0   | 200.0                       | 474.0  | 5299.0 | * 5099.            | 360. AG        | 235.  | 100.0     | .0     | 12.0   | 1.93 | 259.0       |
| 14. Route 7 NB out  | * 454.0   | 470.0                       | 454.0  | 836.0  | * 366.             | 360. AG        | 1822. | 8.3       | .0     | 24.0   |      |             |
| 15. Route 7 SB in   | * 430.0   | 836.0                       | 430.0  | 636.0  | * 200.             | 180. AG        | 825.  | 8.3       | .0     | 24.0   |      |             |
| 16. Route 7 SB L    | * 436.0   | 636.0                       | 436.0  | 242.8  | * 393.             | 180. AG        | 269.  | 100.0     | .0     | 12.0   | 1.05 | 20.0        |
| 17. Route 7 SB TR   | * 424.0   | 636.0                       | 424.0  | 410.8  | * 225.             | 180. AG        | 214.  | 100.0     | .0     | 12.0   | .85  | 11.4        |
| 18. Route 7 SB out  | * 420.0   | 396.0                       | 420.0  | .0     | * 396.             | 180. AG        | 825.  | 8.3       | .0     | 24.0   |      |             |

DATE : 4/15/11  
 TIME : 13:47: 5

-----  
 ADDITIONAL QUEUE LINK PARAMETERS  
 -----

| LINK DESCRIPTION   | *<br>* | CYCLE<br>LENGTH<br>(SEC) | RED<br>TIME<br>(SEC) | CLEARANCE<br>LOST TIME<br>(SEC) | APPROACH<br>VOL<br>(VPH) | SATURATION<br>FLOW RATE<br>(VPH) | IDLE<br>EM FAC<br>(gm/hr) | SIGNAL<br>TYPE | ARRIVAL<br>RATE |
|--------------------|--------|--------------------------|----------------------|---------------------------------|--------------------------|----------------------------------|---------------------------|----------------|-----------------|
| 2. Fort Hill EB LT | *      | 120                      | 95                   | 5.0                             | 379                      | 2044                             | 127.94                    | 3              | 3               |
| 3. Fort Hill EB R  | *      | 120                      | 73                   | 5.0                             | 68                       | 1599                             | 127.94                    | 3              | 3               |
| 6. Bridge WB L     | *      | 120                      | 87                   | 5.0                             | 990                      | 3813                             | 127.94                    | 3              | 3               |
| 7. Bridge WB T     | *      | 120                      | 87                   | 5.0                             | 243                      | 1881                             | 127.94                    | 3              | 3               |
| 8. Bridge WB R     | *      | 120                      | 87                   | 5.0                             | 209                      | 1900                             | 127.94                    | 3              | 3               |
| 11. Route 7 NB L   | *      | 120                      | 101                  | 3.0                             | 244                      | 1711                             | 127.94                    | 3              | 3               |
| 12. Route 7 NB T   | *      | 120                      | 82                   | 5.0                             | 634                      | 3538                             | 127.94                    | 3              | 3               |
| 13. Route 7 NB R   | *      | 120                      | 82                   | 5.0                             | 944                      | 1900                             | 127.94                    | 3              | 3               |
| 16. Route 7 SB L   | *      | 120                      | 94                   | 3.0                             | 323                      | 1769                             | 127.94                    | 3              | 3               |
| 17. Route 7 SB TR  | *      | 120                      | 75                   | 5.0                             | 502                      | 1860                             | 127.94                    | 3              | 3               |

-----  
 RECEPTOR LOCATIONS  
 -----

| RECEPTOR          | *<br>* | COORDINATES (FT) |       |     | *<br>* |
|-------------------|--------|------------------|-------|-----|--------|
|                   |        | X                | Y     | Z   |        |
| 1. EB W Midblock  | *      | 196.0            | 384.0 | 6.0 | *      |
| 2. SW corner      | *      | 394.0            | 384.0 | 6.0 | *      |
| 3. SB S Midblock  | *      | 394.0            | 200.0 | 6.0 | *      |
| 4. NB S Midblock  | *      | 490.0            | 200.0 | 6.0 | *      |
| 5. SE corner      | *      | 490.0            | 384.0 | 6.0 | *      |
| 6. EB E Midblock  | *      | 648.0            | 384.0 | 6.0 | *      |
| 7. WB E Midblock  | *      | 648.0            | 482.0 | 6.0 | *      |
| 8. NE corner      | *      | 490.0            | 482.0 | 6.0 | *      |
| 9. NB N Midblock  | *      | 476.0            | 640.0 | 6.0 | *      |
| 10. SB N Midblock | *      | 400.0            | 640.0 | 6.0 | *      |
| 11. NW corner     | *      | 400.0            | 464.0 | 6.0 | *      |
| 12. WB W Midblock | *      | 196.0            | 464.0 | 6.0 | *      |

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

| WIND ANGLE (DEGR) | REC1 | REC2 | REC3 | REC4 | REC5 | REC6 | REC7 | REC8 | REC9 | REC10 | REC11 | REC12 |
|-------------------|------|------|------|------|------|------|------|------|------|-------|-------|-------|
| 0.                | 5.0  | 6.0  | 5.8  | 6.6  | 7.2  | 5.7  | 4.5  | 5.6  | 7.2  | 5.0   | 5.5   | 4.4   |
| 10.               | 5.2  | 6.9  | 6.6  | 5.7  | 6.4  | 5.4  | 4.3  | 5.0  | 6.5  | 5.4   | 6.2   | 4.5   |
| 20.               | 5.4  | 7.4  | 7.1  | 5.1  | 5.9  | 5.1  | 4.3  | 4.4  | 5.5  | 5.6   | 6.6   | 4.5   |
| 30.               | 5.5  | 7.2  | 7.0  | 4.9  | 5.9  | 5.0  | 4.3  | 4.3  | 5.0  | 5.7   | 6.6   | 4.5   |
| 40.               | 5.9  | 7.3  | 7.0  | 4.7  | 6.3  | 5.1  | 4.3  | 4.3  | 4.8  | 5.6   | 6.5   | 4.6   |
| 50.               | 5.8  | 7.3  | 6.7  | 4.6  | 6.4  | 5.2  | 4.3  | 4.3  | 4.7  | 5.6   | 6.4   | 4.9   |
| 60.               | 5.9  | 7.4  | 6.2  | 4.5  | 6.4  | 5.1  | 4.3  | 4.3  | 4.6  | 5.6   | 6.3   | 4.9   |
| 70.               | 5.9  | 7.3  | 5.8  | 4.4  | 6.1  | 5.2  | 4.3  | 4.3  | 4.5  | 5.5   | 6.2   | 4.8   |
| 80.               | 5.8  | 7.1  | 5.7  | 4.4  | 5.6  | 5.0  | 4.5  | 4.7  | 4.5  | 5.7   | 6.9   | 5.3   |
| 90.               | 5.5  | 6.4  | 5.3  | 4.3  | 5.1  | 4.7  | 4.7  | 5.4  | 4.5  | 5.8   | 7.6   | 5.9   |
| 100.              | 5.0  | 5.8  | 5.1  | 4.3  | 4.5  | 4.4  | 5.0  | 5.8  | 4.6  | 6.1   | 8.1   | 6.0   |
| 110.              | 4.8  | 5.6  | 4.9  | 4.3  | 4.3  | 4.3  | 5.1  | 6.5  | 4.6  | 6.1   | 8.2   | 6.0   |
| 120.              | 4.8  | 5.9  | 4.8  | 4.3  | 4.3  | 4.3  | 5.2  | 6.3  | 4.9  | 6.7   | 8.1   | 5.9   |
| 130.              | 4.6  | 6.2  | 4.8  | 4.3  | 4.3  | 4.3  | 5.2  | 6.1  | 5.2  | 7.0   | 7.9   | 5.7   |
| 140.              | 4.4  | 6.5  | 4.8  | 4.3  | 4.3  | 4.3  | 5.1  | 5.9  | 5.4  | 7.2   | 7.6   | 5.6   |
| 150.              | 4.3  | 6.4  | 4.8  | 4.3  | 4.3  | 4.3  | 5.1  | 5.7  | 5.7  | 7.3   | 7.8   | 5.3   |
| 160.              | 4.3  | 5.9  | 4.7  | 4.3  | 4.4  | 4.3  | 5.3  | 5.6  | 6.1  | 7.1   | 7.6   | 5.1   |
| 170.              | 4.3  | 5.5  | 4.6  | 4.4  | 4.8  | 4.3  | 5.5  | 5.9  | 7.0  | 6.7   | 6.9   | 5.1   |
| 180.              | 4.3  | 4.9  | 4.5  | 4.6  | 5.4  | 4.3  | 5.9  | 6.7  | 8.1  | 5.8   | 5.9   | 4.9   |
| 190.              | 4.3  | 4.4  | 4.3  | 4.7  | 6.3  | 4.3  | 6.2  | 7.4  | 8.8  | 5.1   | 5.4   | 4.9   |
| 200.              | 4.3  | 4.3  | 4.3  | 4.9  | 6.7  | 4.4  | 6.5  | 7.6  | 8.4  | 4.5   | 5.0   | 4.7   |
| 210.              | 4.3  | 4.3  | 4.3  | 4.9  | 6.7  | 4.4  | 7.2  | 7.6  | 8.0  | 4.5   | 5.1   | 4.8   |
| 220.              | 4.3  | 4.3  | 4.3  | 4.9  | 6.5  | 4.6  | 7.5  | 7.4  | 7.4  | 4.5   | 5.2   | 4.8   |
| 230.              | 4.3  | 4.3  | 4.3  | 4.8  | 6.2  | 4.9  | 7.7  | 7.3  | 7.1  | 4.4   | 5.2   | 4.8   |
| 240.              | 4.3  | 4.3  | 4.3  | 4.8  | 5.9  | 4.9  | 7.6  | 7.0  | 6.7  | 4.4   | 5.3   | 4.8   |
| 250.              | 4.3  | 4.3  | 4.3  | 4.9  | 5.7  | 4.9  | 7.4  | 7.0  | 6.4  | 4.3   | 5.3   | 4.8   |
| 260.              | 4.3  | 4.3  | 4.3  | 5.3  | 5.8  | 5.1  | 6.8  | 6.6  | 6.2  | 4.3   | 5.1   | 4.7   |
| 270.              | 4.3  | 4.6  | 4.3  | 5.6  | 6.1  | 5.8  | 6.1  | 6.5  | 6.2  | 4.3   | 4.8   | 4.5   |
| 280.              | 4.5  | 4.8  | 4.3  | 6.0  | 6.4  | 6.3  | 5.2  | 6.2  | 6.1  | 4.3   | 4.5   | 4.4   |
| 290.              | 4.6  | 4.9  | 4.3  | 6.3  | 6.7  | 6.6  | 4.9  | 6.1  | 6.0  | 4.3   | 4.3   | 4.3   |
| 300.              | 4.6  | 5.0  | 4.3  | 6.6  | 7.0  | 7.0  | 5.0  | 6.3  | 6.0  | 4.3   | 4.3   | 4.3   |
| 310.              | 4.6  | 5.0  | 4.4  | 7.0  | 7.3  | 7.0  | 4.9  | 6.5  | 6.2  | 4.3   | 4.3   | 4.3   |
| 320.              | 4.6  | 5.0  | 4.5  | 7.3  | 7.6  | 7.0  | 4.8  | 6.6  | 6.4  | 4.3   | 4.3   | 4.3   |
| 330.              | 4.6  | 4.9  | 4.5  | 7.7  | 7.7  | 6.6  | 4.7  | 6.5  | 6.9  | 4.3   | 4.3   | 4.3   |
| 340.              | 4.6  | 4.9  | 4.5  | 7.6  | 7.9  | 6.5  | 4.6  | 6.6  | 7.2  | 4.3   | 4.3   | 4.3   |
| 350.              | 4.8  | 5.3  | 4.9  | 7.4  | 7.7  | 6.1  | 4.5  | 6.4  | 7.5  | 4.5   | 4.6   | 4.3   |
| 360.              | 5.0  | 6.0  | 5.8  | 6.6  | 7.2  | 5.7  | 4.5  | 5.6  | 7.2  | 5.0   | 5.5   | 4.4   |
| MAX               | 5.9  | 7.4  | 7.1  | 7.7  | 7.9  | 7.0  | 7.7  | 7.6  | 8.8  | 7.3   | 8.2   | 6.0   |
| DEGR.             | 40   | 20   | 20   | 330  | 340  | 300  | 230  | 200  | 190  | 150   | 110   | 100   |

THE HIGHEST CONCENTRATION OF 8.80 PPM OCCURRED AT RECEPTOR REC9 .

DATE : 4/15/11  
 TIME : 13:47: 5

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING  
 THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

| LINK # | * | CO/LINK (PPM) |      |      |      |      |      |      |      |      |       |       |       |
|--------|---|---------------|------|------|------|------|------|------|------|------|-------|-------|-------|
|        |   | REC1          | REC2 | REC3 | REC4 | REC5 | REC6 | REC7 | REC8 | REC9 | REC10 | REC11 | REC12 |
| *      | * | 40            | 20   | 20   | 330  | 340  | 300  | 230  | 200  | 190  | 150   | 110   | 100   |
| 1      | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 2      | * | .5            | .4   | .2   | .2   | .4   | .5   | .4   | .3   | .2   | .2    | .6    | .6    |
| 3      | * | .3            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 4      | * | .0            | .0   | .0   | .0   | .1   | .1   | .1   | .0   | .0   | .0    | .1    | .0    |
| 5      | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 6      | * | .0            | .4   | .3   | .1   | .9   | 1.0  | 1.0  | .9   | .3   | .3    | 1.5   | .3    |
| 7      | * | .0            | .0   | .0   | .0   | .0   | .2   | .5   | .0   | .0   | .1    | .1    | .0    |
| 8      | * | .0            | .0   | .0   | .0   | .0   | .1   | .7   | .0   | .0   | .0    | .0    | .0    |
| 9      | * | .2            | .1   | .0   | .1   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .4    |
| 10     | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 11     | * | .2            | .6   | .6   | .5   | .5   | .2   | .2   | .4   | .5   | .6    | .5    | .1    |
| 12     | * | .0            | .0   | .4   | 1.2  | .0   | .0   | .2   | .3   | .1   | .0    | .0    | .0    |
| 13     | * | .1            | .4   | .4   | .8   | .9   | .2   | .2   | .9   | 2.1  | .3    | .3    | .1    |
| 14     | * | .1            | .2   | .1   | .0   | .2   | .1   | .0   | .0   | .5   | .3    | .0    | .0    |
| 15     | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 16     | * | .1            | .5   | .5   | .4   | .4   | .2   | .1   | .4   | .5   | .6    | .4    | .1    |
| 17     | * | .1            | .5   | .1   | .0   | .2   | .1   | .0   | .0   | .2   | .6    | .4    | .1    |
| 18     | * | .0            | .0   | .2   | .1   | .0   | .0   | .0   | .1   | .1   | .0    | .0    | .0    |

JOB: GristMillMain2010ExistingAM

RUN: GristMillMain2010ExistingAM

DATE : 4/ 7/11  
 TIME : 15:16:42

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S      VD = .0 CM/S      Z0 = 175. CM  
 U = 1.0 M/S      CLAS = 4 (D)      ATIM = 60. MINUTES      MIXH = 1000. M      AMB = 4.3 PPM

LINK VARIABLES

| LINK DESCRIPTION     | *<br>* | X1    | LINK COORDINATES (FT)<br>Y1 | X2    | Y2    | *<br>* | LENGTH<br>(FT) | BRG TYPE<br>(DEG) | VPH   | EF<br>(G/MI) | H<br>(FT) | W<br>(FT) | V/C  | QUEUE<br>(VEH) |
|----------------------|--------|-------|-----------------------------|-------|-------|--------|----------------|-------------------|-------|--------------|-----------|-----------|------|----------------|
| 1. Grist Mill EB in  | *      | .0    | 412.0                       | 200.0 | 412.0 | *      | 200.           | 90. AG            | 1803. | 11.2         | .0        | 36.0      |      |                |
| 2. Grist Mill EB L   | *      | 200.0 | 424.0                       | 862.4 | 424.0 | *      | 662.           | 90. AG            | 254.  | 100.0        | .0        | 12.0      | 1.01 | 33.6           |
| 3. Grist Mill EB LT  | *      | 200.0 | 412.0                       | 234.8 | 412.0 | *      | 35.            | 90. AG            | 254.  | 100.0        | .0        | 12.0      | .74  | 1.8            |
| 4. Grist Mill EB R   | *      | 200.0 | 400.0                       | 298.2 | 400.0 | *      | 98.            | 90. AG            | 203.  | 100.0        | .0        | 12.0      | .52  | 5.0            |
| 5. Grist Mill EB out | *      | 466.0 | 418.0                       | 848.0 | 418.0 | *      | 382.           | 90. AG            | 1803. | 11.2         | .0        | 24.0      |      |                |
| 6. Grist Mill WB in  | *      | 848.0 | 442.0                       | 648.0 | 442.0 | *      | 200.           | 270. AG           | 123.  | 11.2         | .0        | 24.0      |      |                |
| 7. Grist Mill WB LT  | *      | 648.0 | 436.0                       | 506.6 | 436.0 | *      | 141.           | 270. AG           | 423.  | 100.0        | .0        | 12.0      | 1.35 | 7.2            |
| 8. Grist Mill WB TR  | *      | 648.0 | 448.0                       | 361.0 | 448.0 | *      | 287.           | 270. AG           | 423.  | 100.0        | .0        | 12.0      | 1.28 | 14.6           |
| 9. Grist Mill WB out | *      | 406.0 | 442.0                       | .0    | 442.0 | *      | 406.           | 270. AG           | 123.  | 11.2         | .0        | 24.0      |      |                |
| 10. Main NB in       | *      | 444.0 | .0                          | 444.0 | 200.0 | *      | 200.           | 360. AG           | 519.  | 11.2         | .0        | 24.0      |      |                |
| 11. Main NB L        | *      | 438.0 | 200.0                       | 438.0 | 278.5 | *      | 78.            | 360. AG           | 267.  | 100.0        | .0        | 12.0      | .89  | 4.0            |
| 12. Main NB TR       | *      | 450.0 | 200.0                       | 450.0 | 319.4 | *      | 119.           | 360. AG           | 258.  | 100.0        | .0        | 12.0      | .56  | 6.1            |
| 13. Main NB out      | *      | 454.0 | 454.0                       | 454.0 | 836.0 | *      | 382.           | 360. AG           | 519.  | 11.2         | .0        | 24.0      |      |                |
| 14. Main SB in       | *      | 424.0 | 836.0                       | 424.0 | 636.0 | *      | 200.           | 180. AG           | 1716. | 11.2         | .0        | 36.0      |      |                |
| 15. Main SB L        | *      | 436.0 | 636.0                       | 436.0 | 625.5 | *      | 10.            | 180. AG           | 301.  | 100.0        | .0        | 12.0      | .06  | .5             |
| 16. Main SB T        | *      | 424.0 | 636.0                       | 424.0 | 320.1 | *      | 316.           | 180. AG           | 301.  | 100.0        | .0        | 12.0      | 1.00 | 16.0           |
| 17. Main SB R        | *      | 412.0 | 636.0                       | 412.0 | 470.2 | *      | 166.           | 180. AG           | 93.   | 100.0        | .0        | 12.0      | .91  | 8.4            |
| 18. Main SB out      | *      | 420.0 | 396.0                       | 420.0 | .0    | *      | 396.           | 180. AG           | 1716. | 11.2         | .0        | 24.0      |      |                |

DATE : 4/ 7/11  
 TIME : 15:16:42

-----  
 ADDITIONAL QUEUE LINK PARAMETERS  
 -----

| LINK DESCRIPTION    | *<br>* | CYCLE<br>LENGTH<br>(SEC) | RED<br>TIME<br>(SEC) | CLEARANCE<br>LOST TIME<br>(SEC) | APPROACH<br>VOL<br>(VPH) | SATURATION<br>FLOW RATE<br>(VPH) | IDLE<br>EM FAC<br>(gm/hr) | SIGNAL<br>TYPE | ARRIVAL<br>RATE |
|---------------------|--------|--------------------------|----------------------|---------------------------------|--------------------------|----------------------------------|---------------------------|----------------|-----------------|
| 2. Grist Mill EB L  | *      | 110                      | 60                   | 6.0                             | 1329                     | 3459                             | 173.64                    | 3              | 4               |
| 3. Grist Mill EB LT | *      | 110                      | 60                   | 6.0                             | 100                      | 354                              | 173.64                    | 3              | 4               |
| 4. Grist Mill EB R  | *      | 110                      | 48                   | 6.0                             | 374                      | 1463                             | 173.64                    | 3              | 4               |
| 7. Grist Mill WB LT | *      | 110                      | 100                  | 5.0                             | 35                       | 960                              | 173.64                    | 3              | 3               |
| 8. Grist Mill WB TR | *      | 110                      | 100                  | 5.0                             | 88                       | 2558                             | 173.64                    | 3              | 3               |
| 11. Main NB L       | *      | 110                      | 63                   | 4.0                             | 161                      | 485                              | 173.64                    | 3              | 4               |
| 12. Main NB TR      | *      | 110                      | 61                   | 6.0                             | 358                      | 1718                             | 173.64                    | 3              | 4               |
| 15. Main SB L       | *      | 110                      | 71                   | 6.0                             | 27                       | 1563                             | 173.64                    | 3              | 4               |
| 16. Main SB T       | *      | 110                      | 71                   | 6.0                             | 580                      | 2068                             | 173.64                    | 3              | 4               |
| 17. Main SB R       | *      | 110                      | 22                   | 6.0                             | 1109                     | 1668                             | 173.64                    | 3              | 4               |

-----  
 RECEPTOR LOCATIONS  
 -----

| RECEPTOR          | *<br>* | COORDINATES (FT) |       |     | *<br>* |
|-------------------|--------|------------------|-------|-----|--------|
|                   |        | X                | Y     | Z   |        |
| 1. EB W Midblock  | *      | 196.0            | 384.0 | 6.0 | *      |
| 2. SW corner      | *      | 394.0            | 384.0 | 6.0 | *      |
| 3. SB S Midblock  | *      | 394.0            | 200.0 | 6.0 | *      |
| 4. NB S Midblock  | *      | 466.0            | 200.0 | 6.0 | *      |
| 5. SE corner      | *      | 466.0            | 390.0 | 6.0 | *      |
| 6. EB E Midblock  | *      | 648.0            | 390.0 | 6.0 | *      |
| 7. WB E Midblock  | *      | 648.0            | 464.0 | 6.0 | *      |
| 8. NE corner      | *      | 476.0            | 464.0 | 6.0 | *      |
| 9. NB N Midblock  | *      | 476.0            | 640.0 | 6.0 | *      |
| 10. SB N Midblock | *      | 396.0            | 640.0 | 6.0 | *      |
| 11. NW corner     | *      | 396.0            | 464.0 | 6.0 | *      |
| 12. WB W Midblock | *      | 196.0            | 464.0 | 6.0 | *      |

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

| WIND ANGLE (DEGR) | REC1 | REC2 | REC3 | REC4 | REC5 | REC6 | REC7 | REC8 | REC9 | REC10 | REC11 | REC12 |
|-------------------|------|------|------|------|------|------|------|------|------|-------|-------|-------|
| 0.                | 5.1  | 5.7  | 5.3  | 5.7  | 5.9  | 5.8  | 4.3  | 4.7  | 4.5  | 4.7   | 5.0   | 4.3   |
| 10.               | 5.3  | 6.1  | 5.7  | 5.1  | 5.8  | 5.5  | 4.3  | 4.4  | 4.4  | 4.9   | 5.4   | 4.3   |
| 20.               | 5.5  | 6.2  | 5.9  | 5.0  | 5.7  | 5.4  | 4.3  | 4.3  | 4.3  | 5.1   | 5.5   | 4.3   |
| 30.               | 5.7  | 6.0  | 6.1  | 4.9  | 6.1  | 5.3  | 4.3  | 4.3  | 4.3  | 5.1   | 5.4   | 4.4   |
| 40.               | 5.9  | 6.1  | 6.2  | 4.7  | 6.2  | 5.3  | 4.3  | 4.3  | 4.3  | 5.1   | 5.4   | 4.4   |
| 50.               | 5.9  | 6.3  | 5.9  | 4.5  | 6.5  | 5.4  | 4.3  | 4.3  | 4.3  | 5.0   | 5.2   | 4.5   |
| 60.               | 6.0  | 6.6  | 5.7  | 4.5  | 6.8  | 5.4  | 4.3  | 4.3  | 4.3  | 5.0   | 5.2   | 4.4   |
| 70.               | 6.3  | 6.8  | 5.6  | 4.3  | 6.6  | 5.4  | 4.3  | 4.4  | 4.3  | 4.9   | 5.3   | 4.5   |
| 80.               | 6.0  | 6.8  | 5.3  | 4.3  | 6.0  | 5.2  | 4.3  | 5.0  | 4.3  | 5.0   | 5.9   | 5.0   |
| 90.               | 5.5  | 6.3  | 5.3  | 4.3  | 5.3  | 4.8  | 4.6  | 6.1  | 4.3  | 5.2   | 6.8   | 5.4   |
| 100.              | 4.9  | 5.5  | 5.1  | 4.3  | 4.6  | 4.5  | 4.8  | 7.1  | 4.3  | 5.2   | 7.6   | 5.5   |
| 110.              | 4.6  | 5.3  | 4.9  | 4.3  | 4.3  | 4.3  | 5.2  | 7.6  | 4.3  | 5.4   | 7.6   | 5.7   |
| 120.              | 4.6  | 5.4  | 4.9  | 4.3  | 4.3  | 4.3  | 5.3  | 7.4  | 4.5  | 5.7   | 7.3   | 5.3   |
| 130.              | 4.5  | 5.5  | 4.9  | 4.3  | 4.3  | 4.3  | 5.2  | 7.0  | 4.7  | 5.8   | 6.9   | 5.3   |
| 140.              | 4.4  | 5.6  | 5.0  | 4.3  | 4.3  | 4.3  | 5.1  | 6.6  | 4.8  | 6.1   | 6.8   | 5.2   |
| 150.              | 4.4  | 5.8  | 5.0  | 4.3  | 4.3  | 4.3  | 5.2  | 6.3  | 4.9  | 6.0   | 6.8   | 5.2   |
| 160.              | 4.3  | 5.7  | 5.0  | 4.3  | 4.4  | 4.3  | 5.4  | 6.2  | 4.9  | 6.1   | 6.9   | 5.2   |
| 170.              | 4.3  | 5.2  | 4.9  | 4.4  | 4.7  | 4.3  | 5.6  | 6.3  | 5.2  | 5.8   | 6.9   | 5.1   |
| 180.              | 4.3  | 4.9  | 4.6  | 4.5  | 4.9  | 4.3  | 6.0  | 6.5  | 5.4  | 5.4   | 6.6   | 4.8   |
| 190.              | 4.3  | 4.5  | 4.4  | 4.7  | 5.3  | 4.3  | 6.5  | 6.7  | 5.5  | 4.9   | 6.1   | 4.8   |
| 200.              | 4.3  | 4.4  | 4.3  | 4.9  | 5.1  | 4.3  | 6.9  | 6.7  | 5.5  | 4.5   | 5.9   | 4.7   |
| 210.              | 4.3  | 4.3  | 4.3  | 4.9  | 5.2  | 4.4  | 7.1  | 6.6  | 5.3  | 4.5   | 5.8   | 4.7   |
| 220.              | 4.3  | 4.3  | 4.3  | 4.9  | 5.1  | 4.5  | 7.5  | 6.5  | 5.3  | 4.5   | 5.8   | 4.7   |
| 230.              | 4.3  | 4.3  | 4.3  | 4.9  | 5.1  | 4.6  | 7.7  | 6.6  | 5.2  | 4.4   | 6.0   | 4.8   |
| 240.              | 4.3  | 4.3  | 4.3  | 4.9  | 5.2  | 4.6  | 7.9  | 6.7  | 5.2  | 4.4   | 6.0   | 4.8   |
| 250.              | 4.3  | 4.3  | 4.3  | 5.0  | 5.0  | 4.6  | 7.9  | 6.8  | 5.2  | 4.3   | 5.6   | 4.8   |
| 260.              | 4.5  | 4.5  | 4.3  | 5.1  | 5.3  | 4.7  | 7.4  | 6.5  | 5.1  | 4.3   | 5.4   | 4.5   |
| 270.              | 4.7  | 4.7  | 4.3  | 5.4  | 5.5  | 5.6  | 6.4  | 5.9  | 5.0  | 4.3   | 4.7   | 4.4   |
| 280.              | 4.9  | 5.1  | 4.3  | 5.7  | 5.6  | 6.2  | 5.2  | 5.4  | 5.0  | 4.3   | 4.3   | 4.3   |
| 290.              | 5.0  | 4.9  | 4.3  | 5.8  | 5.5  | 6.8  | 4.7  | 5.1  | 4.9  | 4.3   | 4.3   | 4.3   |
| 300.              | 5.0  | 4.8  | 4.4  | 6.0  | 5.7  | 6.9  | 4.4  | 5.0  | 4.9  | 4.3   | 4.3   | 4.3   |
| 310.              | 5.0  | 4.8  | 4.4  | 6.2  | 5.8  | 6.8  | 4.5  | 5.0  | 4.9  | 4.3   | 4.3   | 4.3   |
| 320.              | 4.9  | 4.8  | 4.6  | 6.2  | 5.9  | 6.8  | 4.4  | 5.1  | 4.9  | 4.3   | 4.3   | 4.3   |
| 330.              | 4.9  | 4.9  | 4.5  | 6.4  | 6.0  | 6.5  | 4.4  | 5.1  | 4.9  | 4.3   | 4.3   | 4.3   |
| 340.              | 4.8  | 5.0  | 4.4  | 6.4  | 6.1  | 6.2  | 4.3  | 5.0  | 4.9  | 4.3   | 4.3   | 4.3   |
| 350.              | 5.1  | 5.4  | 4.7  | 6.1  | 6.1  | 6.0  | 4.3  | 4.9  | 4.7  | 4.4   | 4.6   | 4.3   |
| 360.              | 5.1  | 5.7  | 5.3  | 5.7  | 5.9  | 5.8  | 4.3  | 4.7  | 4.5  | 4.7   | 5.0   | 4.3   |
| MAX               | 6.3  | 6.8  | 6.2  | 6.4  | 6.8  | 6.9  | 7.9  | 7.6  | 5.5  | 6.1   | 7.6   | 5.7   |
| DEGR.             | 70   | 70   | 40   | 340  | 60   | 300  | 240  | 110  | 190  | 140   | 110   | 110   |

THE HIGHEST CONCENTRATION OF 7.90 PPM OCCURRED AT RECEPTOR REC7 .



DATE : 4/ 7/11  
 TIME : 15:16:42

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING  
 THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

| LINK # | * | CO/LINK (PPM) |      |      |      |      |      |      |      |      |       |       |       |
|--------|---|---------------|------|------|------|------|------|------|------|------|-------|-------|-------|
|        |   | REC1          | REC2 | REC3 | REC4 | REC5 | REC6 | REC7 | REC8 | REC9 | REC10 | REC11 | REC12 |
| *      | * | 70            | 70   | 40   | 340  | 60   | 300  | 240  | 110  | 190  | 140   | 110   | 110   |
| 1      | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 2      | * | .6            | .5   | .2   | .1   | .6   | .6   | .5   | .5   | .1   | .2    | .5    | .6    |
| 3      | * | .1            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 4      | * | .6            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .1    |
| 5      | * | .1            | .4   | .1   | .0   | .7   | .6   | .4   | .5   | .0   | .1    | .4    | .1    |
| 6      | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 7      | * | .1            | .3   | .1   | .0   | .6   | .6   | 1.0  | .8   | .0   | .2    | .3    | .1    |
| 8      | * | .3            | .5   | .2   | .1   | .6   | .6   | 1.5  | 1.5  | .2   | .2    | 1.5   | .2    |
| 9      | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .1    |
| 10     | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 11     | * | .0            | .0   | .4   | .4   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 12     | * | .0            | .0   | .3   | .8   | .0   | .0   | .0   | .0   | .1   | .0    | .0    | .0    |
| 13     | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .2   | .1    | .0    | .0    |
| 14     | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 15     | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 16     | * | .2            | .5   | .0   | .3   | .0   | .2   | .1   | .0   | .4   | .7    | .6    | .1    |
| 17     | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .3    | .0    | .0    |
| 18     | * | .0            | .3   | .6   | .4   | .0   | .0   | .1   | .0   | .2   | .0    | .0    | .1    |

JOB: GristMillMain2010ExistingPM

RUN: GristMillMain2010ExistingPM

DATE : 4/ 7/11  
 TIME : 16:17:25

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S      VD = .0 CM/S      Z0 = 175. CM  
 U = 1.0 M/S      CLAS = 4 (D)      ATIM = 60. MINUTES      MIXH = 1000. M      AMB = 4.3 PPM

LINK VARIABLES

| LINK DESCRIPTION     | *<br>*<br>* | X1    | LINK COORDINATES (FT) |        | *<br>*<br>* | LENGTH<br>(FT) | BRG TYPE<br>(DEG) | VPH   | EF<br>(G/MI) | H<br>(FT) | W<br>(FT) | V/C  | QUEUE<br>(VEH) |
|----------------------|-------------|-------|-----------------------|--------|-------------|----------------|-------------------|-------|--------------|-----------|-----------|------|----------------|
|                      |             |       | Y1                    | X2     | Y2          |                |                   |       |              |           |           |      |                |
| 1. Grist Mill EB in  | *           | .0    | 412.0                 | 200.0  | 412.0       | 200.           | 90. AG            | 1642. | 11.2         | .0        | 36.0      |      |                |
| 2. Grist Mill EB L   | *           | 200.0 | 424.0                 | 3420.7 | 424.0       | 3221.          | 90. AG            | 265.  | 100.0        | .0        | 12.0      | 1.22 | 163.6          |
| 3. Grist Mill EB LT  | *           | 200.0 | 412.0                 | 200.3  | 412.0       | 0.             | 90. AG            | 265.  | 100.0        | .0        | 12.0      | .01  | .0             |
| 4. Grist Mill EB R   | *           | 200.0 | 400.0                 | 235.4  | 400.0       | 35.            | 90. AG            | 182.  | 100.0        | .0        | 12.0      | .21  | 1.8            |
| 5. Grist Mill EB out | *           | 466.0 | 418.0                 | 848.0  | 418.0       | 382.           | 90. AG            | 1642. | 11.2         | .0        | 24.0      |      |                |
| 6. Grist Mill WB in  | *           | 848.0 | 442.0                 | 648.0  | 442.0       | 200.           | 270. AG           | 32.   | 11.2         | .0        | 24.0      |      |                |
| 7. Grist Mill WB LT  | *           | 648.0 | 436.0                 | 507.3  | 436.0       | 141.           | 270. AG           | 428.  | 100.0        | .0        | 12.0      | 1.83 | 7.1            |
| 8. Grist Mill WB TR  | *           | 648.0 | 448.0                 | 641.9  | 448.0       | 6.             | 270. AG           | 428.  | 100.0        | .0        | 12.0      | .53  | .3             |
| 9. Grist Mill WB out | *           | 406.0 | 442.0                 | .0     | 442.0       | 406.           | 270. AG           | 32.   | 11.2         | .0        | 24.0      |      |                |
| 10. Main NB in       | *           | 444.0 | .0                    | 444.0  | 200.0       | 200.           | 360. AG           | 1041. | 11.2         | .0        | 24.0      |      |                |
| 11. Main NB L        | *           | 438.0 | 200.0                 | 438.0  | 1058.4      | 858.           | 360. AG           | 247.  | 100.0        | .0        | 12.0      | 1.27 | 43.6           |
| 12. Main NB TR       | *           | 450.0 | 200.0                 | 450.0  | 466.7       | 267.           | 360. AG           | 238.  | 100.0        | .0        | 12.0      | .96  | 13.5           |
| 13. Main NB out      | *           | 454.0 | 454.0                 | 454.0  | 836.0       | 382.           | 360. AG           | 1041. | 11.2         | .0        | 24.0      |      |                |
| 14. Main SB in       | *           | 424.0 | 836.0                 | 424.0  | 636.0       | 200.           | 180. AG           | 1798. | 11.2         | .0        | 36.0      |      |                |
| 15. Main SB L        | *           | 436.0 | 636.0                 | 436.0  | 633.7       | 2.             | 180. AG           | 321.  | 100.0        | .0        | 12.0      | .02  | .1             |
| 16. Main SB T        | *           | 424.0 | 636.0                 | 424.0  | 65.0        | 571.           | 180. AG           | 321.  | 100.0        | .0        | 12.0      | 1.08 | 29.0           |
| 17. Main SB R        | *           | 412.0 | 636.0                 | 412.0  | -1441.3     | 2077.          | 180. AG           | 121.  | 100.0        | .0        | 12.0      | 1.15 | 105.5          |
| 18. Main SB out      | *           | 420.0 | 396.0                 | 420.0  | .0          | 396.           | 180. AG           | 1798. | 11.2         | .0        | 24.0      |      |                |

DATE : 4/ 7/11  
 TIME : 16:17:25

-----  
 ADDITIONAL QUEUE LINK PARAMETERS  
 -----

| LINK DESCRIPTION    | *<br>* | CYCLE<br>LENGTH<br>(SEC) | RED<br>TIME<br>(SEC) | CLEARANCE<br>LOST TIME<br>(SEC) | APPROACH<br>VOL<br>(VPH) | SATURATION<br>FLOW RATE<br>(VPH) | IDLE<br>EM FAC<br>(gm/hr) | SIGNAL<br>TYPE | ARRIVAL<br>RATE |
|---------------------|--------|--------------------------|----------------------|---------------------------------|--------------------------|----------------------------------|---------------------------|----------------|-----------------|
| 2. Grist Mill EB L  | *      | 100                      | 57                   | 6.0                             | 1476                     | 3465                             | 173.64                    | 3              | 4               |
| 3. Grist Mill EB LT | *      | 100                      | 57                   | 6.0                             | 1                        | 354                              | 173.64                    | 3              | 4               |
| 4. Grist Mill EB R  | *      | 100                      | 39                   | 6.0                             | 166                      | 1492                             | 173.64                    | 3              | 4               |
| 7. Grist Mill WB LT | *      | 100                      | 92                   | 5.0                             | 22                       | 1232                             | 173.64                    | 3              | 3               |
| 8. Grist Mill WB TR | *      | 100                      | 92                   | 5.0                             | 10                       | 1939                             | 173.64                    | 3              | 3               |
| 11. Main NB L       | *      | 100                      | 53                   | 4.0                             | 326                      | 629                              | 173.64                    | 3              | 4               |
| 12. Main NB TR      | *      | 100                      | 51                   | 6.0                             | 715                      | 1814                             | 173.64                    | 3              | 4               |
| 15. Main SB L       | *      | 100                      | 69                   | 6.0                             | 6                        | 1592                             | 173.64                    | 3              | 4               |
| 16. Main SB T       | *      | 100                      | 69                   | 6.0                             | 446                      | 1801                             | 173.64                    | 3              | 4               |
| 17. Main SB R       | *      | 100                      | 26                   | 6.0                             | 1346                     | 1775                             | 173.64                    | 3              | 4               |

-----  
 RECEPTOR LOCATIONS  
 -----

| RECEPTOR          | *<br>* | COORDINATES (FT) |       |     | *<br>* |
|-------------------|--------|------------------|-------|-----|--------|
|                   |        | X                | Y     | Z   |        |
| 1. EB W Midblock  | *      | 196.0            | 384.0 | 6.0 | *      |
| 2. SW corner      | *      | 394.0            | 384.0 | 6.0 | *      |
| 3. SB S Midblock  | *      | 394.0            | 200.0 | 6.0 | *      |
| 4. NB S Midblock  | *      | 466.0            | 200.0 | 6.0 | *      |
| 5. SE corner      | *      | 466.0            | 390.0 | 6.0 | *      |
| 6. EB E Midblock  | *      | 648.0            | 390.0 | 6.0 | *      |
| 7. WB E Midblock  | *      | 648.0            | 464.0 | 6.0 | *      |
| 8. NE corner      | *      | 476.0            | 464.0 | 6.0 | *      |
| 9. NB N Midblock  | *      | 476.0            | 640.0 | 6.0 | *      |
| 10. SB N Midblock | *      | 396.0            | 640.0 | 6.0 | *      |
| 11. NW corner     | *      | 396.0            | 464.0 | 6.0 | *      |
| 12. WB W Midblock | *      | 196.0            | 464.0 | 6.0 | *      |

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

| WIND ANGLE (DEGR)* | REC1 | REC2 | REC3 | REC4 | REC5 | REC6 | REC7 | REC8 | REC9 | REC10 | REC11 | REC12 |
|--------------------|------|------|------|------|------|------|------|------|------|-------|-------|-------|
| 0.                 | 5.0  | 5.9  | 6.1  | 6.4  | 6.4  | 5.7  | 4.3  | 5.1  | 4.9  | 5.0   | 5.4   | 4.3   |
| 10.                | 4.9  | 6.5  | 6.9  | 5.3  | 5.7  | 5.5  | 4.3  | 4.5  | 4.5  | 5.4   | 6.1   | 4.3   |
| 20.                | 5.2  | 6.7  | 7.3  | 4.9  | 5.5  | 5.4  | 4.3  | 4.3  | 4.3  | 5.7   | 6.2   | 4.4   |
| 30.                | 5.4  | 6.7  | 7.5  | 4.8  | 5.5  | 5.3  | 4.3  | 4.3  | 4.3  | 5.7   | 6.2   | 4.5   |
| 40.                | 5.6  | 6.7  | 7.2  | 4.7  | 5.6  | 5.3  | 4.3  | 4.3  | 4.3  | 5.6   | 6.0   | 4.6   |
| 50.                | 5.7  | 6.9  | 7.0  | 4.6  | 5.9  | 5.3  | 4.3  | 4.3  | 4.3  | 5.5   | 5.9   | 4.7   |
| 60.                | 5.7  | 7.0  | 6.7  | 4.6  | 6.1  | 5.5  | 4.3  | 4.3  | 4.3  | 5.5   | 5.8   | 4.7   |
| 70.                | 5.9  | 7.4  | 6.6  | 4.5  | 6.2  | 5.6  | 4.3  | 4.3  | 4.3  | 5.4   | 5.8   | 4.8   |
| 80.                | 5.9  | 7.7  | 6.5  | 4.5  | 6.0  | 5.4  | 4.5  | 4.7  | 4.3  | 5.5   | 6.3   | 5.2   |
| 90.                | 5.7  | 7.4  | 6.3  | 4.4  | 5.5  | 5.2  | 4.9  | 5.4  | 4.4  | 5.7   | 6.9   | 5.5   |
| 100.               | 5.2  | 6.7  | 6.1  | 4.3  | 4.8  | 4.7  | 5.2  | 6.0  | 4.5  | 5.8   | 7.3   | 5.7   |
| 110.               | 4.9  | 6.4  | 5.9  | 4.3  | 4.4  | 4.4  | 5.2  | 6.1  | 4.5  | 5.9   | 7.2   | 5.7   |
| 120.               | 4.9  | 6.5  | 5.9  | 4.3  | 4.3  | 4.3  | 5.2  | 5.9  | 4.6  | 6.3   | 6.7   | 5.4   |
| 130.               | 4.8  | 6.6  | 6.0  | 4.3  | 4.3  | 4.3  | 5.2  | 5.7  | 4.7  | 6.4   | 6.6   | 5.4   |
| 140.               | 4.7  | 6.7  | 6.2  | 4.3  | 4.3  | 4.3  | 5.2  | 5.5  | 4.7  | 6.5   | 6.9   | 5.4   |
| 150.               | 4.6  | 6.9  | 6.3  | 4.3  | 4.3  | 4.3  | 5.2  | 5.2  | 4.8  | 6.7   | 7.0   | 5.1   |
| 160.               | 4.4  | 7.0  | 6.1  | 4.3  | 4.4  | 4.3  | 5.3  | 5.0  | 4.7  | 6.9   | 7.1   | 5.0   |
| 170.               | 4.4  | 6.6  | 5.8  | 4.5  | 4.9  | 4.3  | 5.5  | 5.5  | 5.2  | 6.5   | 7.1   | 4.8   |
| 180.               | 4.3  | 5.9  | 5.3  | 4.9  | 5.9  | 4.3  | 5.8  | 6.1  | 5.9  | 6.0   | 6.3   | 4.8   |
| 190.               | 4.3  | 4.9  | 4.7  | 5.3  | 6.6  | 4.4  | 6.1  | 6.8  | 6.4  | 5.1   | 5.4   | 4.7   |
| 200.               | 4.3  | 4.5  | 4.4  | 5.7  | 7.0  | 4.4  | 6.4  | 7.0  | 6.4  | 4.6   | 5.0   | 4.6   |
| 210.               | 4.3  | 4.3  | 4.3  | 5.8  | 7.0  | 4.7  | 6.6  | 6.9  | 6.2  | 4.4   | 4.7   | 4.7   |
| 220.               | 4.3  | 4.3  | 4.3  | 5.8  | 6.9  | 4.8  | 6.9  | 6.9  | 6.0  | 4.5   | 4.8   | 4.7   |
| 230.               | 4.3  | 4.3  | 4.3  | 5.8  | 6.6  | 4.9  | 6.9  | 6.6  | 6.0  | 4.4   | 4.8   | 4.7   |
| 240.               | 4.3  | 4.3  | 4.3  | 5.7  | 6.5  | 4.9  | 6.8  | 6.3  | 5.6  | 4.4   | 4.9   | 4.7   |
| 250.               | 4.3  | 4.3  | 4.3  | 5.9  | 6.5  | 4.9  | 6.7  | 6.4  | 5.6  | 4.3   | 4.8   | 4.6   |
| 260.               | 4.4  | 4.4  | 4.3  | 5.9  | 6.6  | 5.1  | 6.2  | 6.4  | 5.6  | 4.3   | 4.7   | 4.5   |
| 270.               | 4.6  | 4.5  | 4.3  | 6.1  | 6.8  | 5.7  | 5.6  | 6.1  | 5.5  | 4.3   | 4.6   | 4.4   |
| 280.               | 4.9  | 4.7  | 4.3  | 6.2  | 6.9  | 6.1  | 5.0  | 5.8  | 5.4  | 4.3   | 4.3   | 4.3   |
| 290.               | 5.0  | 4.8  | 4.3  | 6.4  | 6.8  | 6.4  | 4.8  | 5.6  | 5.4  | 4.3   | 4.3   | 4.3   |
| 300.               | 5.0  | 4.8  | 4.4  | 6.6  | 6.7  | 6.6  | 4.6  | 5.6  | 5.4  | 4.3   | 4.3   | 4.3   |
| 310.               | 4.9  | 4.8  | 4.4  | 6.8  | 6.7  | 6.4  | 4.8  | 5.8  | 5.5  | 4.3   | 4.3   | 4.3   |
| 320.               | 4.9  | 4.8  | 4.5  | 7.0  | 6.9  | 6.5  | 4.7  | 5.9  | 5.7  | 4.3   | 4.3   | 4.3   |
| 330.               | 4.8  | 4.7  | 4.4  | 7.0  | 7.0  | 6.3  | 4.6  | 5.9  | 5.6  | 4.3   | 4.3   | 4.3   |
| 340.               | 4.8  | 4.7  | 4.4  | 7.2  | 7.3  | 5.9  | 4.4  | 5.9  | 5.6  | 4.3   | 4.3   | 4.3   |
| 350.               | 4.8  | 5.1  | 5.0  | 7.1  | 6.9  | 5.8  | 4.3  | 5.6  | 5.4  | 4.6   | 4.7   | 4.3   |
| 360.               | 5.0  | 5.9  | 6.1  | 6.4  | 6.4  | 5.7  | 4.3  | 5.1  | 4.9  | 5.0   | 5.4   | 4.3   |
| MAX DEGR.          | 5.9  | 7.7  | 7.5  | 7.2  | 7.3  | 6.6  | 6.9  | 7.0  | 6.4  | 6.9   | 7.3   | 5.7   |
|                    | 70   | 80   | 30   | 340  | 340  | 300  | 220  | 200  | 190  | 160   | 100   | 100   |

THE HIGHEST CONCENTRATION OF 7.70 PPM OCCURRED AT RECEPTOR REC2 .

DATE : 4/ 7/11  
 TIME : 16:17:25

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING  
 THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

| LINK # | * | CO/LINK (PPM) |      |      |      |      |      |      |      |      |       |       |       |
|--------|---|---------------|------|------|------|------|------|------|------|------|-------|-------|-------|
|        |   | REC1          | REC2 | REC3 | REC4 | REC5 | REC6 | REC7 | REC8 | REC9 | REC10 | REC11 | REC12 |
| *      | * | 70            | 80   | 30   | 340  | 340  | 300  | 220  | 200  | 190  | 160   | 100   | 100   |
| 1      | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 2      | * | .6            | .7   | .2   | .1   | .4   | .6   | .5   | .4   | .1   | .1    | .7    | .7    |
| 3      | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 4      | * | .3            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 5      | * | .1            | .4   | .1   | .0   | .1   | .6   | .4   | .1   | .0   | .1    | .3    | .1    |
| 6      | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 7      | * | .1            | .3   | .1   | .0   | .0   | .6   | .9   | .0   | .0   | .1    | .4    | .1    |
| 8      | * | .0            | .0   | .0   | .0   | .0   | .0   | .2   | .0   | .0   | .0    | .0    | .0    |
| 9      | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 10     | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 11     | * | .1            | .4   | .5   | .7   | .7   | .1   | .1   | .5   | .5   | .5    | .4    | .1    |
| 12     | * | .1            | .3   | .4   | .9   | .7   | .0   | .1   | .6   | .2   | .1    | .2    | .1    |
| 13     | * | .0            | .0   | .0   | .0   | .2   | .1   | .0   | .0   | .4   | .2    | .1    | .0    |
| 14     | * | .0            | .0   | .0   | .0   | .1   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 15     | * | .0            | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0   | .0    | .0    | .0    |
| 16     | * | .2            | .6   | .8   | .6   | .6   | .2   | .2   | .5   | .5   | .9    | .6    | .2    |
| 17     | * | .1            | .3   | .4   | .2   | .2   | .1   | .1   | .2   | .2   | .5    | .3    | .1    |
| 18     | * | .0            | .4   | .7   | .4   | .0   | .0   | .1   | .4   | .2   | .1    | .0    | .0    |

JOB: GristMillMain2030NoBuildAM

RUN: GristMillMain2030NoBuildAM

DATE : 4/15/11  
 TIME : 13:50: 8

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S      VD = .0 CM/S      Z0 = 175. CM  
 U = 1.0 M/S      CLAS = 4 (D)      ATIM = 60. MINUTES      MIXH = 1000. M      AMB = 4.3 PPM

LINK VARIABLES

| LINK DESCRIPTION     | *<br>*<br>* | X1    | LINK COORDINATES (FT)<br>Y1 | X2     | Y2     | *<br>*<br>* | LENGTH<br>(FT) | BRG TYPE<br>(DEG) | VPH   | EF<br>(G/MI) | H<br>(FT) | W<br>(FT) | V/C  | QUEUE<br>(VEH) |
|----------------------|-------------|-------|-----------------------------|--------|--------|-------------|----------------|-------------------|-------|--------------|-----------|-----------|------|----------------|
| 1. Grist Mill EB in  | *           | .0    | 412.0                       | 200.0  | 412.0  | *           | 200.           | 90. AG            | 2164. | 8.3          | .0        | 36.0      |      |                |
| 2. Grist Mill EB L   | *           | 200.0 | 424.0                       | 3595.4 | 424.0  | *           | 3395.          | 90. AG            | 187.  | 100.0        | .0        | 12.0      | 1.21 | 172.5          |
| 3. Grist Mill EB LT  | *           | 200.0 | 412.0                       | 260.0  | 412.0  | *           | 60.            | 90. AG            | 187.  | 100.0        | .0        | 12.0      | .89  | 3.1            |
| 4. Grist Mill EB R   | *           | 200.0 | 400.0                       | 317.8  | 400.0  | *           | 118.           | 90. AG            | 150.  | 100.0        | .0        | 12.0      | .63  | 6.0            |
| 5. Grist Mill EB out | *           | 466.0 | 418.0                       | 848.0  | 418.0  | *           | 382.           | 90. AG            | 2164. | 8.3          | .0        | 24.0      |      |                |
| 6. Grist Mill WB in  | *           | 848.0 | 442.0                       | 648.0  | 442.0  | *           | 200.           | 270. AG           | 148.  | 8.3          | .0        | 24.0      |      |                |
| 7. Grist Mill WB LT  | *           | 648.0 | 436.0                       | -310.6 | 436.0  | *           | 959.           | 270. AG           | 312.  | 100.0        | .0        | 12.0      | 4.12 | 48.7           |
| 8. Grist Mill WB TR  | *           | 648.0 | 448.0                       | 623.6  | 448.0  | *           | 24.            | 270. AG           | 312.  | 100.0        | .0        | 12.0      | .59  | 1.2            |
| 9. Grist Mill WB out | *           | 406.0 | 442.0                       | .0     | 442.0  | *           | 406.           | 270. AG           | 148.  | 8.3          | .0        | 24.0      |      |                |
| 10. Main NB in       | *           | 444.0 | .0                          | 444.0  | 200.0  | *           | 200.           | 360. AG           | 623.  | 8.3          | .0        | 24.0      |      |                |
| 11. Main NB L        | *           | 438.0 | 200.0                       | 438.0  | 755.8  | *           | 556.           | 360. AG           | 197.  | 100.0        | .0        | 12.0      | 1.29 | 28.2           |
| 12. Main NB TR       | *           | 450.0 | 200.0                       | 450.0  | 343.4  | *           | 143.           | 360. AG           | 190.  | 100.0        | .0        | 12.0      | .67  | 7.3            |
| 13. Main NB out      | *           | 454.0 | 454.0                       | 454.0  | 836.0  | *           | 382.           | 360. AG           | 623.  | 8.3          | .0        | 24.0      |      |                |
| 14. Main SB in       | *           | 424.0 | 836.0                       | 424.0  | 636.0  | *           | 200.           | 180. AG           | 2059. | 8.3          | .0        | 36.0      |      |                |
| 15. Main SB L        | *           | 436.0 | 636.0                       | 436.0  | 623.6  | *           | 12.            | 180. AG           | 222.  | 100.0        | .0        | 12.0      | .07  | .6             |
| 16. Main SB T        | *           | 424.0 | 636.0                       | 424.0  | -869.0 | *           | 1505.          | 180. AG           | 222.  | 100.0        | .0        | 12.0      | 1.20 | 76.5           |
| 17. Main SB R        | *           | 412.0 | 636.0                       | 412.0  | -845.9 | *           | 1482.          | 180. AG           | 69.   | 100.0        | .0        | 12.0      | 1.10 | 75.3           |
| 18. Main SB out      | *           | 420.0 | 396.0                       | 420.0  | .0     | *           | 396.           | 180. AG           | 2059. | 8.3          | .0        | 24.0      |      |                |

DATE : 4/15/11  
 TIME : 13:50: 8

-----  
 ADDITIONAL QUEUE LINK PARAMETERS  
 -----

| LINK DESCRIPTION    | *<br>* | CYCLE<br>LENGTH<br>(SEC) | RED<br>TIME<br>(SEC) | CLEARANCE<br>LOST TIME<br>(SEC) | APPROACH<br>VOL<br>(VPH) | SATURATION<br>FLOW RATE<br>(VPH) | IDLE<br>EM FAC<br>(gm/hr) | SIGNAL<br>TYPE | ARRIVAL<br>RATE |
|---------------------|--------|--------------------------|----------------------|---------------------------------|--------------------------|----------------------------------|---------------------------|----------------|-----------------|
| 2. Grist Mill EB L  | *      | 110                      | 60                   | 6.0                             | 1595                     | 3459                             | 127.94                    | 3              | 4               |
| 3. Grist Mill EB LT | *      | 110                      | 60                   | 6.0                             | 120                      | 354                              | 127.94                    | 3              | 4               |
| 4. Grist Mill EB R  | *      | 110                      | 48                   | 6.0                             | 449                      | 1463                             | 127.94                    | 3              | 4               |
| 7. Grist Mill WB LT | *      | 110                      | 100                  | 5.0                             | 107                      | 960                              | 127.94                    | 3              | 3               |
| 8. Grist Mill WB TR | *      | 110                      | 100                  | 5.0                             | 41                       | 2558                             | 127.94                    | 3              | 3               |
| 11. Main NB L       | *      | 110                      | 63                   | 4.0                             | 193                      | 405                              | 127.94                    | 3              | 4               |
| 12. Main NB TR      | *      | 110                      | 61                   | 6.0                             | 430                      | 1718                             | 127.94                    | 3              | 4               |
| 15. Main SB L       | *      | 110                      | 71                   | 6.0                             | 32                       | 1563                             | 127.94                    | 3              | 4               |
| 16. Main SB T       | *      | 110                      | 71                   | 6.0                             | 696                      | 2068                             | 127.94                    | 3              | 4               |
| 17. Main SB R       | *      | 110                      | 22                   | 6.0                             | 1331                     | 1668                             | 127.94                    | 3              | 4               |

-----  
 RECEPTOR LOCATIONS  
 -----

| RECEPTOR          | *<br>* | COORDINATES (FT) |       |     | *<br>* |
|-------------------|--------|------------------|-------|-----|--------|
|                   |        | X                | Y     | Z   |        |
| 1. EB W Midblock  | *      | 196.0            | 384.0 | 6.0 | *      |
| 2. SW corner      | *      | 394.0            | 384.0 | 6.0 | *      |
| 3. SB S Midblock  | *      | 394.0            | 200.0 | 6.0 | *      |
| 4. NB S Midblock  | *      | 466.0            | 200.0 | 6.0 | *      |
| 5. SE corner      | *      | 466.0            | 390.0 | 6.0 | *      |
| 6. EB E Midblock  | *      | 648.0            | 390.0 | 6.0 | *      |
| 7. WB E Midblock  | *      | 648.0            | 464.0 | 6.0 | *      |
| 8. NE corner      | *      | 476.0            | 464.0 | 6.0 | *      |
| 9. NB N Midblock  | *      | 476.0            | 640.0 | 6.0 | *      |
| 10. SB N Midblock | *      | 396.0            | 640.0 | 6.0 | *      |
| 11. NW corner     | *      | 396.0            | 464.0 | 6.0 | *      |
| 12. WB W Midblock | *      | 196.0            | 464.0 | 6.0 | *      |

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

| WIND ANGLE (DEGR)* | REC1 | REC2 | REC3 | REC4 | REC5 | REC6 | REC7 | REC8 | REC9 | REC10 | REC11 | REC12 |
|--------------------|------|------|------|------|------|------|------|------|------|-------|-------|-------|
| 0.                 | 5.3  | 5.7  | 5.7  | 5.9  | 5.8  | 5.4  | 4.3  | 4.8  | 4.6  | 4.6   | 4.9   | 4.3   |
| 10.                | 5.5  | 6.1  | 6.2  | 5.2  | 5.5  | 5.3  | 4.3  | 4.5  | 4.3  | 4.9   | 5.5   | 4.3   |
| 20.                | 5.5  | 6.3  | 6.6  | 4.7  | 5.5  | 5.1  | 4.3  | 4.3  | 4.3  | 5.2   | 5.6   | 4.3   |
| 30.                | 5.9  | 6.2  | 6.6  | 4.6  | 5.5  | 5.1  | 4.3  | 4.3  | 4.3  | 5.3   | 5.5   | 4.4   |
| 40.                | 6.2  | 6.2  | 6.4  | 4.6  | 5.7  | 5.2  | 4.3  | 4.3  | 4.3  | 5.3   | 5.5   | 4.5   |
| 50.                | 6.1  | 6.2  | 6.3  | 4.5  | 5.7  | 5.2  | 4.3  | 4.3  | 4.3  | 5.2   | 5.4   | 4.6   |
| 60.                | 6.2  | 6.5  | 6.1  | 4.5  | 5.8  | 5.3  | 4.3  | 4.3  | 4.3  | 5.2   | 5.3   | 4.5   |
| 70.                | 6.2  | 6.6  | 6.1  | 4.4  | 5.8  | 5.3  | 4.3  | 4.3  | 4.3  | 5.2   | 5.3   | 4.6   |
| 80.                | 6.0  | 6.8  | 5.8  | 4.4  | 5.6  | 5.2  | 4.5  | 4.7  | 4.3  | 5.3   | 5.8   | 5.0   |
| 90.                | 5.6  | 6.4  | 5.6  | 4.4  | 5.2  | 5.0  | 4.8  | 5.2  | 4.4  | 5.3   | 6.3   | 5.5   |
| 100.               | 5.1  | 5.9  | 5.6  | 4.3  | 4.7  | 4.6  | 5.0  | 5.6  | 4.4  | 5.4   | 6.6   | 5.9   |
| 110.               | 4.7  | 5.7  | 5.5  | 4.3  | 4.3  | 4.3  | 5.0  | 5.8  | 4.5  | 5.5   | 6.7   | 6.0   |
| 120.               | 4.7  | 5.8  | 5.5  | 4.3  | 4.3  | 4.3  | 5.1  | 5.8  | 4.5  | 5.7   | 6.6   | 6.1   |
| 130.               | 4.5  | 5.9  | 5.5  | 4.3  | 4.3  | 4.3  | 5.0  | 5.7  | 4.5  | 5.6   | 6.4   | 6.1   |
| 140.               | 4.5  | 6.0  | 5.6  | 4.3  | 4.3  | 4.3  | 5.0  | 5.7  | 4.6  | 5.9   | 6.6   | 5.9   |
| 150.               | 4.6  | 6.1  | 5.7  | 4.3  | 4.3  | 4.3  | 4.9  | 5.5  | 4.6  | 6.0   | 6.7   | 5.9   |
| 160.               | 4.4  | 6.3  | 5.9  | 4.3  | 4.4  | 4.3  | 5.1  | 5.5  | 4.7  | 6.2   | 6.8   | 5.6   |
| 170.               | 4.4  | 6.1  | 5.8  | 4.4  | 4.8  | 4.3  | 5.4  | 5.9  | 4.9  | 6.1   | 6.9   | 5.6   |
| 180.               | 4.3  | 5.5  | 5.3  | 4.9  | 5.5  | 4.3  | 5.6  | 6.4  | 5.6  | 5.6   | 6.4   | 5.4   |
| 190.               | 4.3  | 4.8  | 4.7  | 5.3  | 6.0  | 4.4  | 6.0  | 6.7  | 5.9  | 5.1   | 5.7   | 5.2   |
| 200.               | 4.3  | 4.4  | 4.3  | 5.4  | 6.0  | 4.4  | 6.3  | 6.6  | 5.8  | 4.7   | 5.4   | 5.2   |
| 210.               | 4.3  | 4.3  | 4.3  | 5.4  | 5.9  | 4.6  | 6.6  | 6.5  | 5.7  | 4.6   | 5.2   | 5.3   |
| 220.               | 4.3  | 4.3  | 4.3  | 5.4  | 5.7  | 4.5  | 6.8  | 6.4  | 5.7  | 4.7   | 5.3   | 5.4   |
| 230.               | 4.3  | 4.3  | 4.3  | 5.3  | 5.5  | 4.7  | 6.7  | 6.1  | 5.6  | 4.6   | 5.4   | 5.4   |
| 240.               | 4.3  | 4.3  | 4.3  | 5.2  | 5.5  | 4.7  | 6.8  | 6.3  | 5.6  | 4.6   | 5.5   | 5.5   |
| 250.               | 4.3  | 4.3  | 4.3  | 5.2  | 5.4  | 4.7  | 6.5  | 6.6  | 5.4  | 4.5   | 5.9   | 5.5   |
| 260.               | 4.5  | 4.6  | 4.3  | 5.4  | 5.9  | 5.0  | 6.1  | 6.5  | 5.3  | 4.4   | 5.6   | 5.3   |
| 270.               | 4.9  | 5.1  | 4.3  | 5.5  | 6.1  | 5.6  | 5.5  | 6.0  | 5.1  | 4.3   | 5.1   | 4.9   |
| 280.               | 5.4  | 5.4  | 4.4  | 5.7  | 6.3  | 5.9  | 4.9  | 5.5  | 5.2  | 4.3   | 4.6   | 4.5   |
| 290.               | 5.5  | 5.5  | 4.4  | 5.9  | 6.2  | 6.0  | 4.6  | 5.2  | 5.0  | 4.3   | 4.4   | 4.4   |
| 300.               | 5.5  | 5.2  | 4.6  | 6.3  | 6.2  | 6.1  | 4.5  | 5.2  | 5.1  | 4.3   | 4.3   | 4.3   |
| 310.               | 5.4  | 5.1  | 4.6  | 6.4  | 6.1  | 5.9  | 4.6  | 5.2  | 5.2  | 4.3   | 4.3   | 4.3   |
| 320.               | 5.4  | 5.1  | 4.8  | 6.6  | 6.2  | 6.1  | 4.5  | 5.3  | 5.2  | 4.3   | 4.3   | 4.3   |
| 330.               | 5.2  | 5.0  | 4.7  | 6.6  | 6.1  | 5.9  | 4.4  | 5.4  | 5.2  | 4.3   | 4.3   | 4.3   |
| 340.               | 5.2  | 5.0  | 4.6  | 6.5  | 6.3  | 5.7  | 4.3  | 5.3  | 5.0  | 4.3   | 4.3   | 4.3   |
| 350.               | 5.2  | 5.4  | 5.0  | 6.3  | 6.2  | 5.6  | 4.3  | 5.1  | 4.8  | 4.4   | 4.7   | 4.3   |
| 360.               | 5.3  | 5.7  | 5.7  | 5.9  | 5.8  | 5.4  | 4.3  | 4.8  | 4.6  | 4.6   | 4.9   | 4.3   |
| MAX                | 6.2  | 6.8  | 6.6  | 6.6  | 6.3  | 6.1  | 6.8  | 6.7  | 5.9  | 6.2   | 6.9   | 6.1   |
| DEGR.              | 40   | 80   | 20   | 320  | 280  | 300  | 220  | 190  | 190  | 160   | 170   | 120   |

THE HIGHEST CONCENTRATION OF 6.90 PPM OCCURRED AT RECEPTOR REC11.



DATE : 4/15/11  
 TIME : 13:50: 8

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING  
 THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

| LINK # | *<br>*<br>*<br>* | CO/LINK (PPM) |            |            |             |             |             |             |             |             |              |              |              |
|--------|------------------|---------------|------------|------------|-------------|-------------|-------------|-------------|-------------|-------------|--------------|--------------|--------------|
|        |                  | REC1<br>40    | REC2<br>80 | REC3<br>20 | REC4<br>320 | REC5<br>280 | REC6<br>300 | REC7<br>220 | REC8<br>190 | REC9<br>190 | REC10<br>160 | REC11<br>170 | REC12<br>120 |
| 1      | *                | .0            | .0         | .0         | .0          | .1          | .0          | .0          | .0          | .0          | .0           | .0           | .0           |
| 2      | *                | .3            | .5         | .1         | .1          | .3          | .4          | .3          | .3          | .1          | .1           | .3           | .4           |
| 3      | *                | .4            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .1           |
| 4      | *                | .4            | .0         | .0         | .0          | .1          | .0          | .0          | .0          | .0          | .0           | .0           | .1           |
| 5      | *                | .0            | .4         | .1         | .0          | .0          | .6          | .4          | .2          | .0          | .1           | .0           | .0           |
| 6      | *                | .0            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .0           |
| 7      | *                | .5            | .3         | .2         | .2          | .6          | .6          | .7          | .6          | .2          | .2           | .6           | .8           |
| 8      | *                | .0            | .0         | .0         | .0          | .0          | .0          | .7          | .0          | .0          | .0           | .0           | .0           |
| 9      | *                | .0            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .0           |
| 10     | *                | .0            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .0           |
| 11     | *                | .1            | .3         | .4         | .5          | .4          | .1          | .1          | .3          | .4          | .4           | .3           | .1           |
| 12     | *                | .0            | .0         | .2         | .6          | .0          | .0          | .1          | .2          | .1          | .0           | .1           | .1           |
| 13     | *                | .0            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .2          | .1           | .0           | .0           |
| 14     | *                | .1            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .0           |
| 15     | *                | .0            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .0           |
| 16     | *                | .1            | .4         | .6         | .4          | .3          | .1          | .1          | .4          | .4          | .6           | .6           | .1           |
| 17     | *                | .0            | .2         | .2         | .1          | .1          | .0          | .0          | .1          | .1          | .3           | .3           | .0           |
| 18     | *                | .0            | .4         | .5         | .4          | .1          | .0          | .1          | .3          | .1          | .1           | .4           | .1           |

JOB: GristMillMain2030NoBuildPM

RUN: GristMillMain2030NBPM

DATE : 4/15/11  
 TIME : 13:52:44

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S      VD = .0 CM/S      Z0 = 175. CM  
 U = 1.0 M/S      CLAS = 4 (D)      ATIM = 60. MINUTES      MIXH = 1000. M      AMB = 4.3 PPM

LINK VARIABLES

| LINK DESCRIPTION     | *<br>*<br>* | X1    | LINK COORDINATES (FT) |        | *<br>*<br>* | LENGTH<br>(FT) | BRG TYPE<br>(DEG) | VPH   | EF<br>(G/MI) | H<br>(FT) | W<br>(FT) | V/C  | QUEUE<br>(VEH) |
|----------------------|-------------|-------|-----------------------|--------|-------------|----------------|-------------------|-------|--------------|-----------|-----------|------|----------------|
|                      |             |       | Y1                    | X2     | Y2          |                |                   |       |              |           |           |      |                |
| 1. Grist Mill EB in  | *           | .0    | 412.0                 | 200.0  | 412.0       | 200.           | 90. AG            | 1635. | 8.3          | .0        | 36.0      |      |                |
| 2. Grist Mill EB L   | *           | 200.0 | 424.0                 | 3368.7 | 424.0       | 3169.          | 90. AG            | 196.  | 100.0        | .0        | 12.0      | 1.21 | 161.0          |
| 3. Grist Mill EB LT  | *           | 200.0 | 412.0                 | 200.3  | 412.0       | 0.             | 90. AG            | 196.  | 100.0        | .0        | 12.0      | .01  | .0             |
| 4. Grist Mill EB R   | *           | 200.0 | 400.0                 | 235.4  | 400.0       | 35.            | 90. AG            | 134.  | 100.0        | .0        | 12.0      | .21  | 1.8            |
| 5. Grist Mill EB out | *           | 466.0 | 418.0                 | 848.0  | 418.0       | 382.           | 90. AG            | 1635. | 8.3          | .0        | 24.0      |      |                |
| 6. Grist Mill WB in  | *           | 848.0 | 442.0                 | 648.0  | 442.0       | 200.           | 270. AG           | 32.   | 8.3          | .0        | 24.0      |      |                |
| 7. Grist Mill WB LT  | *           | 648.0 | 436.0                 | 473.0  | 436.0       | 175.           | 270. AG           | 316.  | 100.0        | .0        | 12.0      | 2.44 | 8.9            |
| 8. Grist Mill WB TR  | *           | 648.0 | 448.0                 | 642.8  | 448.0       | 5.             | 270. AG           | 316.  | 100.0        | .0        | 12.0      | .40  | .3             |
| 9. Grist Mill WB out | *           | 406.0 | 442.0                 | .0     | 442.0       | 406.           | 270. AG           | 32.   | 8.3          | .0        | 24.0      |      |                |
| 10. Main NB in       | *           | 444.0 | .0                    | 444.0  | 200.0       | 200.           | 360. AG           | 1041. | 8.3          | .0        | 24.0      |      |                |
| 11. Main NB L        | *           | 438.0 | 200.0                 | 438.0  | 1651.7      | 1452.          | 360. AG           | 182.  | 100.0        | .0        | 12.0      | 1.65 | 73.7           |
| 12. Main NB TR       | *           | 450.0 | 200.0                 | 450.0  | 615.9       | 416.           | 360. AG           | 175.  | 100.0        | .0        | 12.0      | 1.02 | 21.1           |
| 13. Main NB out      | *           | 454.0 | 454.0                 | 454.0  | 836.0       | 382.           | 360. AG           | 1041. | 8.3          | .0        | 24.0      |      |                |
| 14. Main SB in       | *           | 424.0 | 836.0                 | 424.0  | 636.0       | 200.           | 180. AG           | 1798. | 8.3          | .0        | 36.0      |      |                |
| 15. Main SB L        | *           | 436.0 | 636.0                 | 436.0  | 633.7       | 2.             | 180. AG           | 237.  | 100.0        | .0        | 12.0      | .02  | .1             |
| 16. Main SB T        | *           | 424.0 | 636.0                 | 424.0  | 423.8       | 212.           | 180. AG           | 237.  | 100.0        | .0        | 12.0      | .94  | 10.8           |
| 17. Main SB R        | *           | 412.0 | 636.0                 | 412.0  | -2145.7     | 2782.          | 180. AG           | 89.   | 100.0        | .0        | 12.0      | 1.22 | 141.3          |
| 18. Main SB out      | *           | 420.0 | 396.0                 | 420.0  | .0          | 396.           | 180. AG           | 1798. | 8.3          | .0        | 24.0      |      |                |

DATE : 4/15/11  
 TIME : 13:52:44

-----  
 ADDITIONAL QUEUE LINK PARAMETERS  
 -----

| LINK DESCRIPTION    | *<br>* | CYCLE<br>LENGTH<br>(SEC) | RED<br>TIME<br>(SEC) | CLEARANCE<br>LOST TIME<br>(SEC) | APPROACH<br>VOL<br>(VPH) | SATURATION<br>FLOW RATE<br>(VPH) | IDLE<br>EM FAC<br>(gm/hr) | SIGNAL<br>TYPE | ARRIVAL<br>RATE |
|---------------------|--------|--------------------------|----------------------|---------------------------------|--------------------------|----------------------------------|---------------------------|----------------|-----------------|
| 2. Grist Mill EB L  | *      | 100                      | 57                   | 6.0                             | 1469                     | 3459                             | 127.94                    | 3              | 4               |
| 3. Grist Mill EB LT | *      | 100                      | 57                   | 6.0                             | 1                        | 354                              | 127.94                    | 3              | 4               |
| 4. Grist Mill EB R  | *      | 100                      | 39                   | 6.0                             | 166                      | 1463                             | 127.94                    | 3              | 4               |
| 7. Grist Mill WB LT | *      | 100                      | 92                   | 5.0                             | 22                       | 960                              | 127.94                    | 3              | 3               |
| 8. Grist Mill WB TR | *      | 100                      | 92                   | 5.0                             | 10                       | 2558                             | 127.94                    | 3              | 3               |
| 11. Main NB L       | *      | 100                      | 53                   | 4.0                             | 326                      | 485                              | 127.94                    | 3              | 4               |
| 12. Main NB TR      | *      | 100                      | 51                   | 6.0                             | 715                      | 1718                             | 127.94                    | 3              | 4               |
| 15. Main SB L       | *      | 100                      | 69                   | 6.0                             | 6                        | 1563                             | 127.94                    | 3              | 4               |
| 16. Main SB T       | *      | 100                      | 69                   | 6.0                             | 446                      | 2068                             | 127.94                    | 3              | 4               |
| 17. Main SB R       | *      | 100                      | 26                   | 6.0                             | 1346                     | 1668                             | 127.94                    | 3              | 4               |

-----  
 RECEPTOR LOCATIONS  
 -----

| RECEPTOR          | *<br>* | COORDINATES (FT) |       |     | *<br>* |
|-------------------|--------|------------------|-------|-----|--------|
|                   |        | X                | Y     | Z   |        |
| 1. EB W Midblock  | *      | 196.0            | 384.0 | 6.0 | *      |
| 2. SW corner      | *      | 394.0            | 384.0 | 6.0 | *      |
| 3. SB S Midblock  | *      | 394.0            | 200.0 | 6.0 | *      |
| 4. NB S Midblock  | *      | 466.0            | 200.0 | 6.0 | *      |
| 5. SE corner      | *      | 466.0            | 390.0 | 6.0 | *      |
| 6. EB E Midblock  | *      | 648.0            | 390.0 | 6.0 | *      |
| 7. WB E Midblock  | *      | 648.0            | 464.0 | 6.0 | *      |
| 8. NE corner      | *      | 476.0            | 464.0 | 6.0 | *      |
| 9. NB N Midblock  | *      | 476.0            | 640.0 | 6.0 | *      |
| 10. SB N Midblock | *      | 396.0            | 640.0 | 6.0 | *      |
| 11. NW corner     | *      | 396.0            | 464.0 | 6.0 | *      |
| 12. WB W Midblock | *      | 196.0            | 464.0 | 6.0 | *      |

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

| WIND ANGLE (DEGR) | REC1 | REC2 | REC3 | REC4 | REC5 | REC6 | REC7 | REC8 | REC9 | REC10 | REC11 | REC12 |
|-------------------|------|------|------|------|------|------|------|------|------|-------|-------|-------|
| 0.                | 4.8  | 5.7  | 5.4  | 5.8  | 6.2  | 5.1  | 4.3  | 5.2  | 4.9  | 4.9   | 5.2   | 4.3   |
| 10.               | 5.0  | 6.0  | 5.9  | 5.0  | 5.5  | 5.0  | 4.3  | 4.6  | 4.5  | 5.3   | 5.7   | 4.4   |
| 20.               | 4.9  | 6.1  | 6.2  | 4.7  | 5.4  | 4.9  | 4.3  | 4.3  | 4.3  | 5.4   | 6.0   | 4.4   |
| 30.               | 5.2  | 6.1  | 6.1  | 4.6  | 5.4  | 5.1  | 4.3  | 4.3  | 4.3  | 5.4   | 6.0   | 4.5   |
| 40.               | 5.2  | 6.0  | 6.0  | 4.6  | 5.6  | 5.1  | 4.3  | 4.3  | 4.3  | 5.3   | 5.9   | 4.5   |
| 50.               | 5.4  | 5.9  | 5.7  | 4.5  | 5.6  | 5.1  | 4.3  | 4.3  | 4.3  | 5.2   | 5.8   | 4.7   |
| 60.               | 5.3  | 6.0  | 5.6  | 4.5  | 5.6  | 5.1  | 4.3  | 4.3  | 4.3  | 5.1   | 5.6   | 4.6   |
| 70.               | 5.4  | 6.2  | 5.5  | 4.5  | 5.7  | 5.2  | 4.3  | 4.3  | 4.3  | 5.1   | 5.5   | 4.7   |
| 80.               | 5.4  | 6.4  | 5.4  | 4.4  | 5.5  | 5.1  | 4.5  | 4.6  | 4.3  | 5.1   | 6.0   | 4.9   |
| 90.               | 5.4  | 6.1  | 5.3  | 4.4  | 5.1  | 4.9  | 4.8  | 5.1  | 4.4  | 5.3   | 6.5   | 5.3   |
| 100.              | 4.8  | 5.7  | 5.2  | 4.3  | 4.6  | 4.6  | 5.0  | 5.6  | 4.4  | 5.3   | 6.7   | 5.3   |
| 110.              | 4.6  | 5.4  | 5.0  | 4.3  | 4.3  | 4.3  | 5.0  | 5.8  | 4.5  | 5.5   | 6.5   | 5.3   |
| 120.              | 4.7  | 5.4  | 5.1  | 4.3  | 4.3  | 4.3  | 5.0  | 5.7  | 4.5  | 5.9   | 6.2   | 5.1   |
| 130.              | 4.5  | 5.4  | 5.1  | 4.3  | 4.3  | 4.3  | 5.0  | 5.7  | 4.5  | 5.9   | 6.1   | 5.1   |
| 140.              | 4.5  | 5.7  | 5.3  | 4.3  | 4.3  | 4.3  | 4.9  | 5.6  | 4.6  | 6.3   | 5.9   | 4.9   |
| 150.              | 4.5  | 5.6  | 5.3  | 4.3  | 4.3  | 4.3  | 5.0  | 5.5  | 4.6  | 6.3   | 5.8   | 4.9   |
| 160.              | 4.4  | 5.6  | 5.2  | 4.3  | 4.4  | 4.3  | 5.1  | 5.3  | 4.7  | 6.5   | 5.9   | 4.7   |
| 170.              | 4.4  | 5.6  | 5.2  | 4.5  | 4.8  | 4.3  | 5.3  | 5.5  | 4.9  | 6.0   | 5.7   | 4.8   |
| 180.              | 4.3  | 5.0  | 4.8  | 4.7  | 5.3  | 4.3  | 5.5  | 5.8  | 5.6  | 5.4   | 5.4   | 4.7   |
| 190.              | 4.3  | 4.6  | 4.6  | 5.0  | 5.7  | 4.4  | 5.7  | 6.0  | 6.0  | 4.9   | 5.0   | 4.6   |
| 200.              | 4.3  | 4.3  | 4.3  | 5.1  | 5.8  | 4.4  | 5.8  | 6.2  | 6.2  | 4.5   | 4.7   | 4.6   |
| 210.              | 4.3  | 4.3  | 4.3  | 5.1  | 5.8  | 4.5  | 5.9  | 5.8  | 6.0  | 4.4   | 4.6   | 4.6   |
| 220.              | 4.3  | 4.3  | 4.3  | 5.0  | 5.7  | 4.5  | 6.1  | 5.6  | 5.8  | 4.4   | 4.6   | 4.6   |
| 230.              | 4.3  | 4.3  | 4.3  | 5.0  | 5.6  | 4.7  | 6.2  | 5.9  | 5.6  | 4.4   | 4.7   | 4.6   |
| 240.              | 4.3  | 4.3  | 4.3  | 4.9  | 5.6  | 4.6  | 6.0  | 5.8  | 5.5  | 4.4   | 4.7   | 4.6   |
| 250.              | 4.3  | 4.3  | 4.3  | 5.0  | 5.5  | 4.6  | 5.9  | 5.8  | 5.3  | 4.3   | 4.7   | 4.5   |
| 260.              | 4.4  | 4.4  | 4.3  | 5.1  | 5.5  | 4.8  | 5.7  | 5.9  | 5.2  | 4.3   | 4.6   | 4.5   |
| 270.              | 4.5  | 4.5  | 4.3  | 5.2  | 5.7  | 5.2  | 5.2  | 5.9  | 5.1  | 4.3   | 4.5   | 4.4   |
| 280.              | 4.7  | 4.6  | 4.3  | 5.3  | 5.7  | 5.6  | 4.9  | 5.6  | 5.1  | 4.3   | 4.3   | 4.3   |
| 290.              | 4.8  | 4.7  | 4.3  | 5.4  | 5.8  | 5.9  | 4.7  | 5.6  | 5.1  | 4.3   | 4.3   | 4.3   |
| 300.              | 4.8  | 4.7  | 4.4  | 5.6  | 5.8  | 6.0  | 4.7  | 5.7  | 5.2  | 4.3   | 4.3   | 4.3   |
| 310.              | 4.8  | 4.7  | 4.4  | 5.7  | 5.9  | 6.0  | 4.7  | 5.7  | 5.2  | 4.3   | 4.3   | 4.3   |
| 320.              | 4.7  | 4.6  | 4.4  | 5.8  | 6.1  | 6.1  | 4.6  | 5.8  | 5.2  | 4.3   | 4.3   | 4.3   |
| 330.              | 4.7  | 4.6  | 4.4  | 5.9  | 6.4  | 5.9  | 4.5  | 5.9  | 5.3  | 4.3   | 4.3   | 4.3   |
| 340.              | 4.7  | 4.6  | 4.4  | 6.1  | 6.4  | 5.4  | 4.4  | 6.0  | 5.3  | 4.3   | 4.3   | 4.3   |
| 350.              | 4.7  | 4.9  | 4.8  | 6.0  | 6.6  | 5.3  | 4.4  | 5.6  | 5.2  | 4.5   | 4.7   | 4.3   |
| 360.              | 4.8  | 5.7  | 5.4  | 5.8  | 6.2  | 5.1  | 4.3  | 5.2  | 4.9  | 4.9   | 5.2   | 4.3   |
| MAX               | 5.4  | 6.4  | 6.2  | 6.1  | 6.6  | 6.1  | 6.2  | 6.2  | 6.2  | 6.5   | 6.7   | 5.3   |
| DEGR.             | 50   | 80   | 20   | 340  | 350  | 320  | 230  | 200  | 200  | 160   | 100   | 90    |

THE HIGHEST CONCENTRATION OF 6.70 PPM OCCURRED AT RECEPTOR REC11.

DATE : 4/15/11  
 TIME : 13:52:44

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING  
 THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

| LINK # | *<br>*<br>*<br>* | CO/LINK (PPM) |            |            |             |             |             |             |             |             |              |              |             |
|--------|------------------|---------------|------------|------------|-------------|-------------|-------------|-------------|-------------|-------------|--------------|--------------|-------------|
|        |                  | REC1<br>50    | REC2<br>80 | REC3<br>20 | REC4<br>340 | REC5<br>350 | REC6<br>320 | REC7<br>230 | REC8<br>200 | REC9<br>200 | REC10<br>160 | REC11<br>100 | REC12<br>90 |
| 1      | *                | .0            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .0          |
| 2      | *                | .4            | .5         | .1         | .1          | .3          | .4          | .4          | .3          | .1          | .1           | .5           | .4          |
| 3      | *                | .0            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .0          |
| 4      | *                | .3            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .0          |
| 5      | *                | .0            | .3         | .1         | .0          | .1          | .4          | .3          | .1          | .0          | .1           | .2           | .1          |
| 6      | *                | .0            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .0          |
| 7      | *                | .0            | .3         | .1         | .0          | .1          | .5          | .7          | .1          | .0          | .1           | .4           | .1          |
| 8      | *                | .0            | .0         | .0         | .0          | .0          | .0          | .1          | .0          | .0          | .0           | .0           | .0          |
| 9      | *                | .0            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .0          |
| 10     | *                | .0            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .0          |
| 11     | *                | .1            | .3         | .4         | .5          | .5          | .1          | .1          | .4          | .4          | .4           | .3           | .1          |
| 12     | *                | .1            | .2         | .3         | .7          | .6          | .1          | .1          | .5          | .5          | .3           | .2           | .1          |
| 13     | *                | .1            | .0         | .0         | .0          | .2          | .1          | .0          | .0          | .3          | .1           | .1           | .0          |
| 14     | *                | .0            | .0         | .0         | .0          | .1          | .1          | .0          | .0          | .0          | .0           | .0           | .0          |
| 15     | *                | .0            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .0          |
| 16     | *                | .1            | .0         | .1         | .1          | .3          | .1          | .0          | .0          | .3          | .6           | .5           | .1          |
| 17     | *                | .0            | .2         | .3         | .1          | .1          | .0          | .1          | .2          | .2          | .4           | .2           | .1          |
| 18     | *                | .0            | .3         | .5         | .3          | .0          | .0          | .1          | .3          | .1          | .1           | .0           | .0          |

JOB: GristMillMain2030BuildAM

RUN: GristMillMain2030BuildAM

DATE : 4/15/11  
 TIME : 13:54:38

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S      VD = .0 CM/S      Z0 = 175. CM  
 U = 1.0 M/S      CLAS = 4 (D)      ATIM = 60. MINUTES      MIXH = 1000. M      AMB = 4.3 PPM

LINK VARIABLES

| LINK DESCRIPTION     | *<br>*<br>* | X1    | LINK COORDINATES (FT) |        | *<br>*<br>* | LENGTH<br>(FT) | BRG TYPE<br>(DEG) | VPH   | EF<br>(G/MI) | H<br>(FT) | W<br>(FT) | V/C  | QUEUE<br>(VEH) |
|----------------------|-------------|-------|-----------------------|--------|-------------|----------------|-------------------|-------|--------------|-----------|-----------|------|----------------|
|                      |             |       | Y1                    | X2     | Y2          |                |                   |       |              |           |           |      |                |
| 1. Grist Mill EB in  | *           | .0    | 412.0                 | 200.0  | 412.0       | 200.           | 90. AG            | 2164. | 8.3          | .0        | 36.0      |      |                |
| 2. Grist Mill EB L   | *           | 200.0 | 424.0                 | 3595.4 | 424.0       | 3395.          | 90. AG            | 187.  | 100.0        | .0        | 12.0      | 1.21 | 172.5          |
| 3. Grist Mill EB LT  | *           | 200.0 | 412.0                 | 260.0  | 412.0       | 60.            | 90. AG            | 187.  | 100.0        | .0        | 12.0      | .89  | 3.1            |
| 4. Grist Mill EB R   | *           | 200.0 | 400.0                 | 317.8  | 400.0       | 118.           | 90. AG            | 150.  | 100.0        | .0        | 12.0      | .63  | 6.0            |
| 5. Grist Mill EB out | *           | 466.0 | 418.0                 | 848.0  | 418.0       | 382.           | 90. AG            | 2164. | 8.3          | .0        | 24.0      |      |                |
| 6. Grist Mill WB in  | *           | 848.0 | 442.0                 | 648.0  | 442.0       | 200.           | 270. AG           | 148.  | 8.3          | .0        | 24.0      |      |                |
| 7. Grist Mill WB LT  | *           | 648.0 | 436.0                 | -310.6 | 436.0       | 959.           | 270. AG           | 312.  | 100.0        | .0        | 12.0      | 4.12 | 48.7           |
| 8. Grist Mill WB TR  | *           | 648.0 | 448.0                 | 623.6  | 448.0       | 24.            | 270. AG           | 312.  | 100.0        | .0        | 12.0      | .59  | 1.2            |
| 9. Grist Mill WB out | *           | 406.0 | 442.0                 | .0     | 442.0       | 406.           | 270. AG           | 148.  | 8.3          | .0        | 24.0      |      |                |
| 10. Main NB in       | *           | 444.0 | .0                    | 444.0  | 200.0       | 200.           | 360. AG           | 623.  | 8.3          | .0        | 24.0      |      |                |
| 11. Main NB L        | *           | 438.0 | 200.0                 | 438.0  | 755.8       | 556.           | 360. AG           | 197.  | 100.0        | .0        | 12.0      | 1.29 | 28.2           |
| 12. Main NB TR       | *           | 450.0 | 200.0                 | 450.0  | 343.4       | 143.           | 360. AG           | 190.  | 100.0        | .0        | 12.0      | .67  | 7.3            |
| 13. Main NB out      | *           | 454.0 | 454.0                 | 454.0  | 836.0       | 382.           | 360. AG           | 623.  | 8.3          | .0        | 24.0      |      |                |
| 14. Main SB in       | *           | 424.0 | 836.0                 | 424.0  | 636.0       | 200.           | 180. AG           | 2059. | 8.3          | .0        | 36.0      |      |                |
| 15. Main SB L        | *           | 436.0 | 636.0                 | 436.0  | 623.6       | 12.            | 180. AG           | 222.  | 100.0        | .0        | 12.0      | .07  | .6             |
| 16. Main SB T        | *           | 424.0 | 636.0                 | 424.0  | -869.0      | 1505.          | 180. AG           | 222.  | 100.0        | .0        | 12.0      | 1.20 | 76.5           |
| 17. Main SB R        | *           | 412.0 | 636.0                 | 412.0  | -845.9      | 1482.          | 180. AG           | 69.   | 100.0        | .0        | 12.0      | 1.10 | 75.3           |
| 18. Main SB out      | *           | 420.0 | 396.0                 | 420.0  | .0          | 396.           | 180. AG           | 2059. | 8.3          | .0        | 24.0      |      |                |

DATE : 4/15/11  
 TIME : 13:54:38

-----  
 ADDITIONAL QUEUE LINK PARAMETERS  
 -----

| LINK DESCRIPTION    | *<br>* | CYCLE<br>LENGTH<br>(SEC) | RED<br>TIME<br>(SEC) | CLEARANCE<br>LOST TIME<br>(SEC) | APPROACH<br>VOL<br>(VPH) | SATURATION<br>FLOW RATE<br>(VPH) | IDLE<br>EM FAC<br>(gm/hr) | SIGNAL<br>TYPE | ARRIVAL<br>RATE |
|---------------------|--------|--------------------------|----------------------|---------------------------------|--------------------------|----------------------------------|---------------------------|----------------|-----------------|
| 2. Grist Mill EB L  | *      | 110                      | 60                   | 6.0                             | 1595                     | 3459                             | 127.94                    | 3              | 4               |
| 3. Grist Mill EB LT | *      | 110                      | 60                   | 6.0                             | 120                      | 354                              | 127.94                    | 3              | 4               |
| 4. Grist Mill EB R  | *      | 110                      | 48                   | 6.0                             | 449                      | 1463                             | 127.94                    | 3              | 4               |
| 7. Grist Mill WB LT | *      | 110                      | 100                  | 5.0                             | 107                      | 960                              | 127.94                    | 3              | 3               |
| 8. Grist Mill WB TR | *      | 110                      | 100                  | 5.0                             | 41                       | 2558                             | 127.94                    | 3              | 3               |
| 11. Main NB L       | *      | 110                      | 63                   | 4.0                             | 193                      | 405                              | 127.94                    | 3              | 4               |
| 12. Main NB TR      | *      | 110                      | 61                   | 6.0                             | 430                      | 1718                             | 127.94                    | 3              | 4               |
| 15. Main SB L       | *      | 110                      | 71                   | 6.0                             | 32                       | 1563                             | 127.94                    | 3              | 4               |
| 16. Main SB T       | *      | 110                      | 71                   | 6.0                             | 696                      | 2068                             | 127.94                    | 3              | 4               |
| 17. Main SB R       | *      | 110                      | 22                   | 6.0                             | 1331                     | 1668                             | 127.94                    | 3              | 4               |

-----  
 RECEPTOR LOCATIONS  
 -----

| RECEPTOR          | *<br>* | COORDINATES (FT) |       |     | *<br>* |
|-------------------|--------|------------------|-------|-----|--------|
|                   |        | X                | Y     | Z   |        |
| 1. EB W Midblock  | *      | 196.0            | 384.0 | 6.0 | *      |
| 2. SW corner      | *      | 394.0            | 384.0 | 6.0 | *      |
| 3. SB S Midblock  | *      | 394.0            | 200.0 | 6.0 | *      |
| 4. NB S Midblock  | *      | 466.0            | 200.0 | 6.0 | *      |
| 5. SE corner      | *      | 466.0            | 390.0 | 6.0 | *      |
| 6. EB E Midblock  | *      | 648.0            | 390.0 | 6.0 | *      |
| 7. WB E Midblock  | *      | 648.0            | 464.0 | 6.0 | *      |
| 8. NE corner      | *      | 476.0            | 464.0 | 6.0 | *      |
| 9. NB N Midblock  | *      | 476.0            | 640.0 | 6.0 | *      |
| 10. SB N Midblock | *      | 396.0            | 640.0 | 6.0 | *      |
| 11. NW corner     | *      | 396.0            | 464.0 | 6.0 | *      |
| 12. WB W Midblock | *      | 196.0            | 464.0 | 6.0 | *      |

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

| WIND ANGLE (DEGR) | REC1 | REC2 | REC3 | REC4 | REC5 | REC6 | REC7 | REC8 | REC9 | REC10 | REC11 | REC12 |
|-------------------|------|------|------|------|------|------|------|------|------|-------|-------|-------|
| 0.                | 5.3  | 5.7  | 5.7  | 5.9  | 5.8  | 5.4  | 4.3  | 4.8  | 4.6  | 4.6   | 4.9   | 4.3   |
| 10.               | 5.5  | 6.1  | 6.2  | 5.2  | 5.5  | 5.3  | 4.3  | 4.5  | 4.3  | 4.9   | 5.5   | 4.3   |
| 20.               | 5.5  | 6.3  | 6.6  | 4.7  | 5.5  | 5.1  | 4.3  | 4.3  | 4.3  | 5.2   | 5.6   | 4.3   |
| 30.               | 5.9  | 6.2  | 6.6  | 4.6  | 5.5  | 5.1  | 4.3  | 4.3  | 4.3  | 5.3   | 5.5   | 4.4   |
| 40.               | 6.2  | 6.2  | 6.4  | 4.6  | 5.7  | 5.2  | 4.3  | 4.3  | 4.3  | 5.3   | 5.5   | 4.5   |
| 50.               | 6.1  | 6.2  | 6.3  | 4.5  | 5.7  | 5.2  | 4.3  | 4.3  | 4.3  | 5.2   | 5.4   | 4.6   |
| 60.               | 6.2  | 6.5  | 6.1  | 4.5  | 5.8  | 5.3  | 4.3  | 4.3  | 4.3  | 5.2   | 5.3   | 4.5   |
| 70.               | 6.2  | 6.6  | 6.1  | 4.4  | 5.8  | 5.3  | 4.3  | 4.3  | 4.3  | 5.2   | 5.3   | 4.6   |
| 80.               | 6.0  | 6.8  | 5.8  | 4.4  | 5.6  | 5.2  | 4.5  | 4.7  | 4.3  | 5.3   | 5.8   | 5.0   |
| 90.               | 5.6  | 6.4  | 5.6  | 4.4  | 5.2  | 5.0  | 4.8  | 5.2  | 4.4  | 5.3   | 6.3   | 5.5   |
| 100.              | 5.1  | 5.9  | 5.6  | 4.3  | 4.7  | 4.6  | 5.0  | 5.6  | 4.4  | 5.4   | 6.6   | 5.9   |
| 110.              | 4.7  | 5.7  | 5.5  | 4.3  | 4.3  | 4.3  | 5.0  | 5.8  | 4.5  | 5.5   | 6.7   | 6.0   |
| 120.              | 4.7  | 5.8  | 5.5  | 4.3  | 4.3  | 4.3  | 5.1  | 5.8  | 4.5  | 5.7   | 6.6   | 6.1   |
| 130.              | 4.5  | 5.9  | 5.5  | 4.3  | 4.3  | 4.3  | 5.0  | 5.7  | 4.5  | 5.6   | 6.4   | 6.1   |
| 140.              | 4.5  | 6.0  | 5.6  | 4.3  | 4.3  | 4.3  | 5.0  | 5.7  | 4.6  | 5.9   | 6.6   | 5.9   |
| 150.              | 4.6  | 6.1  | 5.7  | 4.3  | 4.3  | 4.3  | 4.9  | 5.5  | 4.6  | 6.0   | 6.7   | 5.9   |
| 160.              | 4.4  | 6.3  | 5.9  | 4.3  | 4.4  | 4.3  | 5.1  | 5.5  | 4.7  | 6.2   | 6.8   | 5.6   |
| 170.              | 4.4  | 6.1  | 5.8  | 4.4  | 4.8  | 4.3  | 5.4  | 5.9  | 4.9  | 6.1   | 6.9   | 5.6   |
| 180.              | 4.3  | 5.5  | 5.3  | 4.9  | 5.5  | 4.3  | 5.6  | 6.4  | 5.6  | 5.6   | 6.4   | 5.4   |
| 190.              | 4.3  | 4.8  | 4.7  | 5.3  | 6.0  | 4.4  | 6.0  | 6.7  | 5.9  | 5.1   | 5.7   | 5.2   |
| 200.              | 4.3  | 4.4  | 4.3  | 5.4  | 6.0  | 4.4  | 6.3  | 6.6  | 5.8  | 4.7   | 5.4   | 5.2   |
| 210.              | 4.3  | 4.3  | 4.3  | 5.4  | 5.9  | 4.6  | 6.6  | 6.5  | 5.7  | 4.6   | 5.2   | 5.3   |
| 220.              | 4.3  | 4.3  | 4.3  | 5.4  | 5.7  | 4.5  | 6.8  | 6.4  | 5.7  | 4.7   | 5.3   | 5.4   |
| 230.              | 4.3  | 4.3  | 4.3  | 5.3  | 5.5  | 4.7  | 6.7  | 6.1  | 5.6  | 4.6   | 5.4   | 5.4   |
| 240.              | 4.3  | 4.3  | 4.3  | 5.2  | 5.5  | 4.7  | 6.8  | 6.3  | 5.6  | 4.6   | 5.5   | 5.5   |
| 250.              | 4.3  | 4.3  | 4.3  | 5.2  | 5.4  | 4.7  | 6.5  | 6.6  | 5.4  | 4.5   | 5.9   | 5.5   |
| 260.              | 4.5  | 4.6  | 4.3  | 5.4  | 5.9  | 5.0  | 6.1  | 6.5  | 5.3  | 4.4   | 5.6   | 5.3   |
| 270.              | 4.9  | 5.1  | 4.3  | 5.5  | 6.1  | 5.6  | 5.5  | 6.0  | 5.1  | 4.3   | 5.1   | 4.9   |
| 280.              | 5.4  | 5.4  | 4.4  | 5.7  | 6.3  | 5.9  | 4.9  | 5.5  | 5.2  | 4.3   | 4.6   | 4.5   |
| 290.              | 5.5  | 5.5  | 4.4  | 5.9  | 6.2  | 6.0  | 4.6  | 5.2  | 5.0  | 4.3   | 4.4   | 4.4   |
| 300.              | 5.5  | 5.2  | 4.6  | 6.3  | 6.2  | 6.1  | 4.5  | 5.2  | 5.1  | 4.3   | 4.3   | 4.3   |
| 310.              | 5.4  | 5.1  | 4.6  | 6.4  | 6.1  | 5.9  | 4.6  | 5.2  | 5.2  | 4.3   | 4.3   | 4.3   |
| 320.              | 5.4  | 5.1  | 4.8  | 6.6  | 6.2  | 6.1  | 4.5  | 5.3  | 5.2  | 4.3   | 4.3   | 4.3   |
| 330.              | 5.2  | 5.0  | 4.7  | 6.6  | 6.1  | 5.9  | 4.4  | 5.4  | 5.2  | 4.3   | 4.3   | 4.3   |
| 340.              | 5.2  | 5.0  | 4.6  | 6.5  | 6.3  | 5.7  | 4.3  | 5.3  | 5.0  | 4.3   | 4.3   | 4.3   |
| 350.              | 5.2  | 5.4  | 5.0  | 6.3  | 6.2  | 5.6  | 4.3  | 5.1  | 4.8  | 4.4   | 4.7   | 4.3   |
| 360.              | 5.3  | 5.7  | 5.7  | 5.9  | 5.8  | 5.4  | 4.3  | 4.8  | 4.6  | 4.6   | 4.9   | 4.3   |
| MAX               | 6.2  | 6.8  | 6.6  | 6.6  | 6.3  | 6.1  | 6.8  | 6.7  | 5.9  | 6.2   | 6.9   | 6.1   |
| DEGR.             | 40   | 80   | 20   | 320  | 280  | 300  | 220  | 190  | 190  | 160   | 170   | 120   |

THE HIGHEST CONCENTRATION OF 6.90 PPM OCCURRED AT RECEPTOR REC11.



DATE : 4/15/11  
 TIME : 13:54:38

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING  
 THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

| LINK # | *<br>*<br>*<br>* | CO/LINK (PPM) |            |            |             |             |             |             |             |             |              |              |              |
|--------|------------------|---------------|------------|------------|-------------|-------------|-------------|-------------|-------------|-------------|--------------|--------------|--------------|
|        |                  | REC1<br>40    | REC2<br>80 | REC3<br>20 | REC4<br>320 | REC5<br>280 | REC6<br>300 | REC7<br>220 | REC8<br>190 | REC9<br>190 | REC10<br>160 | REC11<br>170 | REC12<br>120 |
| 1      | *                | .0            | .0         | .0         | .0          | .1          | .0          | .0          | .0          | .0          | .0           | .0           | .0           |
| 2      | *                | .3            | .5         | .1         | .1          | .3          | .4          | .3          | .3          | .1          | .1           | .3           | .4           |
| 3      | *                | .4            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .1           |
| 4      | *                | .4            | .0         | .0         | .0          | .1          | .0          | .0          | .0          | .0          | .0           | .0           | .1           |
| 5      | *                | .0            | .4         | .1         | .0          | .0          | .6          | .4          | .2          | .0          | .1           | .0           | .0           |
| 6      | *                | .0            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .0           |
| 7      | *                | .5            | .3         | .2         | .2          | .6          | .6          | .7          | .6          | .2          | .2           | .6           | .8           |
| 8      | *                | .0            | .0         | .0         | .0          | .0          | .0          | .7          | .0          | .0          | .0           | .0           | .0           |
| 9      | *                | .0            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .0           |
| 10     | *                | .0            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .0           |
| 11     | *                | .1            | .3         | .4         | .5          | .4          | .1          | .1          | .3          | .4          | .4           | .3           | .1           |
| 12     | *                | .0            | .0         | .2         | .6          | .0          | .0          | .1          | .2          | .1          | .0           | .1           | .1           |
| 13     | *                | .0            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .2          | .1           | .0           | .0           |
| 14     | *                | .1            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .0           |
| 15     | *                | .0            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .0           |
| 16     | *                | .1            | .4         | .6         | .4          | .3          | .1          | .1          | .4          | .4          | .6           | .6           | .1           |
| 17     | *                | .0            | .2         | .2         | .1          | .1          | .0          | .0          | .1          | .1          | .3           | .3           | .0           |
| 18     | *                | .0            | .4         | .5         | .4          | .1          | .0          | .1          | .3          | .1          | .1           | .4           | .1           |

JOB: GristMillMain2030BuildPM

RUN: GristMillMain2030BuildPM

DATE : 4/15/11  
 TIME : 13:56:50

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S      VD = .0 CM/S      Z0 = 175. CM  
 U = 1.0 M/S      CLAS = 4 (D)      ATIM = 60. MINUTES      MIXH = 1000. M      AMB = 4.3 PPM

LINK VARIABLES

| LINK DESCRIPTION     | *<br>*<br>* | X1    | LINK COORDINATES (FT) |        | *<br>*<br>* | LENGTH<br>(FT) | BRG TYPE<br>(DEG) | VPH   | EF<br>(G/MI) | H<br>(FT) | W<br>(FT) | V/C  | QUEUE<br>(VEH) |
|----------------------|-------------|-------|-----------------------|--------|-------------|----------------|-------------------|-------|--------------|-----------|-----------|------|----------------|
|                      |             |       | Y1                    | X2     | Y2          |                |                   |       |              |           |           |      |                |
| 1. Grist Mill EB in  | *           | .0    | 412.0                 | 200.0  | 412.0       | 200.           | 90. AG            | 1642. | 8.3          | .0        | 36.0      |      |                |
| 2. Grist Mill EB L   | *           | 200.0 | 424.0                 | 3420.7 | 424.0       | 3221.          | 90. AG            | 196.  | 100.0        | .0        | 12.0      | 1.22 | 163.6          |
| 3. Grist Mill EB LT  | *           | 200.0 | 412.0                 | 200.6  | 412.0       | 1.             | 90. AG            | 196.  | 100.0        | .0        | 12.0      | .05  | .0             |
| 4. Grist Mill EB R   | *           | 200.0 | 400.0                 | 235.4  | 400.0       | 35.            | 90. AG            | 134.  | 100.0        | .0        | 12.0      | .21  | 1.8            |
| 5. Grist Mill EB out | *           | 466.0 | 418.0                 | 848.0  | 418.0       | 382.           | 90. AG            | 1642. | 8.3          | .0        | 24.0      |      |                |
| 6. Grist Mill WB in  | *           | 848.0 | 442.0                 | 648.0  | 442.0       | 200.           | 270. AG           | 32.   | 8.3          | .0        | 24.0      |      |                |
| 7. Grist Mill WB LT  | *           | 648.0 | 436.0                 | 507.3  | 436.0       | 141.           | 270. AG           | 316.  | 100.0        | .0        | 12.0      | 1.83 | 7.1            |
| 8. Grist Mill WB TR  | *           | 648.0 | 448.0                 | 641.9  | 448.0       | 6.             | 270. AG           | 316.  | 100.0        | .0        | 12.0      | .53  | .3             |
| 9. Grist Mill WB out | *           | 406.0 | 442.0                 | .0     | 442.0       | 406.           | 270. AG           | 32.   | 8.3          | .0        | 24.0      |      |                |
| 10. Main NB in       | *           | 444.0 | .0                    | 444.0  | 200.0       | 200.           | 360. AG           | 1041. | 8.3          | .0        | 24.0      |      |                |
| 11. Main NB L        | *           | 438.0 | 200.0                 | 438.0  | 1058.4      | 858.           | 360. AG           | 182.  | 100.0        | .0        | 12.0      | 1.27 | 43.6           |
| 12. Main NB TR       | *           | 450.0 | 200.0                 | 450.0  | 466.7       | 267.           | 360. AG           | 175.  | 100.0        | .0        | 12.0      | .96  | 13.5           |
| 13. Main NB out      | *           | 454.0 | 454.0                 | 454.0  | 836.0       | 382.           | 360. AG           | 1041. | 8.3          | .0        | 24.0      |      |                |
| 14. Main SB in       | *           | 424.0 | 836.0                 | 424.0  | 636.0       | 200.           | 180. AG           | 1798. | 8.3          | .0        | 36.0      |      |                |
| 15. Main SB L        | *           | 436.0 | 636.0                 | 436.0  | 633.7       | 2.             | 180. AG           | 237.  | 100.0        | .0        | 12.0      | .02  | .1             |
| 16. Main SB T        | *           | 424.0 | 636.0                 | 424.0  | 65.0        | 571.           | 180. AG           | 237.  | 100.0        | .0        | 12.0      | 1.08 | 29.0           |
| 17. Main SB R        | *           | 412.0 | 636.0                 | 412.0  | -1441.3     | 2077.          | 180. AG           | 89.   | 100.0        | .0        | 12.0      | 1.15 | 105.5          |
| 18. Main SB out      | *           | 420.0 | 396.0                 | 420.0  | .0          | 396.           | 180. AG           | 1798. | 8.3          | .0        | 24.0      |      |                |

DATE : 4/15/11  
 TIME : 13:56:50

-----  
 ADDITIONAL QUEUE LINK PARAMETERS  
 -----

| LINK DESCRIPTION    | *<br>* | CYCLE<br>LENGTH<br>(SEC) | RED<br>TIME<br>(SEC) | CLEARANCE<br>LOST TIME<br>(SEC) | APPROACH<br>VOL<br>(VPH) | SATURATION<br>FLOW RATE<br>(VPH) | IDLE<br>EM FAC<br>(gm/hr) | SIGNAL<br>TYPE | ARRIVAL<br>RATE |
|---------------------|--------|--------------------------|----------------------|---------------------------------|--------------------------|----------------------------------|---------------------------|----------------|-----------------|
| 2. Grist Mill EB L  | *      | 100                      | 57                   | 6.0                             | 1476                     | 3465                             | 127.94                    | 3              | 4               |
| 3. Grist Mill EB LT | *      | 100                      | 57                   | 6.0                             | 2                        | 120                              | 127.94                    | 3              | 4               |
| 4. Grist Mill EB R  | *      | 100                      | 39                   | 6.0                             | 166                      | 1492                             | 127.94                    | 3              | 4               |
| 7. Grist Mill WB LT | *      | 100                      | 92                   | 5.0                             | 22                       | 1232                             | 127.94                    | 3              | 3               |
| 8. Grist Mill WB TR | *      | 100                      | 92                   | 5.0                             | 10                       | 1939                             | 127.94                    | 3              | 3               |
| 11. Main NB L       | *      | 100                      | 53                   | 4.0                             | 326                      | 629                              | 127.94                    | 3              | 4               |
| 12. Main NB TR      | *      | 100                      | 51                   | 6.0                             | 715                      | 1814                             | 127.94                    | 3              | 4               |
| 15. Main SB L       | *      | 100                      | 69                   | 6.0                             | 6                        | 1592                             | 127.94                    | 3              | 4               |
| 16. Main SB T       | *      | 100                      | 69                   | 6.0                             | 446                      | 1801                             | 127.94                    | 3              | 4               |
| 17. Main SB R       | *      | 100                      | 26                   | 6.0                             | 1346                     | 1775                             | 127.94                    | 3              | 4               |

-----  
 RECEPTOR LOCATIONS  
 -----

| RECEPTOR          | *<br>* | COORDINATES (FT) |       |     | *<br>* |
|-------------------|--------|------------------|-------|-----|--------|
|                   |        | X                | Y     | Z   |        |
| 1. EB W Midblock  | *      | 196.0            | 384.0 | 6.0 | *      |
| 2. SW corner      | *      | 394.0            | 384.0 | 6.0 | *      |
| 3. SB S Midblock  | *      | 394.0            | 200.0 | 6.0 | *      |
| 4. NB S Midblock  | *      | 466.0            | 200.0 | 6.0 | *      |
| 5. SE corner      | *      | 466.0            | 390.0 | 6.0 | *      |
| 6. EB E Midblock  | *      | 648.0            | 390.0 | 6.0 | *      |
| 7. WB E Midblock  | *      | 648.0            | 464.0 | 6.0 | *      |
| 8. NE corner      | *      | 476.0            | 464.0 | 6.0 | *      |
| 9. NB N Midblock  | *      | 476.0            | 640.0 | 6.0 | *      |
| 10. SB N Midblock | *      | 396.0            | 640.0 | 6.0 | *      |
| 11. NW corner     | *      | 396.0            | 464.0 | 6.0 | *      |
| 12. WB W Midblock | *      | 196.0            | 464.0 | 6.0 | *      |

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

| WIND ANGLE (DEGR) | REC1 | REC2 | REC3 | REC4 | REC5 | REC6 | REC7 | REC8 | REC9 | REC10 | REC11 | REC12 |
|-------------------|------|------|------|------|------|------|------|------|------|-------|-------|-------|
| 0.                | 4.8  | 5.5  | 5.6  | 5.7  | 5.8  | 5.2  | 4.3  | 4.9  | 4.8  | 4.8   | 5.1   | 4.3   |
| 10.               | 4.9  | 5.9  | 6.3  | 5.1  | 5.2  | 5.0  | 4.3  | 4.5  | 4.5  | 5.2   | 5.5   | 4.3   |
| 20.               | 4.9  | 5.9  | 6.6  | 4.7  | 5.0  | 5.0  | 4.3  | 4.3  | 4.3  | 5.4   | 5.8   | 4.4   |
| 30.               | 5.2  | 6.0  | 6.6  | 4.6  | 5.1  | 5.1  | 4.3  | 4.3  | 4.3  | 5.4   | 5.8   | 4.5   |
| 40.               | 5.2  | 6.1  | 6.5  | 4.6  | 5.3  | 5.1  | 4.3  | 4.3  | 4.3  | 5.3   | 5.6   | 4.5   |
| 50.               | 5.3  | 6.2  | 6.2  | 4.5  | 5.5  | 5.1  | 4.3  | 4.3  | 4.3  | 5.2   | 5.6   | 4.7   |
| 60.               | 5.2  | 6.5  | 6.1  | 4.5  | 5.5  | 5.1  | 4.3  | 4.3  | 4.3  | 5.1   | 5.4   | 4.6   |
| 70.               | 5.3  | 6.5  | 5.9  | 4.5  | 5.7  | 5.2  | 4.3  | 4.3  | 4.3  | 5.1   | 5.3   | 4.6   |
| 80.               | 5.4  | 6.7  | 5.8  | 4.4  | 5.5  | 5.1  | 4.5  | 4.6  | 4.3  | 5.1   | 5.9   | 4.7   |
| 90.               | 5.5  | 6.5  | 5.7  | 4.4  | 5.1  | 4.9  | 4.8  | 5.1  | 4.4  | 5.3   | 6.3   | 5.2   |
| 100.              | 4.9  | 6.1  | 5.6  | 4.3  | 4.6  | 4.6  | 5.0  | 5.6  | 4.4  | 5.3   | 6.7   | 5.3   |
| 110.              | 4.7  | 5.8  | 5.4  | 4.3  | 4.3  | 4.3  | 5.0  | 5.7  | 4.5  | 5.4   | 6.4   | 5.3   |
| 120.              | 4.8  | 5.9  | 5.6  | 4.3  | 4.3  | 4.3  | 5.0  | 5.5  | 4.5  | 5.7   | 6.2   | 5.2   |
| 130.              | 4.6  | 5.9  | 5.6  | 4.3  | 4.3  | 4.3  | 5.0  | 5.4  | 4.5  | 5.7   | 6.1   | 5.2   |
| 140.              | 4.6  | 6.2  | 5.8  | 4.3  | 4.3  | 4.3  | 4.9  | 5.1  | 4.6  | 5.9   | 6.1   | 5.0   |
| 150.              | 4.6  | 6.2  | 5.8  | 4.3  | 4.3  | 4.3  | 5.0  | 5.0  | 4.6  | 6.1   | 6.2   | 5.0   |
| 160.              | 4.4  | 6.2  | 5.6  | 4.3  | 4.4  | 4.3  | 5.1  | 4.8  | 4.6  | 6.2   | 6.4   | 4.7   |
| 170.              | 4.4  | 6.1  | 5.5  | 4.4  | 4.8  | 4.3  | 5.3  | 5.1  | 5.0  | 6.0   | 6.3   | 4.8   |
| 180.              | 4.3  | 5.3  | 5.0  | 4.8  | 5.5  | 4.3  | 5.5  | 5.6  | 5.4  | 5.5   | 5.8   | 4.7   |
| 190.              | 4.3  | 4.6  | 4.5  | 5.2  | 6.1  | 4.4  | 5.7  | 6.1  | 5.8  | 5.0   | 5.2   | 4.6   |
| 200.              | 4.3  | 4.3  | 4.3  | 5.4  | 6.2  | 4.4  | 5.8  | 6.5  | 5.9  | 4.4   | 4.6   | 4.6   |
| 210.              | 4.3  | 4.3  | 4.3  | 5.5  | 6.3  | 4.6  | 6.0  | 6.1  | 5.6  | 4.4   | 4.6   | 4.6   |
| 220.              | 4.3  | 4.3  | 4.3  | 5.4  | 6.1  | 4.6  | 6.2  | 5.9  | 5.5  | 4.4   | 4.6   | 4.6   |
| 230.              | 4.3  | 4.3  | 4.3  | 5.4  | 6.0  | 4.8  | 6.3  | 6.0  | 5.4  | 4.4   | 4.7   | 4.6   |
| 240.              | 4.3  | 4.3  | 4.3  | 5.3  | 6.0  | 4.7  | 6.1  | 5.9  | 5.4  | 4.4   | 4.7   | 4.6   |
| 250.              | 4.3  | 4.3  | 4.3  | 5.3  | 5.9  | 4.7  | 5.9  | 5.8  | 5.3  | 4.3   | 4.7   | 4.6   |
| 260.              | 4.4  | 4.4  | 4.3  | 5.5  | 5.9  | 4.9  | 5.7  | 5.9  | 5.2  | 4.3   | 4.6   | 4.5   |
| 270.              | 4.6  | 4.5  | 4.3  | 5.6  | 6.1  | 5.3  | 5.1  | 5.7  | 5.1  | 4.3   | 4.5   | 4.4   |
| 280.              | 4.7  | 4.6  | 4.3  | 5.7  | 6.1  | 5.5  | 4.8  | 5.4  | 5.1  | 4.3   | 4.3   | 4.3   |
| 290.              | 4.8  | 4.7  | 4.3  | 5.8  | 6.1  | 5.9  | 4.6  | 5.4  | 5.1  | 4.3   | 4.3   | 4.3   |
| 300.              | 4.8  | 4.7  | 4.4  | 6.0  | 6.1  | 5.9  | 4.6  | 5.3  | 5.2  | 4.3   | 4.3   | 4.3   |
| 310.              | 4.8  | 4.7  | 4.4  | 6.1  | 6.1  | 5.9  | 4.7  | 5.3  | 5.2  | 4.3   | 4.3   | 4.3   |
| 320.              | 4.7  | 4.6  | 4.4  | 6.2  | 6.1  | 6.0  | 4.6  | 5.4  | 5.2  | 4.3   | 4.3   | 4.3   |
| 330.              | 4.7  | 4.6  | 4.4  | 6.4  | 6.3  | 5.9  | 4.5  | 5.5  | 5.3  | 4.3   | 4.3   | 4.3   |
| 340.              | 4.7  | 4.6  | 4.4  | 6.4  | 6.3  | 5.4  | 4.4  | 5.6  | 5.3  | 4.3   | 4.3   | 4.3   |
| 350.              | 4.7  | 4.9  | 4.9  | 6.3  | 6.3  | 5.3  | 4.3  | 5.3  | 5.1  | 4.5   | 4.7   | 4.3   |
| 360.              | 4.8  | 5.5  | 5.6  | 5.7  | 5.8  | 5.2  | 4.3  | 4.9  | 4.8  | 4.8   | 5.1   | 4.3   |
| MAX               | 5.5  | 6.7  | 6.6  | 6.4  | 6.3  | 6.0  | 6.3  | 6.5  | 5.9  | 6.2   | 6.7   | 5.3   |
| DEGR.             | 90   | 80   | 20   | 330  | 210  | 320  | 230  | 200  | 200  | 160   | 100   | 100   |

THE HIGHEST CONCENTRATION OF 6.70 PPM OCCURRED AT RECEPTOR REC11.

DATE : 4/15/11  
 TIME : 13:56:50

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING  
 THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

| LINK # | *<br>*<br>*<br>* | CO/LINK (PPM) |            |            |             |             |             |             |             |             |              |              |              |    |    |    |    |    |
|--------|------------------|---------------|------------|------------|-------------|-------------|-------------|-------------|-------------|-------------|--------------|--------------|--------------|----|----|----|----|----|
|        |                  | REC1<br>90    | REC2<br>80 | REC3<br>20 | REC4<br>330 | REC5<br>210 | REC6<br>320 | REC7<br>230 | REC8<br>200 | REC9<br>200 | REC10<br>160 | REC11<br>100 | REC12<br>100 |    |    |    |    |    |
| 1      | *                | .0            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .0           |    |    |    |    |    |
| 2      | *                | .4            | .5         | .1         | .1          | .0          | .4          | .4          | .3          | .1          | .1           | .5           | .5           |    |    |    |    |    |
| 3      | *                | .0            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .0           |    |    |    |    |    |
| 4      | *                | .1            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .0           |    |    |    |    |    |
| 5      | *                | .1            | .3         | .1         | .0          | .0          | .4          | .3          | .1          | .0          | .1           | .3           | .1           |    |    |    |    |    |
| 6      | *                | .0            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .0           |    |    |    |    |    |
| 7      | *                | .1            | .2         | .1         | .0          | .0          | .5          | .7          | .0          | .0          | .0           | .3           | .1           |    |    |    |    |    |
| 8      | *                | .0            | .0         | .0         | .0          | .0          | .0          | .1          | .0          | .0          | .0           | .0           | .0           |    |    |    |    |    |
| 9      | *                | .0            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .0           |    |    |    |    |    |
| 10     | *                | .0            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .0           |    |    |    |    |    |
| 11     | *                | .1            | .3         | .4         | .5          | .4          | .1          | .1          | .4          | .4          | .4           | .3           | .1           |    |    |    |    |    |
| 12     | *                | .1            | .2         | .2         | .6          | .6          | .0          | .1          | .5          | .1          | .1           | .2           | .1           |    |    |    |    |    |
| 13     | *                | .0            | .0         | .0         | .0          | .0          | .1          | .0          | .0          | .3          | .1           | .1           | .0           |    |    |    |    |    |
| 14     | *                | .0            | .0         | .0         | .0          | .0          | .1          | .0          | .0          | .0          | .0           | .0           | .0           |    |    |    |    |    |
| 15     | *                | .0            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .0           |    |    |    |    |    |
| 16     | *                | .1            | .4         | .6         | .5          | .5          | .1          | .1          | .4          | .4          | .6           | .5           | .1           |    |    |    |    |    |
| 17     | *                | .1            | .2         | .3         | .1          | .2          | .0          | .1          | .2          | .2          | .4           | .2           | .0           |    |    |    |    |    |
| 18     | *                | .1            | .1         | .3         | .3          | .5          | .3          | .3          | .3          | .3          | .0           | .2           | .1           | .3 | .1 | .1 | .0 | .0 |

JOB: GristMillMain2030MitigatedBuildAM

RUN: GristMillMain2030MitigatedBuildAM

DATE : 4/15/11  
 TIME : 13:58:44

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S      VD = .0 CM/S      Z0 = 175. CM  
 U = 1.0 M/S      CLAS = 4 (D)      ATIM = 60. MINUTES      MIXH = 1000. M      AMB = 4.3 PPM

LINK VARIABLES

| LINK DESCRIPTION     | *<br>* X1 | LINK COORDINATES (FT)<br>Y1 | X2     | Y2     | *<br>* LENGTH (FT) | BRG TYPE (DEG) | VPH   | EF (G/MI) | H (FT) | W (FT) | V/C  | QUEUE (VEH) |
|----------------------|-----------|-----------------------------|--------|--------|--------------------|----------------|-------|-----------|--------|--------|------|-------------|
| 1. Grist Mill EB in  | * .0      | 412.0                       | 200.0  | 412.0  | * 200.             | 90. AG         | 2164. | 8.3       | .0     | 36.0   |      |             |
| 2. Grist Mill EB L   | * 200.0   | 424.0                       | 3595.4 | 424.0  | * 3395.            | 90. AG         | 187.  | 100.0     | .0     | 12.0   | 1.21 | 172.5       |
| 3. Grist Mill EB LT  | * 200.0   | 412.0                       | 260.0  | 412.0  | * 60.              | 90. AG         | 187.  | 100.0     | .0     | 12.0   | .89  | 3.1         |
| 4. Grist Mill EB R   | * 200.0   | 400.0                       | 317.8  | 400.0  | * 118.             | 90. AG         | 150.  | 100.0     | .0     | 12.0   | .63  | 6.0         |
| 5. Grist Mill EB out | * 466.0   | 418.0                       | 848.0  | 418.0  | * 382.             | 90. AG         | 2164. | 8.3       | .0     | 24.0   |      |             |
| 6. Grist Mill WB in  | * 848.0   | 442.0                       | 648.0  | 442.0  | * 200.             | 270. AG        | 148.  | 8.3       | .0     | 24.0   |      |             |
| 7. Grist Mill WB LT  | * 648.0   | 436.0                       | -310.6 | 436.0  | * 959.             | 270. AG        | 312.  | 100.0     | .0     | 12.0   | 4.12 | 48.7        |
| 8. Grist Mill WB TR  | * 648.0   | 448.0                       | 623.6  | 448.0  | * 24.              | 270. AG        | 312.  | 100.0     | .0     | 12.0   | .59  | 1.2         |
| 9. Grist Mill WB out | * 406.0   | 442.0                       | .0     | 442.0  | * 406.             | 270. AG        | 148.  | 8.3       | .0     | 24.0   |      |             |
| 10. Main NB in       | * 444.0   | .0                          | 444.0  | 200.0  | * 200.             | 360. AG        | 623.  | 8.3       | .0     | 24.0   |      |             |
| 11. Main NB L        | * 438.0   | 200.0                       | 438.0  | 755.8  | * 556.             | 360. AG        | 197.  | 100.0     | .0     | 12.0   | 1.29 | 28.2        |
| 12. Main NB TR       | * 450.0   | 200.0                       | 450.0  | 343.4  | * 143.             | 360. AG        | 190.  | 100.0     | .0     | 12.0   | .67  | 7.3         |
| 13. Main NB out      | * 454.0   | 454.0                       | 454.0  | 836.0  | * 382.             | 360. AG        | 623.  | 8.3       | .0     | 24.0   |      |             |
| 14. Main SB in       | * 424.0   | 836.0                       | 424.0  | 636.0  | * 200.             | 180. AG        | 2066. | 8.3       | .0     | 36.0   |      |             |
| 15. Main SB L        | * 436.0   | 636.0                       | 436.0  | 623.6  | * 12.              | 180. AG        | 222.  | 100.0     | .0     | 12.0   | .07  | .6          |
| 16. Main SB T        | * 424.0   | 636.0                       | 424.0  | -869.0 | * 1505.            | 180. AG        | 222.  | 100.0     | .0     | 12.0   | 1.20 | 76.5        |
| 17. Main SB R        | * 412.0   | 636.0                       | 412.0  | -916.4 | * 1552.            | 180. AG        | 69.   | 100.0     | .0     | 12.0   | 1.10 | 78.9        |
| 18. Main SB out      | * 420.0   | 396.0                       | 420.0  | .0     | * 396.             | 180. AG        | 2066. | 8.3       | .0     | 24.0   |      |             |

DATE : 4/15/11  
 TIME : 13:58:44

-----  
 ADDITIONAL QUEUE LINK PARAMETERS  
 -----

| LINK DESCRIPTION    | *<br>* | CYCLE<br>LENGTH<br>(SEC) | RED<br>TIME<br>(SEC) | CLEARANCE<br>LOST TIME<br>(SEC) | APPROACH<br>VOL<br>(VPH) | SATURATION<br>FLOW RATE<br>(VPH) | IDLE<br>EM FAC<br>(gm/hr) | SIGNAL<br>TYPE | ARRIVAL<br>RATE |
|---------------------|--------|--------------------------|----------------------|---------------------------------|--------------------------|----------------------------------|---------------------------|----------------|-----------------|
| 2. Grist Mill EB L  | *      | 110                      | 60                   | 6.0                             | 1595                     | 3459                             | 127.94                    | 3              | 4               |
| 3. Grist Mill EB LT | *      | 110                      | 60                   | 6.0                             | 120                      | 354                              | 127.94                    | 3              | 4               |
| 4. Grist Mill EB R  | *      | 110                      | 48                   | 6.0                             | 449                      | 1463                             | 127.94                    | 3              | 4               |
| 7. Grist Mill WB LT | *      | 110                      | 100                  | 5.0                             | 107                      | 960                              | 127.94                    | 3              | 3               |
| 8. Grist Mill WB TR | *      | 110                      | 100                  | 5.0                             | 41                       | 2558                             | 127.94                    | 3              | 3               |
| 11. Main NB L       | *      | 110                      | 63                   | 4.0                             | 193                      | 405                              | 127.94                    | 3              | 4               |
| 12. Main NB TR      | *      | 110                      | 61                   | 6.0                             | 430                      | 1718                             | 127.94                    | 3              | 4               |
| 15. Main SB L       | *      | 110                      | 71                   | 6.0                             | 32                       | 1563                             | 127.94                    | 3              | 4               |
| 16. Main SB T       | *      | 110                      | 71                   | 6.0                             | 696                      | 2068                             | 127.94                    | 3              | 4               |
| 17. Main SB R       | *      | 110                      | 22                   | 6.0                             | 1338                     | 1668                             | 127.94                    | 3              | 4               |

-----  
 RECEPTOR LOCATIONS  
 -----

| RECEPTOR          | *<br>* | COORDINATES (FT) |       |     | *<br>* |
|-------------------|--------|------------------|-------|-----|--------|
|                   |        | X                | Y     | Z   |        |
| 1. EB W Midblock  | *      | 196.0            | 384.0 | 6.0 | *      |
| 2. SW corner      | *      | 394.0            | 384.0 | 6.0 | *      |
| 3. SB S Midblock  | *      | 394.0            | 200.0 | 6.0 | *      |
| 4. NB S Midblock  | *      | 466.0            | 200.0 | 6.0 | *      |
| 5. SE corner      | *      | 466.0            | 390.0 | 6.0 | *      |
| 6. EB E Midblock  | *      | 648.0            | 390.0 | 6.0 | *      |
| 7. WB E Midblock  | *      | 648.0            | 464.0 | 6.0 | *      |
| 8. NE corner      | *      | 476.0            | 464.0 | 6.0 | *      |
| 9. NB N Midblock  | *      | 476.0            | 640.0 | 6.0 | *      |
| 10. SB N Midblock | *      | 396.0            | 640.0 | 6.0 | *      |
| 11. NW corner     | *      | 396.0            | 464.0 | 6.0 | *      |
| 12. WB W Midblock | *      | 196.0            | 464.0 | 6.0 | *      |

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

| WIND ANGLE (DEGR) | REC1 | REC2 | REC3 | REC4 | REC5 | REC6 | REC7 | REC8 | REC9 | REC10 | REC11 | REC12 |
|-------------------|------|------|------|------|------|------|------|------|------|-------|-------|-------|
| 0.                | 5.3  | 5.7  | 5.7  | 5.9  | 5.8  | 5.4  | 4.3  | 4.8  | 4.6  | 4.6   | 4.9   | 4.3   |
| 10.               | 5.5  | 6.1  | 6.2  | 5.2  | 5.5  | 5.3  | 4.3  | 4.5  | 4.3  | 4.9   | 5.5   | 4.3   |
| 20.               | 5.5  | 6.3  | 6.7  | 4.7  | 5.5  | 5.1  | 4.3  | 4.3  | 4.3  | 5.2   | 5.6   | 4.3   |
| 30.               | 5.9  | 6.2  | 6.6  | 4.6  | 5.5  | 5.1  | 4.3  | 4.3  | 4.3  | 5.3   | 5.5   | 4.4   |
| 40.               | 6.2  | 6.2  | 6.4  | 4.6  | 5.7  | 5.2  | 4.3  | 4.3  | 4.3  | 5.3   | 5.5   | 4.5   |
| 50.               | 6.1  | 6.2  | 6.3  | 4.5  | 5.7  | 5.2  | 4.3  | 4.3  | 4.3  | 5.2   | 5.4   | 4.6   |
| 60.               | 6.2  | 6.5  | 6.1  | 4.5  | 5.8  | 5.3  | 4.3  | 4.3  | 4.3  | 5.2   | 5.3   | 4.5   |
| 70.               | 6.2  | 6.6  | 6.1  | 4.4  | 5.8  | 5.3  | 4.3  | 4.3  | 4.3  | 5.2   | 5.3   | 4.6   |
| 80.               | 6.0  | 6.8  | 5.8  | 4.4  | 5.6  | 5.2  | 4.5  | 4.7  | 4.3  | 5.3   | 5.8   | 5.0   |
| 90.               | 5.6  | 6.4  | 5.6  | 4.4  | 5.2  | 5.0  | 4.8  | 5.2  | 4.4  | 5.3   | 6.3   | 5.5   |
| 100.              | 5.1  | 5.9  | 5.6  | 4.3  | 4.7  | 4.6  | 5.0  | 5.6  | 4.4  | 5.4   | 6.6   | 5.9   |
| 110.              | 4.7  | 5.7  | 5.5  | 4.3  | 4.3  | 4.3  | 5.0  | 5.8  | 4.5  | 5.5   | 6.7   | 6.0   |
| 120.              | 4.7  | 5.8  | 5.5  | 4.3  | 4.3  | 4.3  | 5.1  | 5.8  | 4.5  | 5.7   | 6.6   | 6.1   |
| 130.              | 4.5  | 5.9  | 5.5  | 4.3  | 4.3  | 4.3  | 5.0  | 5.7  | 4.5  | 5.6   | 6.4   | 6.1   |
| 140.              | 4.5  | 6.0  | 5.6  | 4.3  | 4.3  | 4.3  | 5.0  | 5.7  | 4.6  | 5.9   | 6.6   | 5.9   |
| 150.              | 4.6  | 6.1  | 5.7  | 4.3  | 4.3  | 4.3  | 4.9  | 5.5  | 4.6  | 6.0   | 6.7   | 5.9   |
| 160.              | 4.4  | 6.3  | 5.9  | 4.3  | 4.4  | 4.3  | 5.1  | 5.5  | 4.7  | 6.2   | 6.8   | 5.6   |
| 170.              | 4.4  | 6.1  | 5.8  | 4.4  | 4.8  | 4.3  | 5.4  | 5.9  | 4.9  | 6.1   | 6.9   | 5.6   |
| 180.              | 4.3  | 5.5  | 5.3  | 4.9  | 5.5  | 4.3  | 5.6  | 6.4  | 5.6  | 5.6   | 6.4   | 5.4   |
| 190.              | 4.3  | 4.8  | 4.7  | 5.3  | 6.0  | 4.4  | 6.0  | 6.7  | 5.9  | 5.1   | 5.7   | 5.2   |
| 200.              | 4.3  | 4.4  | 4.3  | 5.4  | 6.0  | 4.4  | 6.3  | 6.6  | 5.8  | 4.7   | 5.4   | 5.2   |
| 210.              | 4.3  | 4.3  | 4.3  | 5.4  | 5.9  | 4.6  | 6.6  | 6.5  | 5.7  | 4.6   | 5.2   | 5.3   |
| 220.              | 4.3  | 4.3  | 4.3  | 5.4  | 5.7  | 4.5  | 6.8  | 6.4  | 5.7  | 4.7   | 5.3   | 5.4   |
| 230.              | 4.3  | 4.3  | 4.3  | 5.3  | 5.5  | 4.7  | 6.7  | 6.1  | 5.6  | 4.6   | 5.4   | 5.4   |
| 240.              | 4.3  | 4.3  | 4.3  | 5.2  | 5.5  | 4.7  | 6.8  | 6.3  | 5.6  | 4.6   | 5.5   | 5.5   |
| 250.              | 4.3  | 4.3  | 4.3  | 5.2  | 5.4  | 4.7  | 6.5  | 6.6  | 5.4  | 4.5   | 5.9   | 5.5   |
| 260.              | 4.5  | 4.6  | 4.3  | 5.4  | 5.9  | 5.0  | 6.1  | 6.5  | 5.3  | 4.4   | 5.6   | 5.3   |
| 270.              | 4.9  | 5.1  | 4.3  | 5.5  | 6.1  | 5.6  | 5.5  | 6.0  | 5.1  | 4.3   | 5.1   | 4.9   |
| 280.              | 5.4  | 5.4  | 4.4  | 5.7  | 6.3  | 5.9  | 4.9  | 5.5  | 5.2  | 4.3   | 4.6   | 4.5   |
| 290.              | 5.5  | 5.5  | 4.4  | 5.9  | 6.2  | 6.0  | 4.6  | 5.2  | 5.0  | 4.3   | 4.4   | 4.4   |
| 300.              | 5.5  | 5.2  | 4.6  | 6.3  | 6.2  | 6.1  | 4.5  | 5.2  | 5.1  | 4.3   | 4.3   | 4.3   |
| 310.              | 5.4  | 5.1  | 4.6  | 6.4  | 6.1  | 5.9  | 4.6  | 5.2  | 5.2  | 4.3   | 4.3   | 4.3   |
| 320.              | 5.4  | 5.1  | 4.8  | 6.6  | 6.2  | 6.1  | 4.5  | 5.3  | 5.2  | 4.3   | 4.3   | 4.3   |
| 330.              | 5.2  | 5.0  | 4.7  | 6.6  | 6.1  | 5.9  | 4.4  | 5.4  | 5.2  | 4.3   | 4.3   | 4.3   |
| 340.              | 5.2  | 5.0  | 4.6  | 6.5  | 6.3  | 5.7  | 4.3  | 5.3  | 5.0  | 4.3   | 4.3   | 4.3   |
| 350.              | 5.2  | 5.4  | 5.0  | 6.3  | 6.2  | 5.6  | 4.3  | 5.1  | 4.8  | 4.4   | 4.7   | 4.3   |
| 360.              | 5.3  | 5.7  | 5.7  | 5.9  | 5.8  | 5.4  | 4.3  | 4.8  | 4.6  | 4.6   | 4.9   | 4.3   |
| MAX DEGR.         | 6.2  | 6.8  | 6.7  | 6.6  | 6.3  | 6.1  | 6.8  | 6.7  | 5.9  | 6.2   | 6.9   | 6.1   |
|                   | 40   | 80   | 20   | 320  | 280  | 300  | 220  | 190  | 190  | 160   | 170   | 120   |

THE HIGHEST CONCENTRATION OF 6.90 PPM OCCURRED AT RECEPTOR REC11.



DATE : 4/15/11  
 TIME : 13:58:44

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING  
 THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

| LINK # | *<br>*<br>*<br>* | CO/LINK (PPM) |            |            |             |             |             |             |             |             |              |              |              |
|--------|------------------|---------------|------------|------------|-------------|-------------|-------------|-------------|-------------|-------------|--------------|--------------|--------------|
|        |                  | REC1<br>40    | REC2<br>80 | REC3<br>20 | REC4<br>320 | REC5<br>280 | REC6<br>300 | REC7<br>220 | REC8<br>190 | REC9<br>190 | REC10<br>160 | REC11<br>170 | REC12<br>120 |
| 1      | *                | .0            | .0         | .0         | .0          | .1          | .0          | .0          | .0          | .0          | .0           | .0           | .0           |
| 2      | *                | .3            | .5         | .1         | .1          | .3          | .4          | .3          | .3          | .1          | .1           | .3           | .4           |
| 3      | *                | .4            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .1           |
| 4      | *                | .4            | .0         | .0         | .0          | .1          | .0          | .0          | .0          | .0          | .0           | .0           | .1           |
| 5      | *                | .0            | .4         | .1         | .0          | .0          | .6          | .4          | .2          | .0          | .1           | .0           | .0           |
| 6      | *                | .0            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .0           |
| 7      | *                | .5            | .3         | .2         | .2          | .6          | .6          | .7          | .6          | .2          | .2           | .6           | .8           |
| 8      | *                | .0            | .0         | .0         | .0          | .0          | .0          | .7          | .0          | .0          | .0           | .0           | .0           |
| 9      | *                | .0            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .0           |
| 10     | *                | .0            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .0           |
| 11     | *                | .1            | .3         | .4         | .5          | .4          | .1          | .1          | .3          | .4          | .4           | .3           | .1           |
| 12     | *                | .0            | .0         | .2         | .6          | .0          | .0          | .1          | .2          | .1          | .0           | .1           | .1           |
| 13     | *                | .0            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .2          | .1           | .0           | .0           |
| 14     | *                | .1            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .0           |
| 15     | *                | .0            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .0           |
| 16     | *                | .1            | .4         | .6         | .4          | .3          | .1          | .1          | .4          | .4          | .6           | .6           | .1           |
| 17     | *                | .0            | .2         | .2         | .1          | .1          | .0          | .0          | .1          | .1          | .3           | .3           | .0           |
| 18     | *                | .0            | .4         | .6         | .4          | .1          | .0          | .1          | .3          | .1          | .1           | .4           | .1           |

JOB: GristMillMain2030MitigatedBuildPM

RUN: GristMillMain2030MitigatedBuildPM

DATE : 4/18/11  
 TIME : 8:47:54

The MODE flag has been set to C for calculating CO averages.

SITE & METEOROLOGICAL VARIABLES

VS = .0 CM/S      VD = .0 CM/S      Z0 = 175. CM  
 U = 1.0 M/S      CLAS = 4 (D)      ATIM = 60. MINUTES      MIXH = 1000. M      AMB = 4.3 PPM

LINK VARIABLES

| LINK DESCRIPTION     | *<br>* | X1    | LINK COORDINATES (FT)<br>Y1 | X2     | Y2      | *<br>* | LENGTH<br>(FT) | BRG TYPE<br>(DEG) | VPH   | EF<br>(G/MI) | H<br>(FT) | W<br>(FT) | V/C  | QUEUE<br>(VEH) |
|----------------------|--------|-------|-----------------------------|--------|---------|--------|----------------|-------------------|-------|--------------|-----------|-----------|------|----------------|
| 1. Grist Mill EB in  | *      | .0    | 412.0                       | 200.0  | 412.0   | *      | 200.           | 90. AG            | 1642. | 8.3          | .0        | 36.0      |      |                |
| 2. Grist Mill EB L   | *      | 200.0 | 424.0                       | 3420.7 | 424.0   | *      | 3221.          | 90. AG            | 196.  | 100.0        | .0        | 12.0      | 1.22 | 163.6          |
| 3. Grist Mill EB LT  | *      | 200.0 | 412.0                       | 200.6  | 412.0   | *      | 1.             | 90. AG            | 196.  | 100.0        | .0        | 12.0      | .05  | .0             |
| 4. Grist Mill EB R   | *      | 200.0 | 400.0                       | 235.4  | 400.0   | *      | 35.            | 90. AG            | 134.  | 100.0        | .0        | 12.0      | .21  | 1.8            |
| 5. Grist Mill EB out | *      | 466.0 | 418.0                       | 848.0  | 418.0   | *      | 382.           | 90. AG            | 1642. | 8.3          | .0        | 24.0      |      |                |
| 6. Grist Mill WB in  | *      | 848.0 | 442.0                       | 648.0  | 442.0   | *      | 200.           | 270. AG           | 32.   | 8.3          | .0        | 24.0      |      |                |
| 7. Grist Mill WB LT  | *      | 648.0 | 436.0                       | 507.3  | 436.0   | *      | 141.           | 270. AG           | 316.  | 100.0        | .0        | 12.0      | 1.83 | 7.1            |
| 8. Grist Mill WB TR  | *      | 648.0 | 448.0                       | 641.9  | 448.0   | *      | 6.             | 270. AG           | 316.  | 100.0        | .0        | 12.0      | .53  | .3             |
| 9. Grist Mill WB out | *      | 406.0 | 442.0                       | .0     | 442.0   | *      | 406.           | 270. AG           | 32.   | 8.3          | .0        | 24.0      |      |                |
| 10. Main NB in       | *      | 444.0 | .0                          | 444.0  | 200.0   | *      | 200.           | 360. AG           | 1041. | 8.3          | .0        | 24.0      |      |                |
| 11. Main NB L        | *      | 438.0 | 200.0                       | 438.0  | 1158.6  | *      | 959.           | 360. AG           | 182.  | 100.0        | .0        | 12.0      | 1.32 | 48.7           |
| 12. Main NB TR       | *      | 450.0 | 200.0                       | 450.0  | 399.4   | *      | 199.           | 360. AG           | 175.  | 100.0        | .0        | 12.0      | .51  | 10.1           |
| 13. Main NB out      | *      | 454.0 | 454.0                       | 454.0  | 836.0   | *      | 382.           | 360. AG           | 1041. | 8.3          | .0        | 24.0      |      |                |
| 14. Main SB in       | *      | 424.0 | 836.0                       | 424.0  | 636.0   | *      | 200.           | 180. AG           | 1798. | 8.3          | .0        | 36.0      |      |                |
| 15. Main SB L        | *      | 436.0 | 636.0                       | 436.0  | 633.7   | *      | 2.             | 180. AG           | 237.  | 100.0        | .0        | 12.0      | .02  | .1             |
| 16. Main SB T        | *      | 424.0 | 636.0                       | 424.0  | 65.0    | *      | 571.           | 180. AG           | 237.  | 100.0        | .0        | 12.0      | 1.08 | 29.0           |
| 17. Main SB R        | *      | 412.0 | 636.0                       | 412.0  | -1441.3 | *      | 2077.          | 180. AG           | 89.   | 100.0        | .0        | 12.0      | 1.15 | 105.5          |
| 18. Main SB out      | *      | 420.0 | 396.0                       | 420.0  | .0      | *      | 396.           | 180. AG           | 1798. | 8.3          | .0        | 24.0      |      |                |

DATE : 4/18/11  
 TIME : 8:47:54

-----  
 ADDITIONAL QUEUE LINK PARAMETERS  
 -----

| LINK DESCRIPTION    | *<br>* | CYCLE<br>LENGTH<br>(SEC) | RED<br>TIME<br>(SEC) | CLEARANCE<br>LOST TIME<br>(SEC) | APPROACH<br>VOL<br>(VPH) | SATURATION<br>FLOW RATE<br>(VPH) | IDLE<br>EM FAC<br>(gm/hr) | SIGNAL<br>TYPE | ARRIVAL<br>RATE |
|---------------------|--------|--------------------------|----------------------|---------------------------------|--------------------------|----------------------------------|---------------------------|----------------|-----------------|
| 2. Grist Mill EB L  | *      | 100                      | 57                   | 6.0                             | 1476                     | 3465                             | 127.94                    | 3              | 4               |
| 3. Grist Mill EB LT | *      | 100                      | 57                   | 6.0                             | 2                        | 120                              | 127.94                    | 3              | 4               |
| 4. Grist Mill EB R  | *      | 100                      | 39                   | 6.0                             | 166                      | 1492                             | 127.94                    | 3              | 4               |
| 7. Grist Mill WB LT | *      | 100                      | 92                   | 5.0                             | 22                       | 1232                             | 127.94                    | 3              | 3               |
| 8. Grist Mill WB TR | *      | 100                      | 92                   | 5.0                             | 10                       | 1939                             | 127.94                    | 3              | 3               |
| 11. Main NB L       | *      | 100                      | 53                   | 4.0                             | 326                      | 603                              | 127.94                    | 3              | 4               |
| 12. Main NB TR      | *      | 100                      | 51                   | 6.0                             | 715                      | 3445                             | 127.94                    | 3              | 4               |
| 15. Main SB L       | *      | 100                      | 69                   | 6.0                             | 6                        | 1592                             | 127.94                    | 3              | 4               |
| 16. Main SB T       | *      | 100                      | 69                   | 6.0                             | 446                      | 1801                             | 127.94                    | 3              | 4               |
| 17. Main SB R       | *      | 100                      | 26                   | 6.0                             | 1346                     | 1775                             | 127.94                    | 3              | 4               |

-----  
 RECEPTOR LOCATIONS  
 -----

| RECEPTOR          | *<br>* | COORDINATES (FT) |       |     | *<br>* |
|-------------------|--------|------------------|-------|-----|--------|
|                   |        | X                | Y     | Z   |        |
| 1. EB W Midblock  | *      | 196.0            | 384.0 | 6.0 | *      |
| 2. SW Corner      | *      | 394.0            | 384.0 | 6.0 | *      |
| 3. SB S Midblock  | *      | 394.0            | 200.0 | 6.0 | *      |
| 4. NB S Midblock  | *      | 466.0            | 200.0 | 6.0 | *      |
| 5. SE Corner      | *      | 466.0            | 390.0 | 6.0 | *      |
| 6. EB E Midblock  | *      | 648.0            | 390.0 | 6.0 | *      |
| 7. WB E Midblock  | *      | 648.0            | 464.0 | 6.0 | *      |
| 8. NE Corner      | *      | 476.0            | 464.0 | 6.0 | *      |
| 9. NB N Midblock  | *      | 476.0            | 640.0 | 6.0 | *      |
| 10. SB N Midblock | *      | 396.0            | 640.0 | 6.0 | *      |
| 11. NW Corner     | *      | 396.0            | 464.0 | 6.0 | *      |
| 12. WB W Midblock | *      | 196.0            | 464.0 | 6.0 | *      |

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

| WIND ANGLE (DEGR) | REC1 | REC2 | REC3 | REC4 | REC5 | REC6 | REC7 | REC8 | REC9 | REC10 | REC11 | REC12 |
|-------------------|------|------|------|------|------|------|------|------|------|-------|-------|-------|
| 0.                | 4.8  | 5.5  | 5.6  | 5.7  | 5.7  | 5.2  | 4.3  | 5.0  | 4.8  | 4.8   | 5.1   | 4.3   |
| 10.               | 4.9  | 6.0  | 6.2  | 5.1  | 5.1  | 5.0  | 4.3  | 4.5  | 4.5  | 5.2   | 5.6   | 4.3   |
| 20.               | 4.9  | 5.9  | 6.6  | 4.7  | 5.0  | 5.0  | 4.3  | 4.3  | 4.3  | 5.4   | 5.8   | 4.4   |
| 30.               | 5.2  | 5.9  | 6.5  | 4.6  | 5.1  | 5.1  | 4.3  | 4.3  | 4.3  | 5.4   | 5.8   | 4.5   |
| 40.               | 5.2  | 5.9  | 6.5  | 4.6  | 5.3  | 5.1  | 4.3  | 4.3  | 4.3  | 5.3   | 5.6   | 4.5   |
| 50.               | 5.3  | 6.0  | 6.2  | 4.5  | 5.5  | 5.1  | 4.3  | 4.3  | 4.3  | 5.2   | 5.6   | 4.7   |
| 60.               | 5.2  | 6.3  | 6.1  | 4.5  | 5.5  | 5.1  | 4.3  | 4.3  | 4.3  | 5.1   | 5.4   | 4.6   |
| 70.               | 5.3  | 6.4  | 5.9  | 4.5  | 5.7  | 5.2  | 4.3  | 4.3  | 4.3  | 5.1   | 5.3   | 4.6   |
| 80.               | 5.3  | 6.6  | 5.8  | 4.4  | 5.5  | 5.1  | 4.5  | 4.6  | 4.3  | 5.1   | 5.8   | 4.7   |
| 90.               | 5.5  | 6.5  | 5.7  | 4.4  | 5.1  | 4.9  | 4.8  | 5.1  | 4.4  | 5.3   | 6.2   | 5.2   |
| 100.              | 4.9  | 6.1  | 5.6  | 4.3  | 4.6  | 4.6  | 5.0  | 5.6  | 4.4  | 5.3   | 6.5   | 5.2   |
| 110.              | 4.7  | 5.8  | 5.4  | 4.3  | 4.3  | 4.3  | 5.0  | 5.7  | 4.5  | 5.4   | 6.2   | 5.3   |
| 120.              | 4.8  | 5.9  | 5.6  | 4.3  | 4.3  | 4.3  | 5.0  | 5.5  | 4.5  | 5.7   | 6.0   | 5.2   |
| 130.              | 4.6  | 5.9  | 5.6  | 4.3  | 4.3  | 4.3  | 5.0  | 5.4  | 4.5  | 5.7   | 6.0   | 5.2   |
| 140.              | 4.6  | 6.2  | 5.8  | 4.3  | 4.3  | 4.3  | 4.9  | 5.1  | 4.6  | 5.9   | 5.9   | 5.0   |
| 150.              | 4.6  | 6.2  | 5.8  | 4.3  | 4.3  | 4.3  | 5.0  | 5.0  | 4.6  | 6.0   | 6.1   | 5.0   |
| 160.              | 4.4  | 6.2  | 5.6  | 4.3  | 4.4  | 4.3  | 5.1  | 4.8  | 4.6  | 6.2   | 6.4   | 4.7   |
| 170.              | 4.4  | 6.1  | 5.5  | 4.4  | 4.8  | 4.3  | 5.3  | 5.1  | 4.9  | 6.0   | 6.3   | 4.8   |
| 180.              | 4.3  | 5.3  | 5.0  | 4.8  | 5.5  | 4.3  | 5.5  | 5.6  | 5.4  | 5.5   | 5.8   | 4.7   |
| 190.              | 4.3  | 4.6  | 4.5  | 5.2  | 6.1  | 4.4  | 5.7  | 6.0  | 5.8  | 5.0   | 5.2   | 4.6   |
| 200.              | 4.3  | 4.3  | 4.3  | 5.4  | 6.2  | 4.4  | 5.8  | 6.2  | 5.8  | 4.4   | 4.6   | 4.6   |
| 210.              | 4.3  | 4.3  | 4.3  | 5.5  | 6.3  | 4.6  | 6.0  | 5.8  | 5.6  | 4.4   | 4.6   | 4.6   |
| 220.              | 4.3  | 4.3  | 4.3  | 5.4  | 6.1  | 4.6  | 6.2  | 5.6  | 5.5  | 4.4   | 4.6   | 4.6   |
| 230.              | 4.3  | 4.3  | 4.3  | 5.4  | 6.0  | 4.8  | 6.3  | 5.6  | 5.4  | 4.4   | 4.7   | 4.6   |
| 240.              | 4.3  | 4.3  | 4.3  | 5.3  | 6.0  | 4.7  | 6.1  | 5.5  | 5.4  | 4.4   | 4.7   | 4.6   |
| 250.              | 4.3  | 4.3  | 4.3  | 5.3  | 5.9  | 4.7  | 5.9  | 5.5  | 5.3  | 4.3   | 4.7   | 4.6   |
| 260.              | 4.4  | 4.4  | 4.3  | 5.5  | 5.9  | 4.9  | 5.6  | 5.6  | 5.2  | 4.3   | 4.6   | 4.5   |
| 270.              | 4.6  | 4.5  | 4.3  | 5.6  | 6.0  | 5.3  | 5.0  | 5.5  | 5.1  | 4.3   | 4.5   | 4.4   |
| 280.              | 4.7  | 4.6  | 4.3  | 5.7  | 6.0  | 5.4  | 4.8  | 5.3  | 5.1  | 4.3   | 4.3   | 4.3   |
| 290.              | 4.8  | 4.7  | 4.3  | 5.8  | 5.9  | 5.8  | 4.6  | 5.3  | 5.1  | 4.3   | 4.3   | 4.3   |
| 300.              | 4.8  | 4.7  | 4.4  | 6.0  | 5.8  | 5.9  | 4.6  | 5.3  | 5.2  | 4.3   | 4.3   | 4.3   |
| 310.              | 4.8  | 4.7  | 4.4  | 6.1  | 5.8  | 5.9  | 4.7  | 5.3  | 5.2  | 4.3   | 4.3   | 4.3   |
| 320.              | 4.7  | 4.6  | 4.4  | 6.2  | 5.7  | 6.0  | 4.6  | 5.4  | 5.2  | 4.3   | 4.3   | 4.3   |
| 330.              | 4.7  | 4.6  | 4.4  | 6.4  | 5.8  | 5.9  | 4.5  | 5.5  | 5.3  | 4.3   | 4.3   | 4.3   |
| 340.              | 4.7  | 4.6  | 4.4  | 6.4  | 5.8  | 5.4  | 4.4  | 5.6  | 5.3  | 4.3   | 4.3   | 4.3   |
| 350.              | 4.7  | 4.9  | 4.9  | 6.3  | 5.9  | 5.4  | 4.3  | 5.3  | 5.2  | 4.5   | 4.7   | 4.3   |
| 360.              | 4.8  | 5.5  | 5.6  | 5.7  | 5.7  | 5.2  | 4.3  | 5.0  | 4.8  | 4.8   | 5.1   | 4.3   |
| MAX               | 5.5  | 6.6  | 6.6  | 6.4  | 6.3  | 6.0  | 6.3  | 6.2  | 5.8  | 6.2   | 6.5   | 5.3   |
| DEGR.             | 90   | 80   | 20   | 330  | 210  | 320  | 230  | 200  | 190  | 160   | 100   | 110   |

THE HIGHEST CONCENTRATION OF 6.60 PPM OCCURRED AT RECEPTOR REC3 .

DATE : 4/18/11  
 TIME : 8:47:54

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING  
 THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

| LINK # | *<br>*<br>*<br>* | CO/LINK (PPM) |            |            |             |             |             |             |             |             |              |              |              |
|--------|------------------|---------------|------------|------------|-------------|-------------|-------------|-------------|-------------|-------------|--------------|--------------|--------------|
|        |                  | REC1<br>90    | REC2<br>80 | REC3<br>20 | REC4<br>330 | REC5<br>210 | REC6<br>320 | REC7<br>230 | REC8<br>200 | REC9<br>190 | REC10<br>160 | REC11<br>100 | REC12<br>110 |
| 1      | *                | .0            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .0           |
| 2      | *                | .4            | .5         | .1         | .1          | .0          | .4          | .4          | .3          | .1          | .1           | .5           | .5           |
| 3      | *                | .0            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .0           |
| 4      | *                | .1            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .0           |
| 5      | *                | .1            | .3         | .1         | .0          | .0          | .4          | .3          | .1          | .0          | .1           | .3           | .1           |
| 6      | *                | .0            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .0           |
| 7      | *                | .1            | .2         | .1         | .0          | .0          | .5          | .7          | .0          | .0          | .0           | .3           | .0           |
| 8      | *                | .0            | .0         | .0         | .0          | .0          | .0          | .1          | .0          | .0          | .0           | .0           | .0           |
| 9      | *                | .0            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .0           |
| 10     | *                | .0            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .0           |
| 11     | *                | .1            | .3         | .4         | .5          | .4          | .1          | .1          | .4          | .3          | .4           | .3           | .1           |
| 12     | *                | .1            | .1         | .2         | .6          | .6          | .0          | .1          | .2          | .1          | .1           | .0           | .1           |
| 13     | *                | .0            | .0         | .0         | .0          | .0          | .1          | .0          | .0          | .3          | .1           | .1           | .0           |
| 14     | *                | .0            | .0         | .0         | .0          | .0          | .1          | .0          | .0          | .0          | .0           | .0           | .0           |
| 15     | *                | .0            | .0         | .0         | .0          | .0          | .0          | .0          | .0          | .0          | .0           | .0           | .0           |
| 16     | *                | .1            | .4         | .6         | .5          | .5          | .1          | .1          | .4          | .4          | .6           | .5           | .1           |
| 17     | *                | .1            | .2         | .3         | .1          | .2          | .0          | .1          | .2          | .2          | .4           | .2           | .0           |
| 18     | *                | .1            | .3         | .5         | .3          | .3          | .0          | .1          | .3          | .1          | .1           | .0           | .1           |