

Centered on Solutions<sup>SM</sup>

**S t r u c t u r a l A n a l y s i s R e p o r t**

*140' Existing ROHN SSV Lattice Tower*

*Proposed Verizon Wireless  
Antenna Installation*

*Verizon Site Ref: South Woodstock*

*87 West Quassett Road  
Woodstock, CT*

*Centek Project No. 09122*

*Date: September 13, 2011*



**Prepared for:**  
Verizon Wireless  
99 East River Road, 9<sup>th</sup> Floor  
East Hartford, CT 06108

**CENTEK** Engineering, Inc.

Structural Analysis - 140-ft ROHN SSV Lattice Tower

Verizon Wireless – S Woodstock

Woodstock, CT

September 13, 2011

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## Introduction

The purpose of this report is to summarize the results of the non-linear, P-Δ structural analysis of the existing self supporting lattice tower owned by American Tower Corporation (ATC), located in Woodstock, Connecticut for utilization by Verizon Wireless for a proposed typical panel antenna array installation.

The host tower is a 140-ft three legged, tapered steel lattice tower originally designed and manufactured by UNR-ROHN. The tower geometry and structure member sizes were obtained from standard UNR-ROHN self support tower design drawings with N series tower sections. Foundation information was also taken from UNR-ROHN standard design drawings with plan dimensions verified in the field.

The existing antenna and appurtenance inventory were obtained from a tower mapping and inventory report prepared by JWB tower Services, dated August 18, 2011.

The tower consists of six (6) tapered and one (1) straight vertical leg sections consisting of steel pipe conforming to ASTM A572-50 and solid round steel conforming to ASTM A36. Diagonal lateral support bracing consists of equal angle and solid round steel conforming to ASTM A36. All lateral bracing and flange plate connections are bolted with A325 bolts. The tower face width is 6.56-ft at the bottom tapering to 1.17-ft at the top.

## Antenna and Appurtenance Summary

The existing loads considered in the analysis consist of the following:

### Load Condition #1 - Existing Verizon equipment.

- VERIZON (Existing):

Antenna: Two (2) 11-ft Omni-directional whip antennas (one up, one inverted) mounted on a 6-ft stand-off frame with respective RAD center elevations of ±142.83-ft and 126.5-ft above the tower base.

Coax Cable: Two (2) 7/8" Ø coax cables running on the East leg of the existing tower as specified in Section 3 of this report.

### Load Condition #2 – PROPOSED VERIZON EQUIPMENT.

- VERIZON (Typical LTE Equipment Configuration):

Antenna: Fifteen (15) 5-ft x1-ft panel antennas mounted on three (3) 13-ft T-Frames with a RAD center elevation of ±140-ft above the tower base.

Coax Cables: Eighteen (18) 1-5/8" Ø coax cables running on the leg/face of the existing tower.

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### Primary Assumptions Used in the Analysis

- The tower structure's theoretical capacity not including any assessment of the condition of the tower.
- The tower carries the horizontal and vertical loads due to the weight of antennas, ice load and wind.
- Tower is properly installed and maintained.
- Tower is in plumb condition.
- Tower loading for antennas and mounts as listed in this report.
- All bolts are appropriately tightened providing the necessary connection continuity.
- All welds are fabricated with ER-70S-6 electrodes.
- All members are assumed to be as specified in the original tower design documents.
- All members are "hot dipped" galvanized in accordance with ASTM A123 and ASTM A153 Standards.
- All member protective coatings are in good condition.
- All tower members were properly designed, detailed, fabricated, installed and have been properly maintained since erection.
- Any deviation from the analyzed antenna loading will require a new analysis for verification of structural adequacy.
- **All coax cables routed as specified in Section 3 of this report.**

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## Analysis

The existing tower was analyzed using a comprehensive computer program entitled RISATower. The program analyzes the tower, considering the worst case loading condition. The tower is considered as loaded by concentric forces along the tower legs, and the model assumes that the leg members are subjected to bending, axial, and shear forces.

The existing tower was analyzed for 85mph basic wind speed (fastest mile) with no ice and 74mph with ½ inch accumulative ice to determine stresses in members as per guidelines of TIA/EIA-222-F-96 entitled "Structural Standards for Steel Antenna Towers and Antenna Supporting Structures", the American Institute of Steel Construction (AISC) and the Manual of Steel Construction; Allowable Stress Design (ASD).

## Tower Loading

Tower loading was determined by the basic wind speed as applied to projected surface areas with modification factors per TIA/EIA-222-F, gravity loads of the tower structure and its components, and the application of ½" radial ice tower structure and its components.

Basic Wind Speed: Windham v = 80 mph  
(fastest mile) [Section 16 of TIA/EIA-222-F-96]

Woodstock; v = 100 mph (3 second gust) equivalent to v = 85 mph (fastest mile) [Appendix K of the 2005 CT Building Code Supplement]

*Appendix K wind speed criteria controls.*

Load Cases: Load Case 1; 85 mph wind speed w/ no ice plus gravity load – used in calculation of tower stresses. [Section 2.3.16 of TIA/EIA-222-F-96]

Load Case 2; 74 mph wind speed w/ ½" radial ice plus gravity load – used in calculation of tower stresses. This load case typically controls the design of lattice towers. [Section 2.3.16 of TIA/EIA-222-F-96]

Load Case 3; 45 mph wind speed w/ no ice plus gravity load – used in calculation of tower stresses. [Does not conform to Section 2.3.16 of TIA/EIA-222-F-96]

Load Case 4; 39 mph wind speed w/ ½" radial ice plus gravity load – used in calculation of tower stresses. This load case typically controls the design of lattice towers. [Does not conform to Section 2.3.16 of TIA/EIA-222-F-96]

Load Case 6; Seismic – not checked [Section 1614.5 of State Bldg. Code 2005] does not control in the design of this structure type

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## Tower Capacity

Tower stresses were calculated utilizing the structural analysis software RISATower. Allowable stresses were determined based on Table 5 of the TIA/EIA code with a 1/3 increase per Section 3.1.1.1 of the same code.

**Under Load Condition #1 (existing conditions)** the tower program failed to converge based on excessive displacement of the structure. Successive analyses utilizing the same loading condition were conducted at reduced wind speeds until the stability of the structure was within the program tolerances and convergence was possible. Convergence of the tower was only possible by reducing the basic wind speed (fastest mile) to 45mph without ice and 39mph with 1/2in radial ice, which does not meet the provisions of the TIA/EIA standard or Appendix K of the Connecticut State Building Code.

Calculated stresses were evaluated at the aforementioned reduced wind speed and were **NOT** found to be within allowable limits. In Load Case 4, per RISATower "Section Capacity Table", this tower was found to be **271.1%** of its total capacity. Please refer to Table 1 below for reference.

<u>Table 1.</u>			
Tower Section	Elevation	Stress Ratio (percentage of capacity)	Result
Leg (T1)	140'-0"- 120'-0"	271.1%	<b>FAIL</b>
Leg (T2)	120'-0"- 100'-0"	163.7%	<b>FAIL</b>
Leg (T3)	100'-0"- 80'-0"	102.6%	<b>FAIL</b>

Note: The above results are based on the assumption that all tower members were properly designed, detailed, fabricated, installed and have been properly maintained since erection. A review of the tower mapping report finds that some of the tower members are damaged and warrant replacement. Additionally, the effects of the vegetative growth observed on the lower section of the tower were not considered in evaluation of the tower.

**Load Condition #2 (proposed equipment)** was not evaluated. Considering the significant overstress under Load Condition #1 it is safe to assume that the subject tower will not accommodate any additional loading.

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Woodstock, CT

September 13, 2011

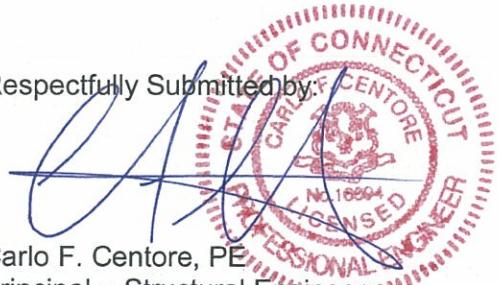
### Conclusion

This analysis finds that the subject tower structure is not adequate to support the existing or proposed loading condition. Reinforcement of the structure is considered impracticable due to the magnitude of overstress displayed and the instability of the structure. Replacement of the tower structure in its entirety is warranted.

The analysis provided is based, in part, on the information provided to this office by Verizon Wireless. If the existing conditions are different than the information in this report, Centek Engineering, Inc. must be contacted for resolution of any potential issues.

Please feel free to call with any questions or comments.

Respectfully Submitted by:



Carlo F. Centore, PE  
Principal ~ Structural Engineer

Prepared by:

Jason R. Mead  
Structural Engineer

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**Standard Conditions for Furnishing of  
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Existing Structures**

All engineering services are performed on the basis that the information used is current and correct. This information may consist of, but is not necessarily limited to:

- Information supplied by the client regarding the structure itself, its foundations, the soil conditions, the antenna and feed line loading on the structure and its components, or other relevant information.
- Information from the field and/or drawings in the possession of Centek Engineering, Inc. or generated by field inspections or measurements of the structure.
- It is the responsibility of the client to ensure that the information provided to Centek Engineering, Inc. and used in the performance of our engineering services is correct and complete. In the absence of information to the contrary, we assume that all structures were constructed in accordance with the drawings and specifications and are in an un-corroded condition and have not deteriorated. It is therefore assumed that its capacity has not significantly changed from the "as new" condition.
- All services will be performed to the codes specified by the client, and we do not imply to meet any other codes or requirements unless explicitly agreed in writing. If wind and ice loads or other relevant parameters are to be different from the minimum values recommended by the codes, the client shall specify the exact requirement. In the absence of information to the contrary, all work will be performed in accordance with the latest revision of ANSI/ASCE10 & ANSI/EIA-222
- All services performed, results obtained, and recommendations made are in accordance with generally accepted engineering principles and practices. Centek Engineering, Inc. is not responsible for the conclusions, opinions and recommendations made by others based on the information we supply.

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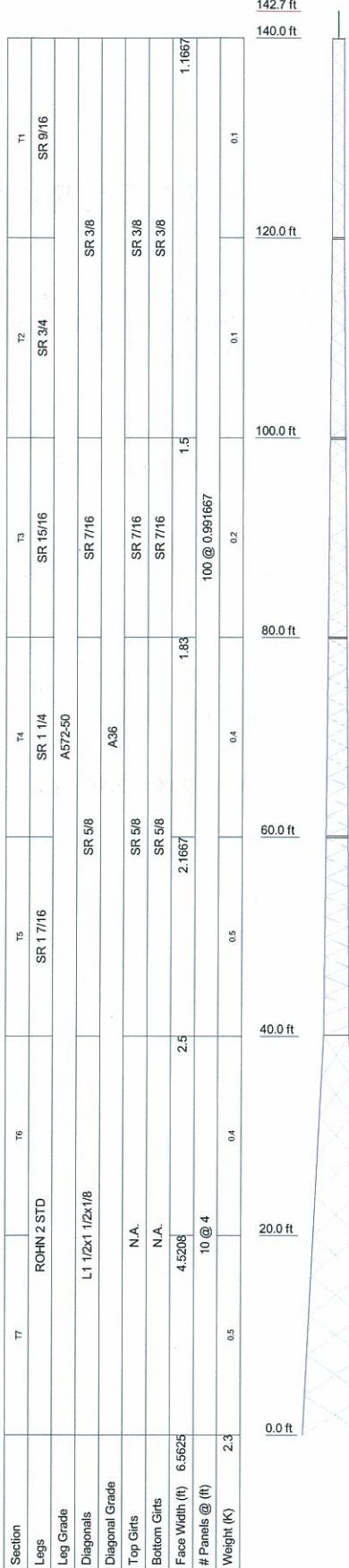
*September 13, 2011*

## GENERAL DESCRIPTION OF STRUCTURAL ANALYSIS PROGRAM

RISATower, is an integrated structural analysis and design software package for Designed specifically for the telecommunications industry, RISATower, formerly ERITower, automates much of the tower analysis and design required by the TIA/EIA 222 Standard.

### RISATower Features:

- RISATower can analyze and design 3- and 4-sided guyed towers, 3- and 4-sided self-supporting towers and either round or tapered ground mounted poles with or without guys.
- The program analyzes towers using the TIA-222-G (2005) standard or any of the previous TIA/EIA standards back to RS-222 (1959). Steel design is checked using the AISC ASD 9th Edition or the AISC LRFD specifications.
- Linear and non-linear (P-delta) analyses can be used in determining displacements and forces in the structure. Wind pressures and forces are automatically calculated.
- Extensive graphics plots include material take-off, shear-moment, leg compression, displacement, twist, feed line, guy anchor and stress plots.
- RISATower contains unique features such as True Cable behavior, hog rod take-up, foundation stiffness and much more.



### DESIGNED APPURTEINANCE LOADING

TYPE	ELEVATION	TYPE	ELEVATION
11' x 3" Dia Omni (ATC)	143	11' x 3" Dia Omni (ATC)	127
Rohn 6' Side-Arm(1) (ATC)	134.67		

### MATERIAL STRENGTH

GRADE	Fy	Fu	GRADE	Fy	Fu
A572-50	50 ksi	65 ksi	A36	36 ksi	58 ksi

### TOWER DESIGN NOTES

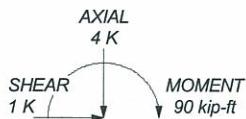
1. Tower is located in Windham County, Connecticut.
2. Tower designed for a 45 mph basic wind in accordance with the TIA/EIA-222-F Standard.
3. Tower is also designed for a 39 mph basic wind with 0.50 in ice.
4. Deflections are based upon a 50 mph wind.
5. 2.67 ft ROHN Tapered Top is included for load transfer only.
6. Load Condition #1 - Existing Tower
7. TOWER RATING: 271.1%

#### MAX. CORNER REACTIONS AT BASE:

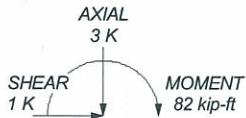
DOWN: 17 K

UPLIFT: -14 K

SHEAR: 1 K



TORQUE 1 kip-ft  
39 mph WIND - 0.5000 in ICE



TORQUE 1 kip-ft  
REACTIONS - 45 mph WIND

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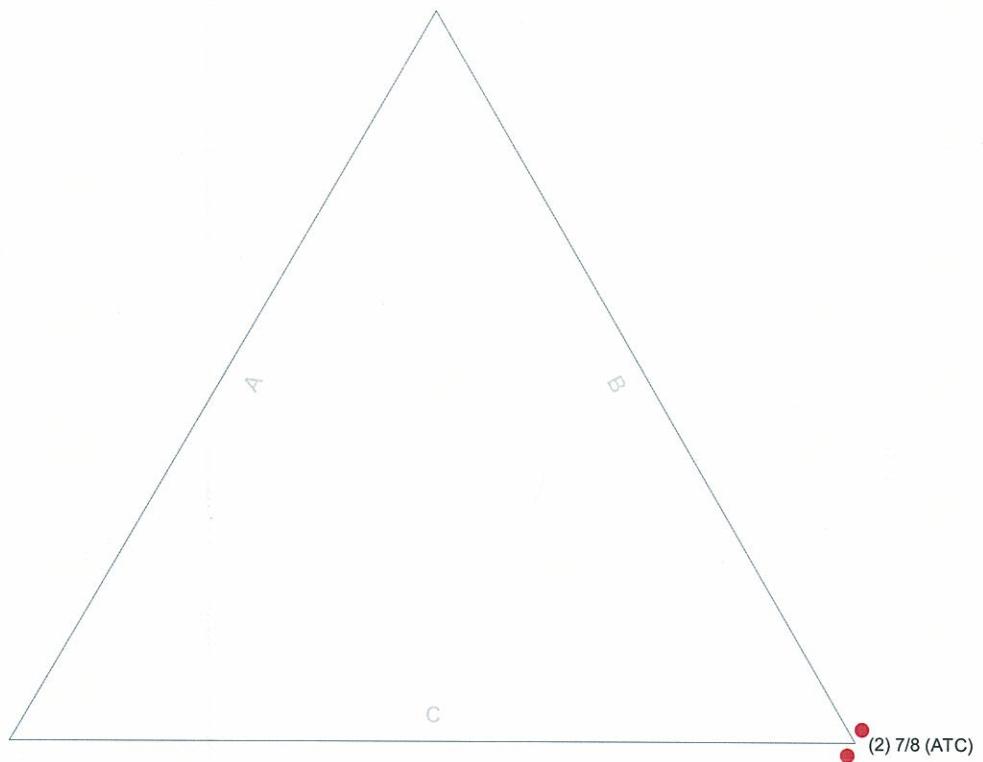
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Job: 140-ft ROHN SSV Woodstock - Exist

Project: 87 West Quasset Road	Drawn by: Jrm	App'd:
Client: Verizon Wireless		
Code: TIA/EIA-222-F	Date: 09/02/11	Scale: NTS
Path: E-1		

# Feedline Plan

Round \_\_\_\_\_ Flat \_\_\_\_\_ App In Face \_\_\_\_\_ App Out Face \_\_\_\_\_



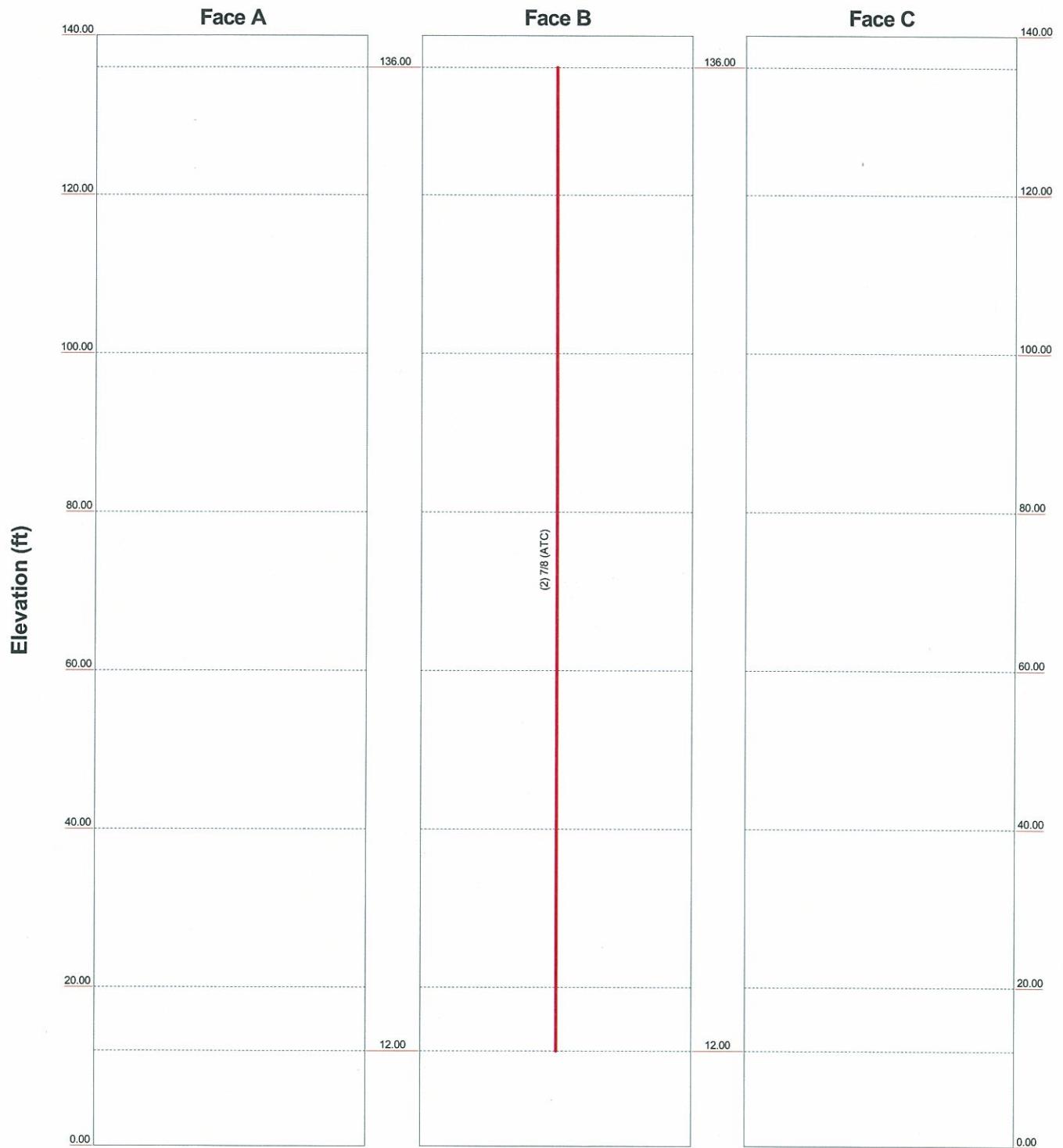
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Project: 87 West Quasset Road		
Client:	Drawn by:	App'd:
Verizon Wireless	Jrm	
Code: TIA/EIA-222-F	Date: 09/02/11	Scale: NTS
Path:		Dwg No. E-7

# Feedline Distribution Chart

**0' - 140'**

— Round    
 — Flat    
 — App In Face    
 — App Out Face    
 — Truss Leg

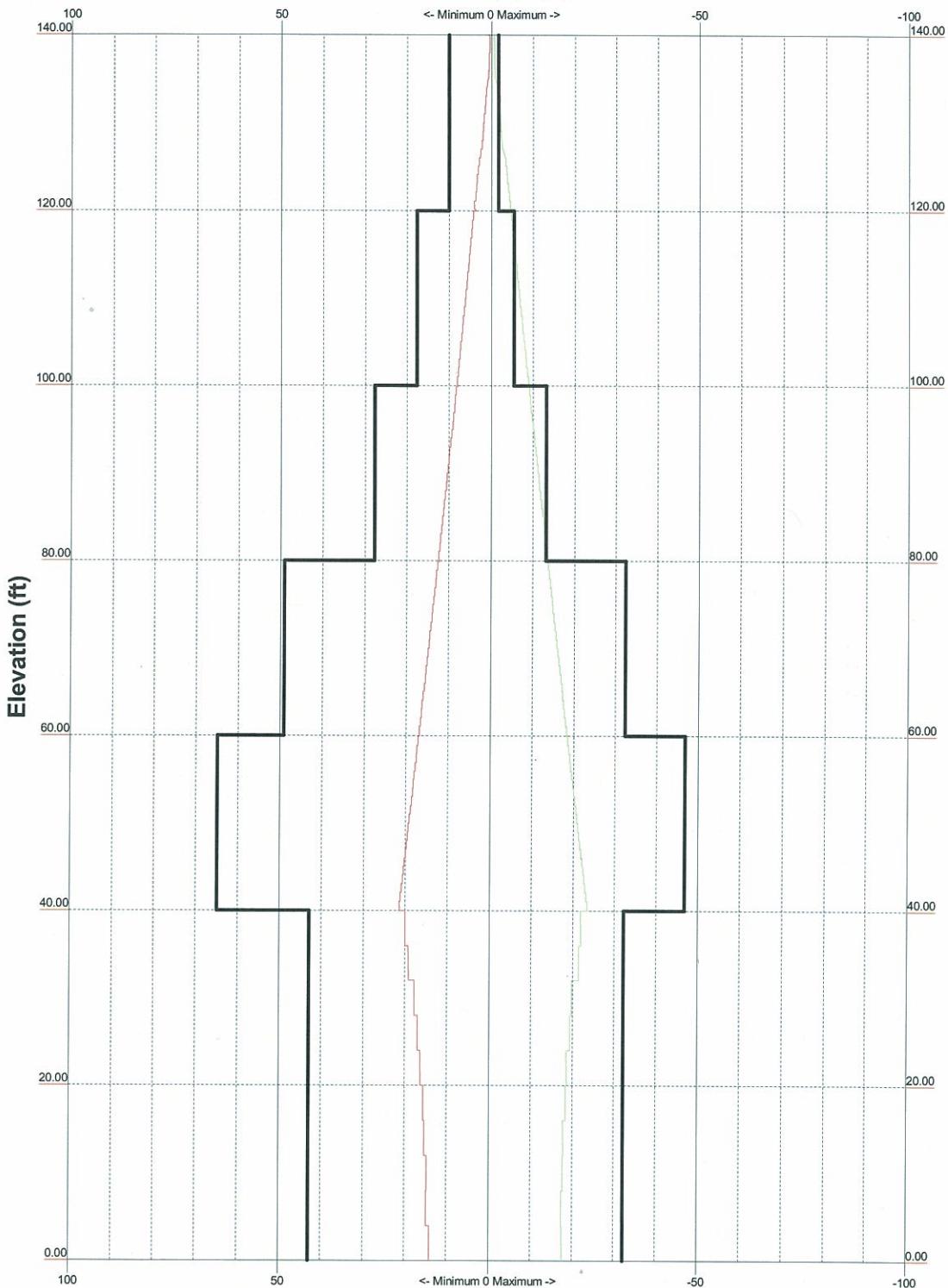


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Project: <b>87 West Quasset Road</b>		
Client: Verizon Wireless	Drawn by: Jrm	App'd:
Code: TIA/EIA-222-F	Date: 09/02/11	Scale: NTS
Path:		Dwg No. E-7

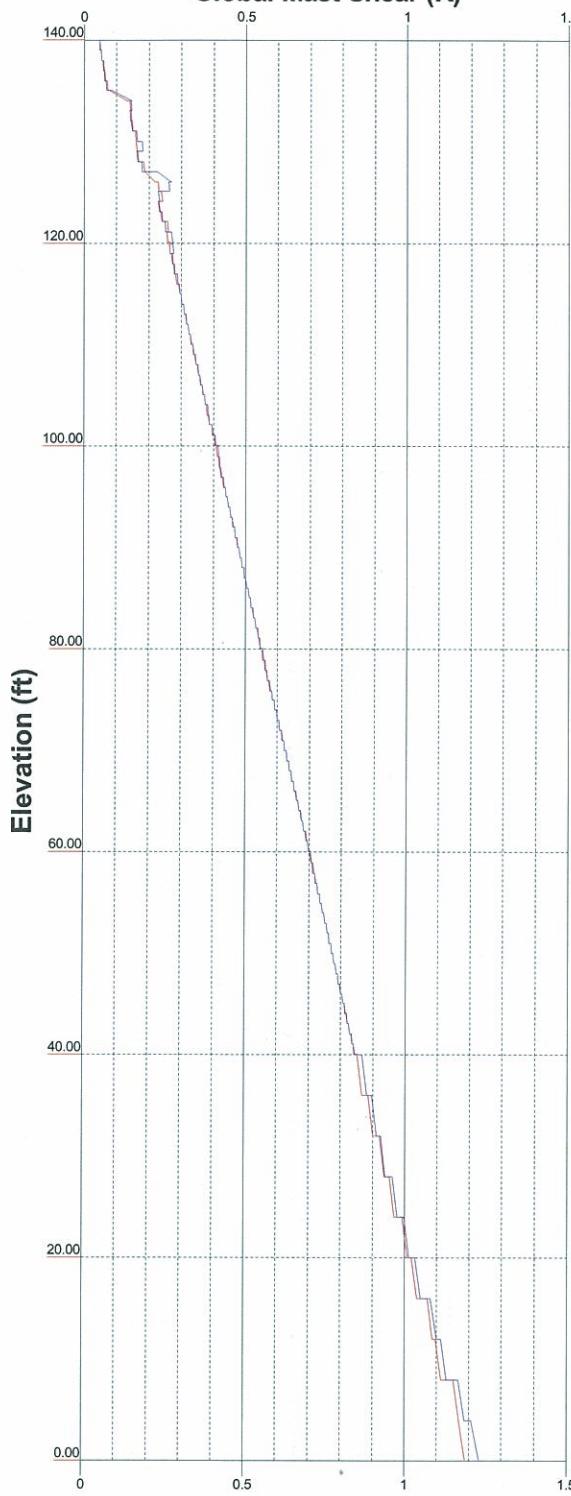
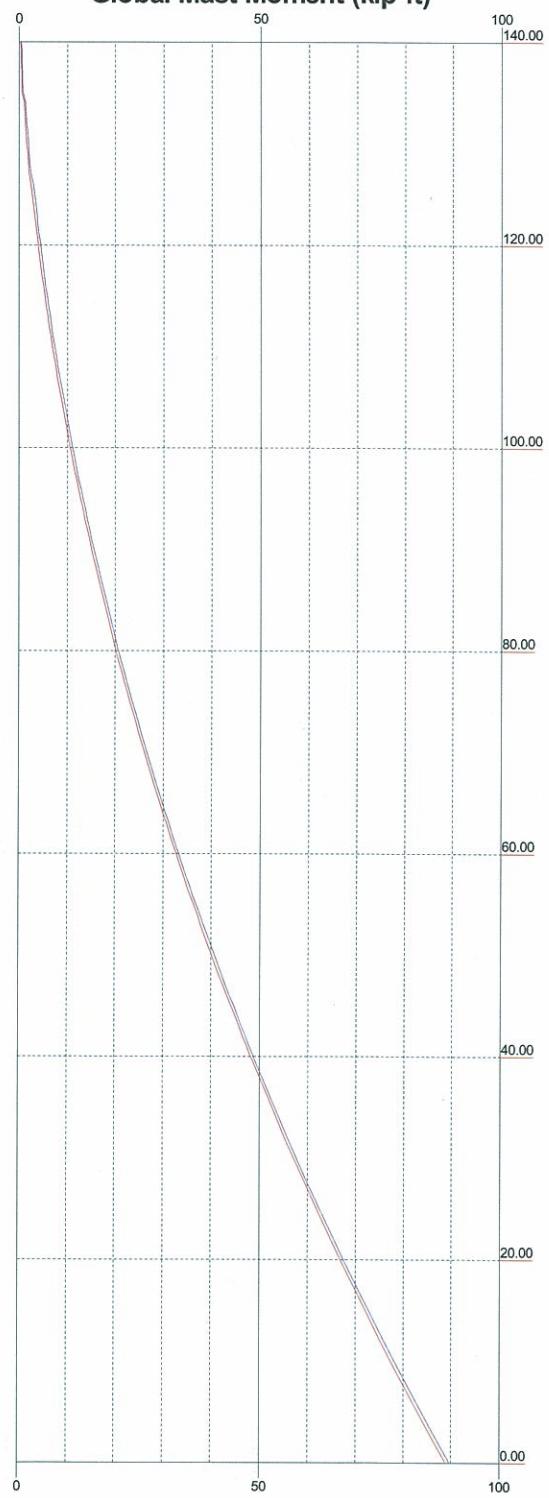
**TIA/EIA-222-F - 45 mph/39 mph 0.5000 in Ice**

**Leg Capacity** — **Leg Compression (K)**



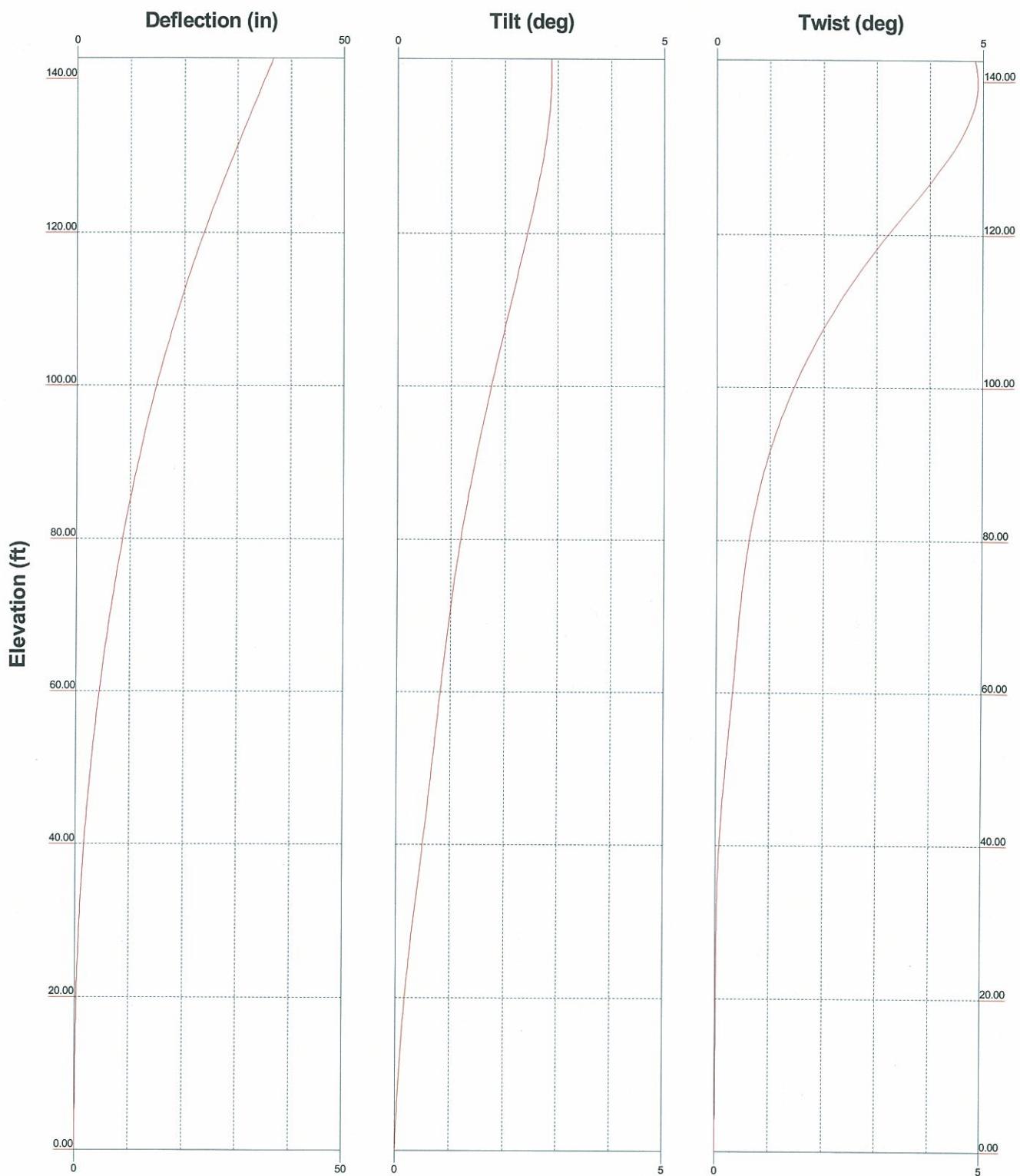
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Path: Dwg No. E-3

**Global Mast Shear (K)****Global Mast Moment (kip-ft)**

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Client: Verizon Wireless Drawn by: Jrm App'd:  
Code: TIA/EIA-222-F Date: 09/02/11 Scale: NTS  
Path: Dwg No. E-4



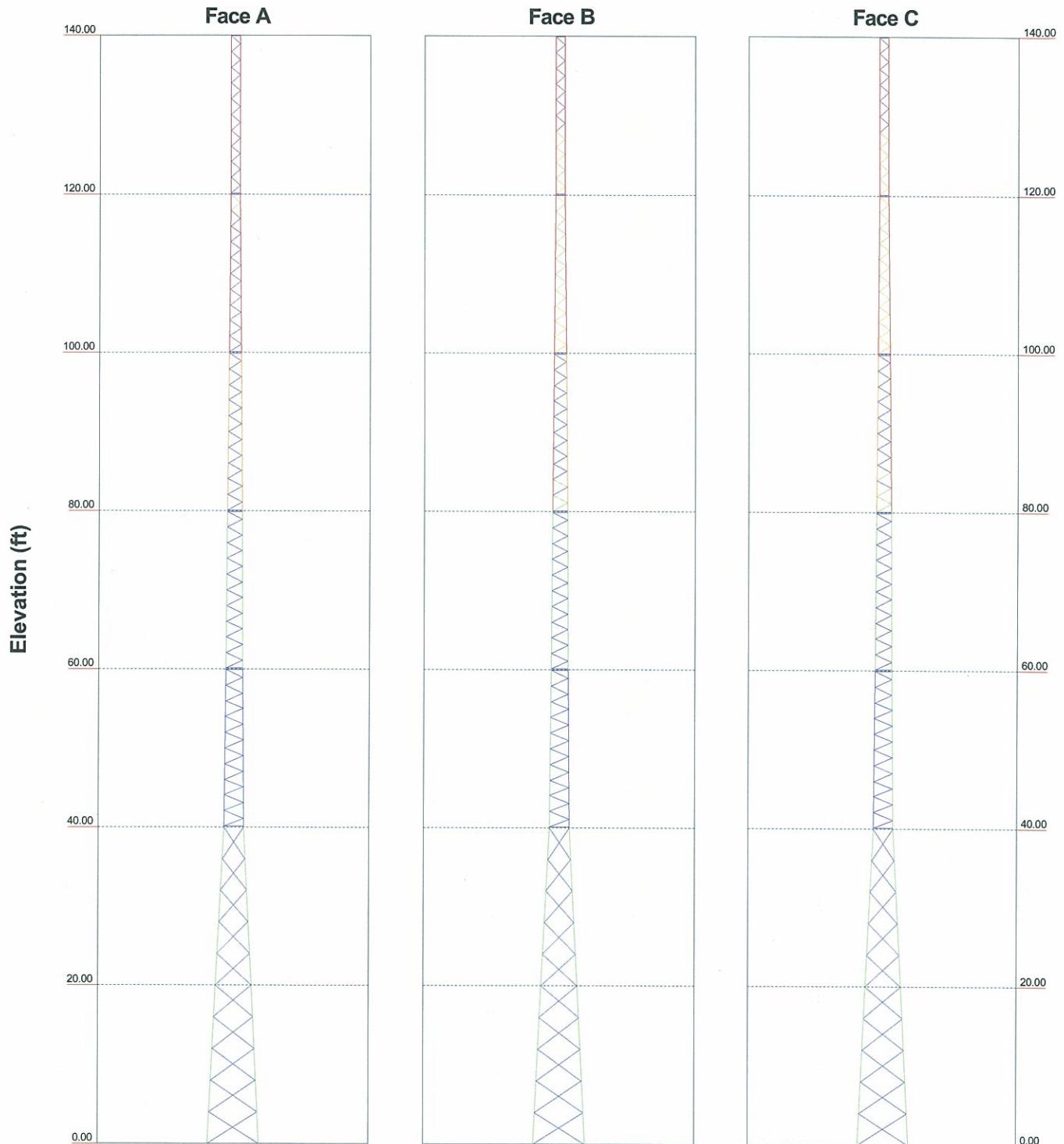
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Project: **87 West Quasset Road**  
Client: Verizon Wireless Drawn by: Jrm App'd:  
Code: **TIA/EIA-222-F** Date: **09/02/11** Scale: **NTS**  
Path: **E-5**

### Stress Distribution Chart

0' - 140'

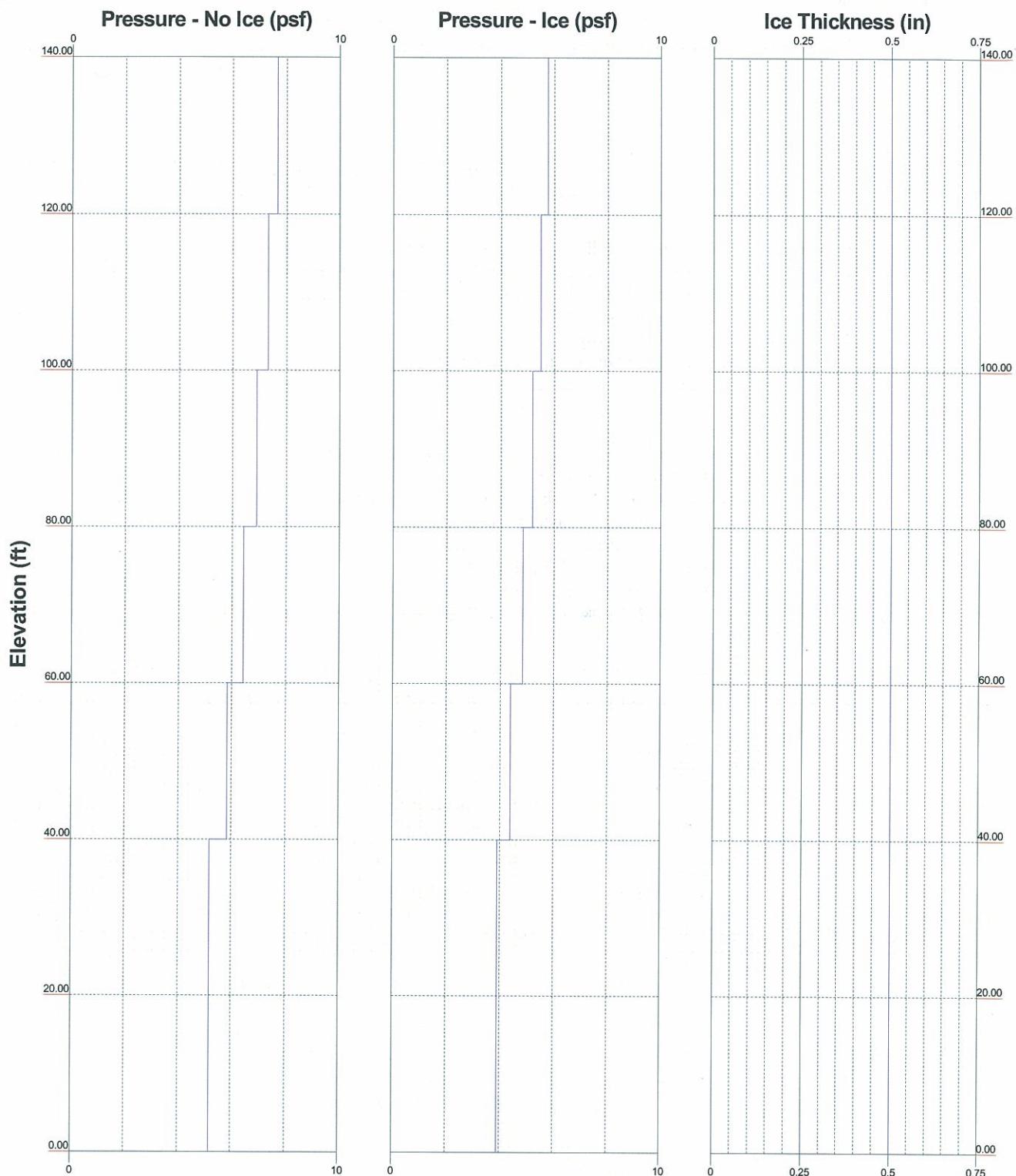
█ > 100%   
 █ 90%-100%   
 █ 75%-90%   
 █ 50%-75%   
 █ < 50% Overstress



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Path:		Dwg No: E-8	

**Wind Pressures and Ice Thickness**  
 TIA/EIA-222-F - 45 mph/39 mph 0.5000 in Ice



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FAX: (203) 488-8587	App'd:
	Code: <b>TIA/EIA-222-F</b>
	Date: <b>09/02/11</b>
	Scale: <b>NTS</b>
	Path: <b>Dwg No. E-9</b>

<b>RISATower</b>	<b>Job</b> 140-ft ROHN SSV Woodstock - Exist	<b>Page</b> 1 of 26
<b>CENTEK Engineering, Inc.</b> 63-2 N Branford Rd Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	<b>Project</b> 87 West Quasset Road	<b>Date</b> 16:18:22 09/02/11
	<b>Client</b> Verizon Wireless	<b>Designed by</b> Jrm

## Tower Input Data

The main tower is a 3x free standing tower with an overall height of 140.00 ft above the ground line.

The base of the tower is set at an elevation of 0.00 ft above the ground line.

The face width of the tower is 1.17 ft at the top and 6.56 ft at the base.

This tower is designed using the TIA/EIA-222-F standard.

The following design criteria apply:

Tower is located in Windham County, Connecticut.

Basic wind speed of 45 mph.

Nominal ice thickness of 0.5000 in.

Ice density of 56 pcf.

A wind speed of 39 mph is used in combination with ice.

Temperature drop of 50 °F.

Deflections calculated using a wind speed of 50 mph.

Load Condition #1 - Existing Tower.

A non-linear (P-delta) analysis was used.

Pressures are calculated at each section.

Stress ratio used in tower member design is 1.333.

Local bending stresses due to climbing loads, feedline supports, and appurtenance mounts are not considered.

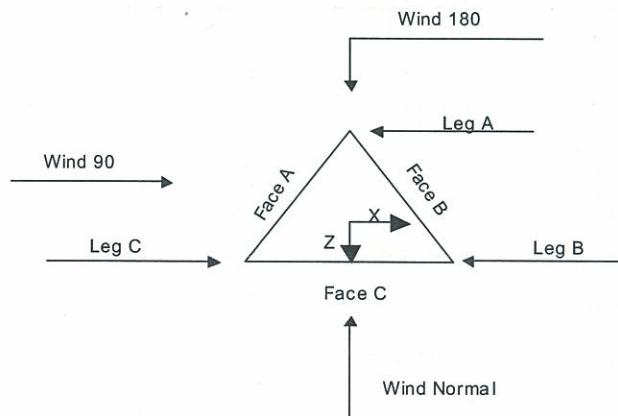
## Options

- |                                     |                                      |                                      |
|-------------------------------------|--------------------------------------|--------------------------------------|
| Consider Moments - Legs             | Distribute Leg Loads As Uniform      | ✓ Treat Feedline Bundles As Cylinder |
| Consider Moments - Horizontals      | Assume Legs Pinned                   | Use ASCE 10 X-Brace Ly Rules         |
| Consider Moments - Diagonals        | ✓ Assume Rigid Index Plate           | Calculate Redundant Bracing Forces   |
| Use Moment Magnification            | ✓ Use Clear Spans For Wind Area      | Ignore Redundant Members in FEA      |
| ✓ Use Code Stress Ratios            | ✓ Use Clear Spans For KL/r           | SR Leg Bolts Resist Compression      |
| ✓ Use Code Safety Factors - Guys    | Retention Guys To Initial Tension    | ✓ All Leg Panels Have Same Allowable |
| Escalate Ice                        | Bypass Mast Stability Checks         | Offset Girt At Foundation            |
| Always Use Max Kz                   | ✓ Use Azimuth Dish Coefficients      | ✓ Consider Feedline Torque           |
| Use Special Wind Profile            | Project Wind Area of Appurt.         | Include Angle Block Shear Check      |
| ✓ Include Bolts In Member Capacity  | Autocalc Torque Arm Areas            | Poles                                |
| Leg Bolts Are At Top Of Section     | ✓ SR Members Have Cut Ends           | Include Shear-Torsion Interaction    |
| Secondary Horizontal Braces Leg     | ✓ Sort Capacity Reports By Component | Always Use Sub-Critical Flow         |
| Use Diamond Inner Bracing (4 Sided) | Triangulate Diamond Inner Bracing    | Use Top Mounted Sockets              |
| Add IBC .6D+W Combination           |                                      |                                      |

# RISA Tower

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Job	140-ft ROHN SSV Woodstock - Exist	Page	2 of 26
Project	87 West Quasset Road	Date	16:18:22 09/02/11
Client	Verizon Wireless	Designed by	Jrm



Triangular Tower

## Tower Section Geometry

Tower Section	Tower Elevation	Assembly Database	Description	Section Width	Number of Sections	Section Length
				ft	ft	ft
T1	140.00-120.00			1.17	1	20.00
T2	120.00-100.00			1.17	1	20.00
T3	100.00-80.00			1.50	1	20.00
T4	80.00-60.00			1.83	1	20.00
T5	60.00-40.00			2.17	1	20.00
T6	40.00-20.00			2.50	1	20.00
T7	20.00-0.00			4.52	1	20.00

## Tower Section Geometry (cont'd)

Tower Section	Tower Elevation	Diagonal Spacing	Bracing Type	Has K Brace End Panels	Has Horizontals	Top Girt Offset	Bottom Girt Offset
	ft	ft				in	in
T1	140.00-120.00	0.99	K Brace Left	No	No	1.0000	1.0000
T2	120.00-100.00	0.99	K Brace Left	No	No	1.0000	1.0000
T3	100.00-80.00	0.99	K Brace Left	No	No	1.0000	1.0000
T4	80.00-60.00	0.99	K Brace Left	No	No	1.0000	1.0000
T5	60.00-40.00	0.99	K Brace Left	No	No	1.0000	1.0000
T6	40.00-20.00	4.00	X Brace	No	No	0.0000	0.0000
T7	20.00-0.00	4.00	X Brace	No	No	0.0000	0.0000

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	<b>Project</b>	87 West Quasset Road	<b>Date</b>	16:18:22 09/02/11
	<b>Client</b>	Verizon Wireless	<b>Designed by</b>	Jrm

### Tower Section Geometry (cont'd)

Tower Elevation ft	Leg Type	Leg Size	Leg Grade	Diagonal Type	Diagonal Size	Diagonal Grade
T1 140.00-120.00	Solid Round	9/16	A572-50 (50 ksi)	Solid Round	3/8	A36 (36 ksi)
T2 120.00-100.00	Solid Round	3/4	A572-50 (50 ksi)	Solid Round	3/8	A36 (36 ksi)
T3 100.00-80.00	Solid Round	15/16	A572-50 (50 ksi)	Solid Round	7/16	A36 (36 ksi)
T4 80.00-60.00	Solid Round	1 1/4	A572-50 (50 ksi)	Solid Round	5/8	A36 (36 ksi)
T5 60.00-40.00	Solid Round	1 7/16	A572-50 (50 ksi)	Solid Round	5/8	A36 (36 ksi)
T6 40.00-20.00	Pipe	ROHN 2 STD	A572-50 (50 ksi)	Equal Angle	L1 1/2x1 1/2x1/8	A36 (36 ksi)
T7 20.00-0.00	Pipe	ROHN 2 STD	A572-50 (50 ksi)	Equal Angle	L1 1/2x1 1/2x1/8	A36 (36 ksi)

### Tower Section Geometry (cont'd)

Tower Elevation ft	Top Girt Type	Top Girt Size	Top Girt Grade	Bottom Girt Type	Bottom Girt Size	Bottom Girt Grade
T1 140.00-120.00	Solid Round	3/8	A36 (36 ksi)	Solid Round	3/8	A36 (36 ksi)
T2 120.00-100.00	Solid Round	3/8	A36 (36 ksi)	Solid Round	3/8	A36 (36 ksi)
T3 100.00-80.00	Solid Round	7/16	A36 (36 ksi)	Solid Round	7/16	A36 (36 ksi)
T4 80.00-60.00	Solid Round	5/8	A36 (36 ksi)	Solid Round	5/8	A36 (36 ksi)
T5 60.00-40.00	Solid Round	5/8	A36 (36 ksi)	Solid Round	5/8	A36 (36 ksi)

### Tower Section Geometry (cont'd)

Tower Elevation ft	Gusset Area (per face) ft <sup>2</sup>	Gusset Thickness in	Gusset Grade	Adjust. Factor $A_f$	Adjust. Factor $A_r$	Weight Mult.	Double Angle Stitch Bolt Spacing Diagonals in	Double Angle Stitch Bolt Spacing Horizontals in
T1 140.00-120.00	0.00	0.0000	A36 (36 ksi)	1	1	1.02	36.0000	36.0000
T2 120.00-100.00	0.00	0.0000	A36 (36 ksi)	1	1	1.02	36.0000	36.0000
T3 100.00-80.00	0.00	0.0000	A36 (36 ksi)	1	1	1.02	36.0000	36.0000
T4 80.00-60.00	0.00	0.0000	A36 (36 ksi)	1	1	1.02	36.0000	36.0000

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Tower Elevation	Gusset Area (per face)	Gusset Thickness	Gusset Grade	Adjust. Factor $A_f$	Adjust. Factor $A_r$	Weight Mult.	Double Angle Stitch Bolt Spacing Diagonals	Double Angle Stitch Bolt Spacing Horizontals
ft	ft <sup>2</sup>	in					in	in
T5 60.00-40.00	0.00	0.0000	A36 (36 ksi)	1	1	1.02	36.0000	36.0000
T6 40.00-20.00	0.00	0.0000	A36 (36 ksi)	1	1	1.02	36.0000	36.0000
T7 20.00-0.00	0.00	0.0000	A36 (36 ksi)	1	1	1.02	36.0000	36.0000

## Tower Section Geometry (cont'd)

<sup>1</sup>Note: K factors are applied to member segment lengths. K-braces without inner supporting members will have the K factor in the out-of-plane direction applied to the overall length.

## Tower Section Geometry (cont'd)

<b>RISATower</b>  <b>CENTEK Engineering, Inc.</b> 63-2 N Branford Rd Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job	140-ft ROHN SSV Woodstock - Exist	Page
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### Tower Section Geometry (cont'd)

Tower Elevation ft	Leg Connection Type	Leg		Diagonal		Top Girt		Bottom Girt		Mid Girt		Long Horizontal		Short Horizontal	
		Bolt Size	No.	Bolt Size	No.	Bolt Size	No.	Bolt Size	No.	Bolt Size	No.	Bolt Size	No.	Bolt Size	No.
T1 140.00-	Flange	0.3750	4	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
120.00		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T2 120.00-	Flange	0.3750	4	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
100.00		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T3 100.00-	Flange	0.5000	4	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
80.00		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T4 80.00-60.00	Flange	0.6250	4	0.3750	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T5 60.00-40.00	Flange	0.6250	4	0.3750	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T6 40.00-20.00	Flange	0.6250	4	0.5000	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T7 20.00-0.00	Flange	0.6250	4	0.5000	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	

### Feed Line/Linear Appurtenances - Entered As Round Or Flat

Description	Face or Leg	Allow Shield	Component Type	Placement ft	Total Number	Number Per Row	Clear Spacing in	Width or Diameter in	Perimeter in	Weight plf
7/8 (ATC)	B	No	Ar (Leg)	136.00 - 12.00	2	1	1.1100	1.1100		0.54

### Feed Line/Linear Appurtenances Section Areas

Tower Section	Tower Elevation ft	Face	$A_R$ ft <sup>2</sup>	$A_F$ ft <sup>2</sup>	$C_A A_{A\ In Face}$ ft <sup>2</sup>	$C_A A_{A\ Out Face}$ ft <sup>2</sup>	Weight K
T1	140.00-120.00	A	0.000	0.000	0.000	0.000	0.00
		B	2.960	0.000	0.000	0.000	0.02
		C	2.960	0.000	0.000	0.000	0.00
T2	120.00-100.00	A	0.000	0.000	0.000	0.000	0.00
		B	3.700	0.000	0.000	0.000	0.02
		C	3.700	0.000	0.000	0.000	0.00
T3	100.00-80.00	A	0.000	0.000	0.000	0.000	0.00
		B	3.700	0.000	0.000	0.000	0.02
		C	3.700	0.000	0.000	0.000	0.00
T4	80.00-60.00	A	0.000	0.000	0.000	0.000	0.00
		B	3.700	0.000	0.000	0.000	0.02
		C	3.700	0.000	0.000	0.000	0.00
T5	60.00-40.00	A	0.000	0.000	0.000	0.000	0.00
		B	3.700	0.000	0.000	0.000	0.02
		C	3.700	0.000	0.000	0.000	0.00
T6	40.00-20.00	A	0.000	0.000	0.000	0.000	0.00
		B	3.700	0.000	0.000	0.000	0.02

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Tower Section	Tower Elevation ft	Face	$A_R$ ft <sup>2</sup>	$A_F$ ft <sup>2</sup>	$C_A A_A$ In Face ft <sup>2</sup>	$C_A A_A$ Out Face ft <sup>2</sup>	Weight K
T7	20.00-0.00	C	3.700	0.000	0.000	0.000	0.00
		A	0.000	0.000	0.000	0.000	0.00
		B	1.480	0.000	0.000	0.000	0.01
		C	1.480	0.000	0.000	0.000	0.00

### Feed Line/Linear Appurtenances Section Areas - With Ice

Tower Section	Tower Elevation ft	Face or Leg	Ice Thickness in	$A_R$ ft <sup>2</sup>	$A_F$ ft <sup>2</sup>	$C_A A_A$ In Face ft <sup>2</sup>	$C_A A_A$ Out Face ft <sup>2</sup>	Weight K
T1	140.00-120.00	A	0.500	0.000	0.000	0.000	0.000	0.00
		B		5.627	0.000	0.000	0.000	0.05
		C		5.627	0.000	0.000	0.000	0.00
T2	120.00-100.00	A	0.500	0.000	0.000	0.000	0.000	0.00
		B		7.033	0.000	0.000	0.000	0.06
		C		7.033	0.000	0.000	0.000	0.00
T3	100.00-80.00	A	0.500	0.000	0.000	0.000	0.000	0.00
		B		7.033	0.000	0.000	0.000	0.06
		C		7.033	0.000	0.000	0.000	0.00
T4	80.00-60.00	A	0.500	0.000	0.000	0.000	0.000	0.00
		B		7.033	0.000	0.000	0.000	0.06
		C		7.033	0.000	0.000	0.000	0.00
T5	60.00-40.00	A	0.500	0.000	0.000	0.000	0.000	0.00
		B		7.033	0.000	0.000	0.000	0.06
		C		7.033	0.000	0.000	0.000	0.00
T6	40.00-20.00	A	0.500	0.000	0.000	0.000	0.000	0.00
		B		7.033	0.000	0.000	0.000	0.06
		C		7.033	0.000	0.000	0.000	0.00
T7	20.00-0.00	A	0.500	0.000	0.000	0.000	0.000	0.00
		B		2.813	0.000	0.000	0.000	0.02
		C		2.813	0.000	0.000	0.000	0.00

### Feed Line Center of Pressure

Section	Elevation ft	$CP_x$ in	$CP_z$ in	$CP_x$ Ice in	$CP_z$ Ice in
T1	140.00-120.00	1.4280	0.8244	1.0433	0.6024
T2	120.00-100.00	1.6345	0.9437	1.2984	0.7496
T3	100.00-80.00	1.7465	1.0083	1.4680	0.8476
T4	80.00-60.00	1.6369	0.9451	1.5252	0.8806
T5	60.00-40.00	1.7276	0.9974	1.6470	0.9509
T6	40.00-20.00	1.5548	0.8976	1.8650	1.0768
T7	20.00-0.00	0.8500	0.4907	1.0313	0.5954

### Antenna Pole Forces ROHN Tapered Top

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Length of Pole	<i>I<sub>x</sub></i>	<i>I<sub>y</sub></i>	Modulus <i>E</i>	Antenna Pole <i>C<sub>A</sub>A<sub>A</sub></i>	Antenna Pole Weight <i>p/lf</i>	Length of Beacon	Beacon <i>C<sub>A</sub>A<sub>A</sub></i>	Beacon Weight
ft	in <sup>4</sup>	in <sup>4</sup>	ksi	ft <sup>2</sup> /ft	ft	ft	ft <sup>2</sup>	K
2.67	1.0000	1.0000	29000	No Ice With Ice	0.24 0.34	0.07 0.10	0.00	0.00 0.00

### Discrete Tower Loads

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustment	Placement	<i>C<sub>A</sub>A<sub>A</sub></i> Front	<i>C<sub>A</sub>A<sub>A</sub></i> Side	Weight
			ft ft ft	°	ft	ft <sup>2</sup>	ft <sup>2</sup>	K
11' x 3" Dia Omni (ATC)	B	From Leg	6.00 0.00 0.00	0.0000	143.00	No Ice 1/2" Ice	3.30 4.43	3.30 4.43 0.06
11' x 3" Dia Omni (ATC)	B	From Leg	6.00 0.00 0.00	0.0000	127.00	No Ice 1/2" Ice	3.30 4.43	3.30 4.43 0.06
Rohn 6' Side-Arm(1) (ATC)	B	From Leg	3.00 0.00 0.00	0.0000	134.67	No Ice 1/2" Ice	5.04 6.78	5.04 6.78 0.11 0.14

### Tower Pressures - No Ice

$$G_H = 1.138$$

Section Elevation	<i>z</i>	<i>K<sub>Z</sub></i>	<i>q<sub>z</sub></i>	<i>A<sub>G</sub></i>	<i>F a c e</i>	<i>A<sub>F</sub></i>	<i>A<sub>R</sub></i>	<i>A<sub>leg</sub></i>	Leg %	<i>C<sub>A</sub>A<sub>A</sub></i> In Face ft <sup>2</sup>	<i>C<sub>A</sub>A<sub>A</sub></i> Out Face ft <sup>2</sup>
	ft	ft	psf	ft <sup>2</sup>		ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>			
T1 140.00- 120.00	130.00	1.48	8	24.272	A B C	0.000 0.000 0.000	2.864 5.824 5.824	1.875	65.48	0.000	0.000
T2 120.00- 100.00	110.00	1.411	7	27.917	A B C	0.000 0.000 0.000	3.570 7.270 7.270	2.500	70.03	0.000	0.000
T3 100.00- 80.00	90.00	1.332	7	34.863	A B C	0.000 0.000 0.000	4.588 8.288 8.288	3.125	34.39	0.000	0.000
T4 80.00-60.00	70.00	1.24	6	42.050	A B C	0.000 0.000 0.000	6.567 10.267 10.267	4.167	37.71	0.000	0.000
T5 60.00-40.00	50.00	1.126	6	49.063	A B C	0.000 0.000 0.000	7.528 11.228 11.228	4.792	63.45	0.000	0.000
T6 40.00-20.00	30.00	1	5	74.171	A B C	6.311 6.311 6.311	7.930 11.630 11.630	4.902	40.58	0.000	0.000
T7 20.00-0.00	10.00	1	.5	114.796	A	8.248	7.930	7.930	42.68	0.000	0.000

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Section Elevation	z	K <sub>Z</sub>	q <sub>z</sub>	A <sub>G</sub>	F <sub>a</sub>	A <sub>F</sub>	A <sub>R</sub>	A <sub>leg</sub>	Leg %	C <sub>A</sub> A <sub>In</sub> Face ft <sup>2</sup>	C <sub>A</sub> A <sub>Out</sub> Face ft <sup>2</sup>
ft	ft		psf	ft <sup>2</sup>		ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>			
					B	8.248	9.410		44.91	0.000	0.000
					C	8.248	9.410		44.91	0.000	0.000

### Tower Pressure - With Ice

$$G_H = 1.138$$

Section Elevation	z	K <sub>Z</sub>	q <sub>z</sub>	t <sub>Z</sub>	A <sub>G</sub>	F <sub>a</sub>	A <sub>F</sub>	A <sub>R</sub>	A <sub>leg</sub>	Leg %	C <sub>A</sub> A <sub>In</sub> Face ft <sup>2</sup>	C <sub>A</sub> A <sub>Out</sub> Face ft <sup>2</sup>
ft	ft		psf	in	ft <sup>2</sup>		ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>			
T1 140.00-120.00	130.00	1.48	6	0.5000	25.938	A	0.000	8.833	5.208	58.96	0.000	0.000
						B	0.000	14.460				
						C	0.000	14.460				
T2 120.00-100.00	110.00	1.411	5	0.5000	29.584	A	0.000	9.756	5.834	59.79	0.000	0.000
						B	0.000	16.790				
						C	0.000	16.790				
T3 100.00-80.00	90.00	1.332	5	0.5000	36.529	A	0.000	11.265	6.459	57.33	0.000	0.000
						B	0.000	18.298				
						C	0.000	18.298				
T4 80.00-60.00	70.00	1.24	5	0.5000	43.717	A	0.000	13.741	7.500	54.58	0.000	0.000
						B	0.000	20.775				
						C	0.000	20.775				
T5 60.00-40.00	50.00	1.126	4	0.5000	50.730	A	0.000	15.240	8.125	53.32	0.000	0.000
						B	0.000	22.273				
						C	0.000	22.273				
T6 40.00-20.00	30.00	1	4	0.5000	75.840	A	6.311	15.477	11.269	51.72	0.000	0.000
						B	6.311	22.510				
						C	6.311	22.510				
T7 20.00-0.00	10.00	1	4	0.5000	116.465	A	8.248	16.768	11.270	45.05	0.000	0.000
						B	8.248	19.582				
						C	8.248	19.582				

### Tower Pressure - Service

$$G_H = 1.138$$

Section Elevation	z	K <sub>Z</sub>	q <sub>z</sub>	A <sub>G</sub>	F <sub>a</sub>	A <sub>F</sub>	A <sub>R</sub>	A <sub>leg</sub>	Leg %	C <sub>A</sub> A <sub>In</sub> Face ft <sup>2</sup>	C <sub>A</sub> A <sub>Out</sub> Face ft <sup>2</sup>
ft	ft		psf	ft <sup>2</sup>		ft <sup>2</sup>	ft <sup>2</sup>	ft <sup>2</sup>			
T1 140.00-120.00	130.00	1.48	9	24.272	A	0.000	2.864	1.875	65.48	0.000	0.000
					B	0.000	5.824				
					C	0.000	5.824				
T2 120.00-100.00	110.00	1.411	9	27.917	A	0.000	3.570	2.500	70.03	0.000	0.000
					B	0.000	7.270				
					C	0.000	7.270				
T3 100.00-80.00	90.00	1.332	9	34.863	A	0.000	4.588	3.125	68.12	0.000	0.000
					B	0.000	8.288				
					C	0.000	8.288				
T4 80.00-60.00	70.00	1.24	8	42.050	A	0.000	6.567	4.167	63.45	0.000	0.000
					B	0.000	10.267				

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Section Elevation	z	Kz	qz	AG	Fa ce	Af	Ar	Aleg	Leg %	CAA In Face ft <sup>2</sup>	CAA Out Face ft <sup>2</sup>
ft	ft		psf	ft <sup>2</sup>		ft <sup>2</sup>	ft <sup>2</sup>				
T5 60.00-40.00	50.00	1.126	7	49.063	C	0.000	10.267		40.58	0.000	0.000
					A	0.000	7.528	4.792	63.65	0.000	0.000
					B	0.000	11.228		42.68	0.000	0.000
					C	0.000	11.228		42.68	0.000	0.000
T6 40.00-20.00	30.00	1	6	74.171	A	6.311	7.930	7.930	55.68	0.000	0.000
					B	6.311	11.630		44.20	0.000	0.000
					C	6.311	11.630		44.20	0.000	0.000
T7 20.00-0.00	10.00	1	6	114.796	A	8.248	7.930	7.930	49.02	0.000	0.000
					B	8.248	9.410		44.91	0.000	0.000
					C	8.248	9.410		44.91	0.000	0.000

### Tower Forces - No Ice - Wind Normal To Face

Section Elevation	Add Weight	Self Weight	Fa ce	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
T1 140.00-120.00	0.02	0.09	A	0.118	2.893	0.577	1	1	1.653	0.08	3.76	C
			B	0.24	2.468	0.599	1	1		3.490		
			C	0.24	2.468	0.599	1	1		3.490		
T2 120.00-100.00	0.02	0.13	A	0.128	2.855	0.578	1	1	2.065	0.09	4.40	C
			B	0.26	2.407	0.605	1	1		4.395		
			C	0.26	2.407	0.605	1	1		4.395		
T3 100.00-80.00	0.02	0.21	A	0.132	2.84	0.579	1	1	2.656	0.10	4.83	C
			B	0.238	2.475	0.599	1	1		4.963		
			C	0.238	2.475	0.599	1	1		4.963		
T4 80.00-60.00	0.02	0.41	A	0.156	2.749	0.582	1	1	3.825	0.11	5.53	C
			B	0.244	2.455	0.6	1	1		6.164		
			C	0.244	2.455	0.6	1	1		6.164		
T5 60.00-40.00	0.02	0.51	A	0.153	2.759	0.582	1	1	4.381	0.11	5.57	C
			B	0.229	2.502	0.597	1	1		6.700		
			C	0.229	2.502	0.597	1	1		6.700		
T6 40.00-20.00	0.02	0.42	A	0.192	2.623	0.589	1	1	10.980	0.19	9.65	C
			B	0.242	2.462	0.6	1	1		13.287		
			C	0.242	2.462	0.6	1	1		13.287		
T7 20.00-0.00	0.01	0.48	A	0.141	2.805	0.58	1	1	12.849	0.22	11.16	C
			B	0.154	2.757	0.582	1	1		13.726		
			C	0.154	2.757	0.582	1	1		13.726		
Sum Weight:	0.13	2.26						OTM	49.49 kip-ft	0.90		

### Tower Forces - No Ice - Wind 60 To Face

Section Elevation	Add Weight	Self Weight	Fa ce	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
T1 140.00-120.00	0.02	0.09	A	0.118	2.893	0.577	0.8	1	1.653	0.08	3.76	C
			B	0.24	2.468	0.599	0.8	1		3.490		
			C	0.24	2.468	0.599	0.8	1		3.490		
T2 120.00-100.00	0.02	0.13	A	0.128	2.855	0.578	0.8	1	2.065	0.09	4.40	C
			B	0.26	2.407	0.605	0.8	1		4.395		
			C	0.26	2.407	0.605	0.8	1		4.395		

<b>RISATower</b>	<b>Job</b> 140-ft ROHN SSV Woodstock - Exist	<b>Page</b> 10 of 26
<b>CENTEK Engineering, Inc.</b> 63-2 N Branford Rd Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	<b>Project</b> 87 West Quasset Road	<b>Date</b> 16:18:22 09/02/11
	<b>Client</b> Verizon Wireless	<b>Designed by</b> Jrm

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
T3 100.00-80.00	0.02	0.21	A	0.132	2.84	0.579	0.8	1	2.656	0.10	4.83	C
			B	0.238	2.475	0.599	0.8	1	4.963			
			C	0.238	2.475	0.599	0.8	1	4.963			
T4 80.00-60.00	0.02	0.41	A	0.156	2.749	0.582	0.8	1	3.825	0.11	5.53	C
			B	0.244	2.455	0.6	0.8	1	6.164			
			C	0.244	2.455	0.6	0.8	1	6.164			
T5 60.00-40.00	0.02	0.51	A	0.153	2.759	0.582	0.8	1	4.381	0.11	5.57	C
			B	0.229	2.502	0.597	0.8	1	6.700			
			C	0.229	2.502	0.597	0.8	1	6.700			
T6 40.00-20.00	0.02	0.42	A	0.192	2.623	0.589	0.8	1	9.718	0.17	8.73	C
			B	0.242	2.462	0.6	0.8	1	12.025			
			C	0.242	2.462	0.6	0.8	1	12.025			
T7 20.00-0.00	0.01	0.48	A	0.141	2.805	0.58	0.8	1	11.199	0.20	9.82	C
			B	0.154	2.757	0.582	0.8	1	12.076			
			C	0.154	2.757	0.582	0.8	1	12.076			
Sum Weight:	0.13	2.26						OTM	48.67 kip-ft	0.85		

## Tower Forces - No Ice - Wind 90 To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
ft	K	K							ft <sup>2</sup>	K	plf	
T1 140.00-120.00	0.02	0.09	A	0.118	2.893	0.577	0.85	1	1.653	0.08	3.76	C
			B	0.24	2.468	0.599	0.85	1	3.490			
			C	0.24	2.468	0.599	0.85	1	3.490			
T2 120.00-100.00	0.02	0.13	A	0.128	2.855	0.578	0.85	1	2.065	0.09	4.40	C
			B	0.26	2.407	0.605	0.85	1	4.395			
			C	0.26	2.407	0.605	0.85	1	4.395			
T3 100.00-80.00	0.02	0.21	A	0.132	2.84	0.579	0.85	1	2.656	0.10	4.83	C
			B	0.238	2.475	0.599	0.85	1	4.963			
			C	0.238	2.475	0.599	0.85	1	4.963			
T4 80.00-60.00	0.02	0.41	A	0.156	2.749	0.582	0.85	1	3.825	0.11	5.53	C
			B	0.244	2.455	0.6	0.85	1	6.164			
			C	0.244	2.455	0.6	0.85	1	6.164			
T5 60.00-40.00	0.02	0.51	A	0.153	2.759	0.582	0.85	1	4.381	0.11	5.57	C
			B	0.229	2.502	0.597	0.85	1	6.700			
			C	0.229	2.502	0.597	0.85	1	6.700			
T6 40.00-20.00	0.02	0.42	A	0.192	2.623	0.589	0.85	1	10.034	0.18	8.96	C
			B	0.242	2.462	0.6	0.85	1	12.341			
			C	0.242	2.462	0.6	0.85	1	12.341			
T7 20.00-0.00	0.01	0.48	A	0.141	2.805	0.58	0.85	1	11.612	0.20	10.16	C
			B	0.154	2.757	0.582	0.85	1	12.489			
			C	0.154	2.757	0.582	0.85	1	12.489			
Sum Weight:	0.13	2.26						OTM	48.87 kip-ft	0.86		

## Tower Forces - With Ice - Wind Normal To Face

**RISATower**

**CENTEK Engineering, Inc.**  
 63-2 N Branford Rd  
 Branford, CT 06405  
 Phone: (203) 488-0580  
 FAX: (203) 488-8587

	Job	140-ft ROHN SSV Woodstock - Exist	Page	11 of 26
	Project	87 West Quasset Road	Date	16:18:22 09/02/11
	Client	Verizon Wireless	Designed by	Jrm

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
T1 140.00-120.00	0.05	0.18	A	0.341	2.194	0.629	1	1	5.557	0.13	6.33	C
			B	0.557	1.837	0.728	1	1	10.534			
			C	0.557	1.837	0.728	1	1	10.534			
T2 120.00-100.00	0.06	0.24	A	0.33	2.22	0.625	1	1	6.102	0.14	7.03	C
			B	0.568	1.828	0.734	1	1	12.328			
			C	0.568	1.828	0.734	1	1	12.328			
T3 100.00-80.00	0.06	0.33	A	0.308	2.274	0.619	1	1	6.968	0.14	7.15	C
			B	0.501	1.899	0.698	1	1	12.772			
			C	0.501	1.899	0.698	1	1	12.772			
T4 80.00-60.00	0.06	0.58	A	0.314	2.259	0.62	1	1	8.525	0.15	7.55	C
			B	0.475	1.934	0.685	1	1	14.234			
			C	0.475	1.934	0.685	1	1	14.234			
T5 60.00-40.00	0.06	0.70	A	0.3	2.295	0.616	1	1	9.388	0.15	7.39	C
			B	0.439	1.992	0.668	1	1	14.885			
			C	0.439	1.992	0.668	1	1	14.885			
T6 40.00-20.00	0.06	0.78	A	0.287	2.33	0.612	1	1	15.784	0.19	9.69	C
			B	0.38	2.105	0.644	1	1	20.800			
			C	0.38	2.105	0.644	1	1	20.800			
T7 20.00-0.00	0.02	0.90	A	0.215	2.547	0.594	1	1	18.201	0.22	10.92	C
			B	0.239	2.471	0.599	1	1	19.980			
			C	0.239	2.471	0.599	1	1	19.980			
Sum Weight:	0.38	3.71						OTM	70.75 kip-ft	1.12		

**Tower Forces - With Ice - Wind 60 To Face**

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
T1 140.00-120.00	0.05	0.18	A	0.341	2.194	0.629	0.8	1	5.557	0.13	6.33	C
			B	0.557	1.837	0.728	0.8	1	10.534			
			C	0.557	1.837	0.728	0.8	1	10.534			
T2 120.00-100.00	0.06	0.24	A	0.33	2.22	0.625	0.8	1	6.102	0.14	7.03	C
			B	0.568	1.828	0.734	0.8	1	12.328			
			C	0.568	1.828	0.734	0.8	1	12.328			
T3 100.00-80.00	0.06	0.33	A	0.308	2.274	0.619	0.8	1	6.968	0.14	7.15	C
			B	0.501	1.899	0.698	0.8	1	12.772			
			C	0.501	1.899	0.698	0.8	1	12.772			
T4 80.00-60.00	0.06	0.58	A	0.314	2.259	0.62	0.8	1	8.525	0.15	7.55	C
			B	0.475	1.934	0.685	0.8	1	14.234			
			C	0.475	1.934	0.685	0.8	1	14.234			
T5 60.00-40.00	0.06	0.70	A	0.3	2.295	0.616	0.8	1	9.388	0.15	7.39	C
			B	0.439	1.992	0.668	0.8	1	14.885			
			C	0.439	1.992	0.668	0.8	1	14.885			
T6 40.00-20.00	0.06	0.78	A	0.287	2.33	0.612	0.8	1	14.522	0.18	9.10	C
			B	0.38	2.105	0.644	0.8	1	19.537			
			C	0.38	2.105	0.644	0.8	1	19.537			
T7 20.00-0.00	0.02	0.90	A	0.215	2.547	0.594	0.8	1	16.551	0.20	10.02	C
			B	0.239	2.471	0.599	0.8	1	18.330			
			C	0.239	2.471	0.599	0.8	1	18.330			
Sum Weight:	0.38	3.71						OTM	70.22 kip-ft	1.09		

<b>RISA Tower</b>  <b>CENTEK Engineering, Inc.</b> 63-2 N Branford Rd Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job 140-ft ROHN SSV Woodstock - Exist										Page 12 of 26
	Project 87 West Quasset Road										Date 16:18:22 09/02/11
	Client Verizon Wireless										Designed by Jrm

### Tower Forces - With Ice - Wind 90 To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
T1 140.00- 120.00	0.05	0.18	A	0.341	2.194	0.629	0.85	1	5.557	0.13	6.33	C
			B	0.557	1.837	0.728	0.85	1	10.534			
			C	0.557	1.837	0.728	0.85	1	10.534			
T2 120.00- 100.00	0.06	0.24	A	0.33	2.22	0.625	0.85	1	6.102	0.14	7.03	C
			B	0.568	1.828	0.734	0.85	1	12.328			
			C	0.568	1.828	0.734	0.85	1	12.328			
T3 100.00- 80.00	0.06	0.33	A	0.308	2.274	0.619	0.85	1	6.968	0.14	7.15	C
			B	0.501	1.899	0.698	0.85	1	12.772			
			C	0.501	1.899	0.698	0.85	1	12.772			
T4 80.00- 60.00	0.06	0.58	A	0.314	2.259	0.62	0.85	1	8.525	0.15	7.55	C
			B	0.475	1.934	0.685	0.85	1	14.234			
			C	0.475	1.934	0.685	0.85	1	14.234			
T5 60.00- 40.00	0.06	0.70	A	0.3	2.295	0.616	0.85	1	9.388	0.15	7.39	C
			B	0.439	1.992	0.668	0.85	1	14.885			
			C	0.439	1.992	0.668	0.85	1	14.885			
T6 40.00- 20.00	0.06	0.78	A	0.287	2.33	0.612	0.85	1	14.838	0.18	9.25	C
			B	0.38	2.105	0.644	0.85	1	19.853			
			C	0.38	2.105	0.644	0.85	1	19.853			
T7 20.00-0.00	0.02	0.90	A	0.215	2.547	0.594	0.85	1	16.964	0.20	10.25	C
			B	0.239	2.471	0.599	0.85	1	18.743			
			C	0.239	2.471	0.599	0.85	1	18.743			
Sum Weight:	0.38	3.71						OTM	70.35 kip-ft	1.10		

### Tower Forces - Service - Wind Normal To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
T1 140.00- 120.00	0.02	0.09	A	0.118	2.893	0.577	1	1	1.653	0.09	4.64	C
			B	0.24	2.468	0.599	1	1	3.490			
			C	0.24	2.468	0.599	1	1	3.490			
T2 120.00- 100.00	0.02	0.13	A	0.128	2.855	0.578	1	1	2.065	0.11	5.43	C
			B	0.26	2.407	0.605	1	1	4.395			
			C	0.26	2.407	0.605	1	1	4.395			
T3 100.00- 80.00	0.02	0.21	A	0.132	2.84	0.579	1	1	2.656	0.12	5.96	C
			B	0.238	2.475	0.599	1	1	4.963			
			C	0.238	2.475	0.599	1	1	4.963			
T4 80.00- 60.00	0.02	0.41	A	0.156	2.749	0.582	1	1	3.825	0.14	6.83	C
			B	0.244	2.455	0.6	1	1	6.164			
			C	0.244	2.455	0.6	1	1	6.164			
T5 60.00- 40.00	0.02	0.51	A	0.153	2.759	0.582	1	1	4.381	0.14	6.88	C
			B	0.229	2.502	0.597	1	1	6.700			
			C	0.229	2.502	0.597	1	1	6.700			
T6 40.00- 20.00	0.02	0.42	A	0.192	2.623	0.589	1	1	10.980	0.24	11.91	C
			B	0.242	2.462	0.6	1	1	13.287			
			C	0.242	2.462	0.6	1	1	13.287			
T7 20.00-0.00	0.01	0.48	A	0.141	2.805	0.58	1	1	12.849	0.28	13.78	C
			B	0.154	2.757	0.582	1	1	13.726			
			C	0.154	2.757	0.582	1	1	13.726			

<b>RISATower</b>  <b>CENTEK Engineering, Inc.</b> 63-2 N Branford Rd Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job 140-ft ROHN SSV Woodstock - Exist										Page 13 of 26	
	Project 87 West Quasset Road										Date 16:18:22 09/02/11	
	Client Verizon Wireless										Designed by Jrm	

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F K	w plf	Ctrl. Face
Sum Weight:	0.13	2.26						OTM	61.09 kip-ft	1.11		

### Tower Forces - Service - Wind 60 To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F K	w plf	Ctrl. Face
T1 140.00-120.00	0.02	0.09	A B C	0.118 0.24 0.24	2.893 2.468 2.468	0.577 0.599 0.599	0.8 0.8 0.8	1 1 1	1.653 3.490 3.490	0.09	4.64	C
T2 120.00-100.00	0.02	0.13	A B C	0.128 0.26 0.26	2.855 2.407 2.407	0.578 0.605 0.605	0.8 0.8 0.8	1 1 1	2.065 4.395 4.395	0.11	5.43	C
T3 100.00-80.00	0.02	0.21	A B C	0.132 0.238 0.238	2.84 2.475 2.475	0.579 0.599 0.599	0.8 0.8 0.8	1 1 1	2.656 4.963 4.963	0.12	5.96	C
T4 80.00-60.00	0.02	0.41	A B C	0.156 0.244 0.244	2.749 2.455 2.455	0.582 0.6 0.6	0.8 0.8 0.8	1 1 1	3.825 6.164 6.164	0.14	6.83	C
T5 60.00-40.00	0.02	0.51	A B C	0.153 0.229 0.229	2.759 2.502 2.502	0.582 0.597 0.597	0.8 0.8 0.8	1 1 1	4.381 6.700 6.700	0.14	6.88	C
T6 40.00-20.00	0.02	0.42	A B C	0.192 0.242 0.242	2.623 2.462 2.462	0.589 0.6 0.6	0.8 0.8 0.8	1 1 1	9.718 12.025 12.025	0.22	10.78	C
T7 20.00-0.00	0.01	0.48	A B C	0.141 0.154 0.154	2.805 2.757 2.757	0.58 0.582 0.582	0.8 0.8 0.8	1 1 1	11.199 12.076 12.076	0.24	12.13	C
Sum Weight:	0.13	2.26						OTM	60.08 kip-ft	1.05		

### Tower Forces - Service - Wind 90 To Face

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub> ft <sup>2</sup>	F K	w plf	Ctrl. Face
T1 140.00-120.00	0.02	0.09	A B C	0.118 0.24 0.24	2.893 2.468 2.468	0.577 0.599 0.599	0.85 0.85 0.85	1 1 1	1.653 3.490 3.490	0.09	4.64	C
T2 120.00-100.00	0.02	0.13	A B C	0.128 0.26 0.26	2.855 2.407 2.407	0.578 0.605 0.605	0.85 0.85 0.85	1 1 1	2.065 4.395 4.395	0.11	5.43	C
T3 100.00-80.00	0.02	0.21	A B C	0.132 0.238 0.238	2.84 2.475 2.475	0.579 0.599 0.599	0.85 0.85 0.85	1 1 1	2.656 4.963 4.963	0.12	5.96	C
T4 80.00-60.00	0.02	0.41	A B C	0.156 0.244 0.244	2.749 2.455 2.455	0.582 0.6 0.6	0.85 0.85 0.85	1 1 1	3.825 6.164 6.164	0.14	6.83	C

<b>RISA Tower</b>  <b>CENTEK Engineering, Inc.</b> 63-2 N Branford Rd Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job	140-ft ROHN SSV Woodstock - Exist	Page
	Project	87 West Quasset Road	14 of 26
	Client	Verizon Wireless	Date 16:18:22 09/02/11 Designed by Jrm

Section Elevation ft	Add Weight K	Self Weight K	F a c e	e	C <sub>F</sub>	R <sub>R</sub>	D <sub>F</sub>	D <sub>R</sub>	A <sub>E</sub>	F	w	Ctrl. Face
									ft <sup>2</sup>	K	plf	
T5 60.00-40.00	0.02	0.51	A B C	0.153 0.229 0.229	2.759 2.502 2.502	0.582 0.597 0.597	0.85 0.85 0.85	1 1 1	4.381 6.700 6.700	0.14	6.88	C
T6 40.00-20.00	0.02	0.42	A B C	0.192 0.242 0.242	2.623 2.462 2.462	0.589 0.6 0.6	0.85 0.85 0.85	1 1 1	10.034 12.341 12.341	0.22	11.07	C
T7 20.00-0.00	0.01	0.48	A B C	0.141 0.154 0.154	2.805 2.757 2.757	0.58 0.582 0.582	0.85 0.85 0.85	1 1 1	11.612 12.489 12.489	0.25	12.54	C
Sum Weight:	0.13	2.26						OTM	60.34 kip-ft		1.07	

### Force Totals

Load Case	Vertical Forces K	Sum of Forces X K	Sum of Forces Z K	Sum of Overturning Moments, M <sub>x</sub> kip-ft	Sum of Overturning Moments, M <sub>z</sub> kip-ft	Sum of Torques kip-ft
Leg Weight	1.33					
Bracing Weight	0.93					
Total Member Self-Weight	2.26			0.55	-0.96	
Total Weight	2.59			0.55	-0.96	
Wind 0 deg - No Ice		0.00	-1.01	-63.59	-0.96	0.58
Wind 30 deg - No Ice		0.49	-0.84	-54.47	-32.73	0.67
Wind 60 deg - No Ice		0.83	-0.48	-31.11	-55.81	0.58
Wind 90 deg - No Ice		0.97	0.00	0.55	-64.49	0.34
Wind 120 deg - No Ice		0.87	0.50	32.63	-56.51	0.00
Wind 150 deg - No Ice		0.49	0.84	55.58	-32.73	-0.34
Wind 180 deg - No Ice		0.00	0.96	63.88	-0.96	-0.58
Wind 210 deg - No Ice		-0.49	0.84	55.58	30.81	-0.67
Wind 240 deg - No Ice		-0.87	0.50	32.63	54.59	-0.58
Wind 270 deg - No Ice		-0.97	0.00	0.55	62.57	-0.34
Wind 300 deg - No Ice		-0.83	-0.48	-31.11	53.88	0.00
Wind 330 deg - No Ice		-0.49	-0.84	-54.47	30.81	0.34
Member Ice	1.45					
Total Weight Ice	4.35			0.89	-1.55	
Wind 0 deg - Ice		0.00	-1.23	-84.69	-1.55	0.61
Wind 30 deg - Ice		0.60	-1.05	-72.87	44.13	0.71
Wind 60 deg - Ice		1.04	-0.60	-41.63	-75.20	0.61
Wind 90 deg - Ice		1.21	0.00	0.89	-86.72	0.35
Wind 120 deg - Ice		1.07	0.62	43.68	-75.66	0.00
Wind 150 deg - Ice		0.60	1.05	74.66	-44.13	-0.35
Wind 180 deg - Ice		0.00	1.20	85.94	-1.55	-0.61
Wind 210 deg - Ice		-0.60	1.05	74.66	41.04	-0.71
Wind 240 deg - Ice		-1.07	0.62	43.68	72.57	-0.61
Wind 270 deg - Ice		-1.21	0.00	0.89	83.63	-0.35
Wind 300 deg - Ice		-1.04	-0.60	-41.63	72.11	0.00
Wind 330 deg - Ice		-0.60	-1.05	-72.87	41.04	0.35
Total Weight	2.59			0.55	-0.96	
Wind 0 deg - Service		0.00	-1.24	-78.73	-0.81	0.72
Wind 30 deg - Service		0.60	-1.04	-67.46	-40.03	0.83
Wind 60 deg - Service		1.03	-0.59	-38.62	-68.52	0.72
Wind 90 deg - Service		1.20	0.00	0.47	-79.25	0.41
Wind 120 deg - Service		1.08	0.62	40.07	-69.40	0.00
Wind 150 deg - Service		0.60	1.04	68.40	-40.03	-0.41
Wind 180 deg - Service		0.00	1.19	78.65	-0.81	-0.72

<b>RISA Tower</b>  <b>CENTEK Engineering, Inc.</b> 63-2 N Branford Rd Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	<b>Job</b>	140-ft ROHN SSV Woodstock - Exist	<b>Page</b>	15 of 26
	<b>Project</b>	87 West Quasset Road	<b>Date</b>	16:18:22 09/02/11
	<b>Client</b>	Verizon Wireless	<b>Designed by</b>	Jrm

Load Case	Vertical Forces K	Sum of Forces X K	Sum of Forces Z K	Sum of Overturning Moments, $M_x$ kip-ft	Sum of Overturning Moments, $M_z$ kip-ft	Sum of Torques kip-ft
Wind 210 deg - Service		-0.60	1.04	68.40	38.41	-0.83
Wind 240 deg - Service		-1.08	0.62	40.07	67.77	-0.72
Wind 270 deg - Service		-1.20	0.00	0.47	77.62	-0.41
Wind 300 deg - Service		-1.03	-0.59	-38.62	66.90	0.00
Wind 330 deg - Service		-0.60	-1.04	-67.46	38.41	0.41

### Load Combinations

Comb. No.	Description
1	Dead Only
2	Dead+Wind 0 deg - No Ice
3	Dead+Wind 30 deg - No Ice
4	Dead+Wind 60 deg - No Ice
5	Dead+Wind 90 deg - No Ice
6	Dead+Wind 120 deg - No Ice
7	Dead+Wind 150 deg - No Ice
8	Dead+Wind 180 deg - No Ice
9	Dead+Wind 210 deg - No Ice
10	Dead+Wind 240 deg - No Ice
11	Dead+Wind 270 deg - No Ice
12	Dead+Wind 300 deg - No Ice
13	Dead+Wind 330 deg - No Ice
14	Dead+Ice+Temp
15	Dead+Wind 0 deg+Ice+Temp
16	Dead+Wind 30 deg+Ice+Temp
17	Dead+Wind 60 deg+Ice+Temp
18	Dead+Wind 90 deg+Ice+Temp
19	Dead+Wind 120 deg+Ice+Temp
20	Dead+Wind 150 deg+Ice+Temp
21	Dead+Wind 180 deg+Ice+Temp
22	Dead+Wind 210 deg+Ice+Temp
23	Dead+Wind 240 deg+Ice+Temp
24	Dead+Wind 270 deg+Ice+Temp
25	Dead+Wind 300 deg+Ice+Temp
26	Dead+Wind 330 deg+Ice+Temp
27	Dead+Wind 0 deg - Service
28	Dead+Wind 30 deg - Service
29	Dead+Wind 60 deg - Service
30	Dead+Wind 90 deg - Service
31	Dead+Wind 120 deg - Service
32	Dead+Wind 150 deg - Service
33	Dead+Wind 180 deg - Service
34	Dead+Wind 210 deg - Service
35	Dead+Wind 240 deg - Service
36	Dead+Wind 270 deg - Service
37	Dead+Wind 300 deg - Service
38	Dead+Wind 330 deg - Service

### Maximum Member Forces

**RISA Tower**

**CENTEK Engineering, Inc.**  
 63-2 N Branford Rd  
 Branford, CT 06405  
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 FAX: (203) 488-8587

Job	140-ft ROHN SSV Woodstock - Exist	Page	16 of 26
Project	87 West Quasset Road	Date	16:18:22 09/02/11
Client	Verizon Wireless	Designed by	Jrm

Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Force K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
T1	140 - 120	Leg	Max Tension	21	4.07	-0.00	-0.00
			Max. Compression	19	-4.68	-0.01	-0.00
			Max. Mx	22	-0.12	-0.06	0.03
			Max. My	21	-1.49	0.03	0.07
			Max. Vy	23	-0.78	0.01	-0.00
		Diagonal	Max. Vx	22	-0.83	0.00	0.01
			Max Tension	28	1.10	0.00	0.00
			Max. Compression	34	-1.09	0.00	0.00
			Max. Mx	20	0.17	0.00	0.00
			Max. My	22	-0.48	0.00	0.00
		Top Girt	Max. Vy	20	-0.00	0.00	0.00
			Max. Vx	22	0.00	0.00	0.00
			Max Tension	16	0.51	0.00	0.00
			Max. Compression	34	-0.07	0.00	0.00
			Max. Mx	14	0.44	0.00	0.00
		Bottom Girt	Max. My	22	0.38	0.00	-0.00
			Max. Vy	14	-0.00	0.00	0.00
			Max. Vx	22	0.00	0.00	0.00
			Max Tension	34	-0.52	0.00	0.00
			Max. Compression	28	-0.46	0.00	0.00
T2	120 - 100	Leg	Max. Mx	14	0.00	0.00	0.00
			Max. My	22	0.22	0.00	-0.00
			Max. Vy	14	-0.00	0.00	0.00
			Max. Vx	22	0.00	0.00	0.00
		Pole Antenna	Max Tension	21	0.48	-0.00	-0.01
			Max. Compression	2	-0.00	0.00	-0.00
			Max. Mx	36	0.00	0.01	-0.00
			Max. My	27	0.00	-0.00	0.01
			Max. Vy	36	-0.01	0.01	-0.00
		Diagonal	Max. Vx	27	-0.01	-0.00	0.01
			Max. Torque	21			-0.00
			Max Tension	21	8.09	-0.00	0.00
			Max. Compression	19	-8.93	0.01	-0.00
			Max. Mx	21	3.33	-0.02	0.04
T3	100 - 80	Leg	Max. My	34	-1.20	-0.01	0.06
			Max. Vy	28	-0.16	0.02	-0.05
			Max. Vx	34	-0.45	-0.01	0.06
		Top Girt	Max Tension	34	1.16	0.00	0.00
			Max. Compression	28	-1.14	0.00	0.00
			Max. Mx	18	0.54	0.00	0.00
			Max. My	16	-1.01	0.00	-0.00
			Max. Vy	18	-0.00	0.00	0.00
		Bottom Girt	Max. Vx	16	0.00	0.00	0.00
			Max Tension	28	0.48	0.00	0.00
			Max. Compression	34	-0.57	0.00	0.00
			Max. Mx	14	-0.00	0.00	0.00
			Max. My	22	-0.25	0.00	-0.00
		Leg	Max. Vy	14	-0.00	0.00	0.00
			Max. Vx	22	0.00	0.00	0.00
			Max Tension	34	0.37	0.00	0.00
			Max. Compression	28	-0.30	0.00	0.00
			Max. Mx	14	0.00	0.00	0.00
			Max. My	22	0.13	0.00	-0.00
			Max. Vy	14	-0.00	0.00	0.00
			Max. Vx	22	0.00	0.00	0.00

**RISATower**

**CENTEK Engineering, Inc.**  
 63-2 N Branford Rd  
 Branford, CT 06405  
 Phone: (203) 488-0580  
 FAX: (203) 488-8587

	<b>Job</b>	140-ft ROHN SSV Woodstock - Exist	<b>Page</b>	17 of 26
	<b>Project</b>	87 West Quasset Road	<b>Date</b>	16:18:22 09/02/11
	<b>Client</b>	Verizon Wireless	<b>Designed by</b>	Jrm

Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Force K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
T4	80 - 60	Leg	Diagonal	Max Tension	34	0.87	0.00
				Max. Compression	28	-0.87	0.00
				Max. Mx	18	0.52	0.00
				Max. My	16	-0.80	0.00
				Max. Vy	18	-0.00	0.00
				Max. Vx	16	0.00	0.00
			Top Girt	Max Tension	28	0.33	0.00
				Max. Compression	34	-0.40	0.00
				Max. Mx	14	-0.00	0.00
				Max. My	22	-0.15	0.00
T5	60 - 40	Leg	Bottom Girt	Max Tension	22	0.00	0.00
				Max. Compression	34	0.24	0.00
				Max. Mx	14	0.00	0.00
				Max. My	22	0.07	0.00
				Max. Vy	14	-0.00	0.00
				Max. Vx	22	0.00	0.00
			Diagonal	Max Tension	21	16.85	-0.01
				Max. Compression	19	-18.41	0.02
				Max. Mx	23	-12.13	0.04
				Max. My	34	-0.98	0.02
T4	80 - 60	Top Girt		Max. Vy	23	-0.33	0.02
				Max. Vx	34	-0.32	0.02
			Bottom Girt	Max Tension	35	0.75	0.00
				Max. Compression	27	-0.76	0.00
				Max. Mx	18	0.54	0.00
				Max. My	17	-0.47	0.00
				Max. Vy	18	0.00	0.00
				Max. Vx	17	0.00	0.00
			Diagonal	Max Tension	28	0.23	0.00
				Max. Compression	34	-0.26	0.00
T5	60 - 40	Top Girt		Max. Mx	14	-0.00	0.00
				Max. My	22	-0.09	0.00
				Max. Vy	14	-0.00	0.00
				Max. Vx	22	0.00	0.00
			Bottom Girt	Max Tension	34	0.19	0.00
				Max. Compression	28	-0.17	0.00
				Max. Mx	14	0.00	0.00
				Max. My	22	0.04	0.00
				Max. Vy	14	-0.00	0.00
				Max. Vx	22	0.00	0.00
T4	80 - 60	Bottom Girt	Diagonal	Max Tension	21	21.37	-0.01
				Max. Compression	19	-23.42	0.08
				Max. Mx	21	21.35	-0.08
				Max. My	28	-0.74	-0.03
				Max. Vy	23	-0.33	0.05
				Max. Vx	34	-0.34	0.01
			Top Girt	Max Tension	35	0.69	0.00
				Max. Compression	27	-0.71	0.00
				Max. Mx	18	0.50	0.00
				Max. My	17	-0.40	0.00
T5	60 - 40	Top Girt		Max. Vy	18	-0.00	0.00
				Max. Vx	17	0.00	0.00
			Bottom Girt	Max Tension	27	0.16	0.00
				Max. Compression	35	-0.18	0.00
				Max. Mx	14	-0.00	0.00
				Max. My	22	-0.04	0.00
				Max. Vy	14	0.00	0.00
				Max. Vx	22	-0.00	0.00
			Bottom Girt	Max Tension	22	0.36	0.00

<b>RISATower</b>  <b>CENTEK Engineering, Inc.</b> 63-2 N Branford Rd Branford, CT 06405 Phone: (203) 488-0580 FAX: (203) 488-8587	Job	140-ft ROHN SSV Woodstock - Exist	Page
	Project	87 West Quasset Road	Date
	Client	Verizon Wireless	Designed by Jrm

Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Force K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
T6	40 - 20	Leg	Max. Compression	28	-0.34	0.00	0.00
			Max. Mx	14	0.01	0.00	0.00
			Max. Vy	14	-0.00	0.00	0.00
			Max. Vx	22	0.00	0.00	0.00
			Max Tension	17	20.08	-0.08	-0.01
			Max. Compression	19	-21.88	0.02	0.00
		Diagonal	Max. Mx	21	20.06	-0.08	0.02
			Max. My	18	-0.71	-0.00	0.14
			Max. Vy	21	-0.02	-0.06	0.00
			Max. Vx	18	0.04	-0.00	0.14
			Max Tension	17	1.03	0.00	0.00
			Max. Compression	23	-1.15	0.02	-0.00
T7	20 - 0	Leg	Max. Mx	18	0.04	0.02	-0.00
			Max. My	18	-0.62	0.02	-0.01
			Max. Vy	18	-0.01	0.02	-0.00
			Max. Vx	18	0.00	0.02	-0.01
			Max Tension	21	15.62	0.01	0.00
			Max. Compression	19	-18.36	-0.01	-0.00
		Diagonal	Max. Mx	21	14.69	-0.09	0.00
			Max. My	20	-1.01	0.06	-0.05
			Max. Vy	21	-0.04	-0.09	0.00
			Max. Vx	28	0.02	-0.00	-0.05
			Max Tension	16	0.38	0.00	0.00
			Max. Compression	16	-0.38	0.00	0.00

### Maximum Reactions

Location	Condition	Gov. Load Comb.	Vertical K	Horizontal, X K	Horizontal, Z K
Leg C	Max. Vert	23	16.85	0.68	-0.32
	Max. H <sub>x</sub>	35	14.98	0.87	-0.42
	Max. H <sub>z</sub>	18	-12.14	-0.82	0.50
	Min. Vert	17	-14.20	-0.96	0.49
	Min. H <sub>x</sub>	17	-14.20	-0.96	0.49
	Min. H <sub>z</sub>	35	14.98	0.87	-0.42
Leg B	Max. Vert	19	17.35	-0.65	-0.38
	Max. H <sub>x</sub>	25	-13.67	0.92	0.53
	Max. H <sub>z</sub>	25	-13.67	0.92	0.53
	Min. Vert	25	-13.67	0.92	0.53
	Min. H <sub>x</sub>	31	15.27	-0.84	-0.48
	Min. H <sub>z</sub>	31	15.27	-0.84	-0.48
Leg A	Max. Vert	15	16.85	0.06	0.75
	Max. H <sub>x</sub>	17	9.03	0.15	0.27
	Max. H <sub>z</sub>	27	14.98	0.07	0.96
	Min. Vert	21	-14.20	-0.05	-1.08
	Min. H <sub>x</sub>	23	-6.52	-0.14	-0.64
	Min. H <sub>z</sub>	21	-14.20	-0.05	-1.08

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Job	140-ft ROHN SSV Woodstock - Exist	Page	19 of 26
Project	87 West Quasset Road	Date	16:18:22 09/02/11
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## Tower Mast Reaction Summary

Load Combination	Vertical	Shear <sub>x</sub>	Shear <sub>z</sub>	Overspinning Moment, M <sub>x</sub>	Overspinning Moment, M <sub>z</sub>	Torque
	K	K	K	kip-ft	kip-ft	kip-ft
Dead Only	2.59	0.00	0.00	0.59	-1.01	-0.00
Dead+Wind 0 deg - No Ice	2.59	0.00	-1.01	-64.87	-1.04	0.61
Dead+Wind 30 deg - No Ice	2.59	0.49	-0.84	-55.58	-33.43	0.70
Dead+Wind 60 deg - No Ice	2.59	0.83	-0.48	-31.76	-56.97	0.61
Dead+Wind 90 deg - No Ice	2.59	0.97	0.00	0.55	-65.82	0.35
Dead+Wind 120 deg - No Ice	2.59	0.87	0.50	33.29	-57.65	0.00
Dead+Wind 150 deg - No Ice	2.59	0.49	0.84	56.73	-33.39	-0.35
Dead+Wind 180 deg - No Ice	2.59	0.00	0.96	65.22	-0.98	-0.61
Dead+Wind 210 deg - No Ice	2.59	-0.49	0.84	56.75	31.41	-0.71
Dead+Wind 240 deg - No Ice	2.59	-0.87	0.50	33.34	55.65	-0.62
Dead+Wind 270 deg - No Ice	2.59	-0.97	0.00	0.62	63.79	-0.35
Dead+Wind 300 deg - No Ice	2.59	-0.83	-0.48	-31.70	54.91	0.00
Dead+Wind 330 deg - No Ice	2.59	-0.49	-0.84	-55.55	31.36	0.35
Dead+Ice+Temp	4.35	0.00	0.00	0.97	-1.68	-0.00
Dead+Wind 0 deg+Ice+Temp	4.35	0.00	-1.23	-87.54	-1.71	0.67
Dead+Wind 30 deg+Ice+Temp	4.35	0.60	-1.05	-75.36	-45.73	0.77
Dead+Wind 60 deg+Ice+Temp	4.35	1.04	-0.60	-43.07	-77.83	0.66
Dead+Wind 90 deg+Ice+Temp	4.35	1.21	-0.00	0.90	-89.72	0.38
Dead+Wind 120 deg+Ice+Temp	4.35	1.07	0.62	45.18	-78.25	0.00
Dead+Wind 150 deg+Ice+Temp	4.35	0.60	1.05	77.25	-45.66	-0.38
Dead+Wind 180 deg+Ice+Temp	4.35	0.00	1.20	88.95	-1.63	-0.67
Dead+Wind 210 deg+Ice+Temp	4.35	-0.60	1.05	77.29	42.39	-0.78
Dead+Wind 240 deg+Ice+Temp	4.35	-1.07	0.62	45.26	74.94	-0.68
Dead+Wind 270 deg+Ice+Temp	4.35	-1.21	0.00	1.02	86.36	-0.39
Dead+Wind 300 deg+Ice+Temp	4.35	-1.04	-0.60	-42.97	74.43	0.00
Dead+Wind 330 deg+Ice+Temp	4.35	-0.60	-1.05	-75.30	42.31	0.39
Dead+Wind 0 deg - Service	2.59	0.00	-1.24	-80.22	-1.04	0.76
Dead+Wind 30 deg - Service	2.59	0.60	-1.04	-68.76	-41.03	0.86
Dead+Wind 60 deg - Service	2.59	1.03	-0.59	-39.35	-70.08	0.75
Dead+Wind 90 deg - Service	2.59	1.20	0.00	0.54	-81.01	0.43
Dead+Wind 120 deg - Service	2.59	1.08	0.62	40.95	-70.93	0.00
Dead+Wind 150 deg - Service	2.59	0.60	1.04	69.89	-40.98	-0.43
Dead+Wind 180 deg - Service	2.59	0.00	1.19	80.38	-0.97	-0.75
Dead+Wind 210 deg - Service	2.59	-0.60	1.04	69.92	39.02	-0.87
Dead+Wind 240 deg - Service	2.59	-1.08	0.62	41.02	68.94	-0.76
Dead+Wind 270 deg - Service	2.59	-1.20	0.00	0.62	78.98	-0.44
Dead+Wind 300 deg - Service	2.59	-1.03	-0.59	-39.28	68.03	0.00
Dead+Wind 330 deg - Service	2.59	-0.60	-1.04	-68.71	38.96	0.44

## Solution Summary

Load Comb.	Sum of Applied Forces			Sum of Reactions			% Error
	PX K	PY K	PZ K	PX K	PY K	PZ K	
1	0.00	-2.59	0.00	0.00	2.59	0.00	0.000%
2	0.00	-2.59	-1.01	-0.00	2.59	1.01	0.000%
3	0.49	-2.59	-0.84	-0.49	2.59	0.84	0.000%
4	0.83	-2.59	-0.48	-0.83	2.59	0.48	0.000%
5	0.97	-2.59	0.00	-0.97	2.59	0.00	0.000%
6	0.87	-2.59	0.50	-0.87	2.59	-0.50	0.000%
7	0.49	-2.59	0.84	-0.49	2.59	-0.84	0.000%
8	0.00	-2.59	0.96	-0.00	2.59	-0.96	0.000%
9	-0.49	-2.59	0.84	0.49	2.59	-0.84	0.000%
10	-0.87	-2.59	0.50	0.87	2.59	-0.50	0.000%
11	-0.97	-2.59	0.00	0.97	2.59	0.00	0.000%

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Load Comb.	Sum of Applied Forces			Sum of Reactions			% Error
	PX K	PY K	PZ K	PX K	PY K	PZ K	
12	-0.83	-2.59	-0.48	0.83	2.59	0.48	0.000%
13	-0.49	-2.59	-0.84	0.49	2.59	0.84	0.000%
14	0.00	-4.35	0.00	0.00	4.35	0.00	0.000%
15	0.00	4.35	-1.23	-0.00	4.35	1.23	0.000%
16	0.60	4.35	-1.05	-0.60	4.35	1.05	0.000%
17	1.04	4.35	-0.60	-1.04	4.35	0.60	0.000%
18	1.21	4.35	0.00	-1.21	4.35	0.00	0.000%
19	1.07	4.35	0.62	-1.07	4.35	-0.62	0.000%
20	0.60	4.35	1.05	-0.60	4.35	-1.05	0.000%
21	0.00	4.35	1.20	-0.00	4.35	-1.20	0.000%
22	-0.60	4.35	1.05	0.60	4.35	-1.05	0.000%
23	-1.07	4.35	0.62	1.07	4.35	-0.62	0.000%
24	-1.21	4.35	0.00	1.21	4.35	-0.00	0.000%
25	-1.04	4.35	-0.60	1.04	4.35	0.60	0.000%
26	-0.60	4.35	-1.05	0.60	4.35	1.05	0.000%
27	0.00	-2.59	-1.24	0.00	2.59	1.24	0.000%
28	0.60	-2.59	-1.04	-0.60	2.59	1.04	0.000%
29	1.03	-2.59	-0.59	-1.03	2.59	0.59	0.000%
30	1.20	-2.59	0.00	-1.20	2.59	0.00	0.000%
31	1.08	-2.59	0.62	-1.08	2.59	-0.62	0.000%
32	0.60	-2.59	1.04	-0.60	2.59	-1.04	0.000%
33	0.00	-2.59	1.19	-0.00	2.59	-1.19	0.000%
34	-0.60	-2.59	1.04	0.60	2.59	-1.04	0.000%
35	-1.08	-2.59	0.62	1.08	2.59	-0.62	0.000%
36	-1.20	-2.59	0.00	1.20	2.59	-0.00	0.000%
37	-1.03	-2.59	-0.59	1.03	2.59	0.59	0.000%
38	-0.60	-2.59	-1.04	0.60	2.59	1.04	0.000%

### Non-Linear Convergence Results

Load Combination	Converged?	Number of Cycles	Displacement Tolerance	Force Tolerance
1	Yes	4	0.00000001	0.00000001
2	Yes	5	0.00000001	0.00054492
3	Yes	5	0.00000001	0.00090122
4	Yes	5	0.00004241	0.00065746
5	Yes	5	0.00000001	0.00017434
6	Yes	4	0.00000001	0.00085831
7	Yes	5	0.00009394	0.00033922
8	Yes	6	0.00004683	0.00059762
9	Yes	6	0.00000001	0.00019796
10	Yes	5	0.00000001	0.00052594
11	Yes	5	0.00000001	0.00011917
12	Yes	4	0.00000001	0.00026884
13	Yes	5	0.00000001	0.00010272
14	Yes	4	0.00000001	0.00018218
15	Yes	5	0.00000001	0.00077150
16	Yes	6	0.00003549	0.00043017
17	Yes	6	0.00007623	0.00059570
18	Yes	5	0.00010109	0.00026662
19	Yes	5	0.00005631	0.00006764
20	Yes	5	0.00046015	0.00041515
21	Yes	7	0.00024954	0.00079203
22	Yes	6	0.00003995	0.00069316
23	Yes	5	0.00000001	0.00081982
24	Yes	5	0.00000001	0.00029773

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25	Yes	4	0.00000001	0.00068969
26	Yes	5	0.00000001	0.00025649
27	Yes	6	0.00000001	0.00010953
28	Yes	6	0.00004375	0.00067750
29	Yes	6	0.00005624	0.00081074
30	Yes	5	0.00007123	0.00030681
31	Yes	5	0.00000001	0.00003764
32	Yes	5	0.00024647	0.00044322
33	Yes	7	0.00009778	0.00099582
34	Yes	6	0.00000001	0.00034294
35	Yes	6	0.00000001	0.00030001
36	Yes	5	0.00000001	0.00023250
37	Yes	4	0.00000001	0.00054269
38	Yes	5	0.00000001	0.00019543

### Maximum Tower Deflections - Service Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
Pole Antenna	142.67 - 140	36.677	31	2.8772	4.8595
T1	140 - 120	35.070	31	2.8746	4.9061
T2	120 - 100	23.637	31	2.4226	3.2138
T3	100 - 80	14.783	31	1.7489	1.4354
T4	80 - 60	8.577	31	1.1823	0.6090
T5	60 - 40	4.372	31	0.8089	0.3077
T6	40 - 20	1.611	31	0.4934	0.0698
T7	20 - 0	0.326	31	0.1718	0.0165

### Critical Deflections and Radius of Curvature - Service Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
143.00	11' x 3" Dia Omni	31	36.677	2.8772	4.8892	8444
134.67	Rohn 6' Side-Arm(1)	31	31.881	2.8202	4.7122	4814
127.00	11' x 3" Dia Omni	31	27.430	2.6428	4.0162	2256

### Maximum Tower Deflections - Design Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
Pole Antenna	142.67 - 140	41.814	19	3.2750	4.2328
T1	140 - 120	39.986	19	3.2726	4.2301
T2	120 - 100	26.987	19	2.7566	2.7917
T3	100 - 80	16.892	19	2.0013	1.2543
T4	80 - 60	9.783	19	1.3557	0.5352
T5	60 - 40	4.966	19	0.9256	0.2714

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Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
T6	40 - 20	1.814	19	0.5617	0.0618
T7	20 - 0	0.361	19	0.1928	0.0147

### Critical Deflections and Radius of Curvature - Design Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
143.00	11' x 3" Dia Omni	19	41.814	3.2750	4.2328	7086
134.67	Rohn 6' Side-Arm(1)	19	36.359	3.2106	4.0706	4152
127.00	11' x 3" Dia Omni	19	31.301	3.0072	3.4792	1992

### Bolt Design Data

Section No.	Elevation ft	Component Type	Bolt Grade	Bolt Size in	Number Of Bolts	Maximum Load per Bolt K	Allowable Load K	Ratio Load Allowable	Allowable Ratio	Criteria
T1	140	Leg	A325N	0.3750	4	0.93	4.86	0.192 ✓	1.333	Bolt Tension
T2	120	Leg	A325N	0.3750	4	1.98	4.86	0.407 ✓	1.333	Bolt Tension
T3	100	Leg	A325N	0.5000	4	3.08	8.64	0.357 ✓	1.333	Bolt Tension
T4	80	Leg	A325N	0.6250	4	4.20	13.50	0.311 ✓	1.333	Bolt Tension
		Diagonal	A325N	0.3750	1	0.74	2.32	0.318 ✓	1.333	Bolt Shear
T5	60	Leg	A325N	0.6250	4	5.34	13.50	0.396 ✓	1.333	Bolt Tension
		Diagonal	A325N	0.3750	1	0.70	2.32	0.303 ✓	1.333	Bolt Shear
T6	40	Leg	A325N	0.6250	4	4.07	13.50	0.302 ✓	1.333	Bolt Tension
		Diagonal	A325N	0.5000	1	1.03	3.17	0.324 ✓	1.333	Member Bearing
T7	20	Leg	A325N	0.6250	4	3.53	13.50	0.261 ✓	1.333	Bolt Tension
		Diagonal	A325N	0.5000	1	0.38	3.17	0.120 ✓	1.333	Member Bearing

### Compression Checks

### Leg Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	F <sub>a</sub> ksi	A in <sup>2</sup>	Actual P K	Allow. P <sub>a</sub> K	Ratio P P <sub>a</sub>
T1	140 - 120	9/16	20.00	0.99	169.2 K=2.00	5.213	0.2485	-4.68	1.30	3.614 X

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Section No.	Elevation	Size	L	L <sub>u</sub>	Kl/r	F <sub>a</sub>	A	Actual P	Allow. P <sub>a</sub>	Ratio P/P <sub>a</sub>
	ft		ft	ft		ksi	in <sup>2</sup>	K	K	
T2	120 - 100	KL/R > 150 (C) - 3 3/4	20.00	0.99	126.9 K=2.00	9.267	0.4418	-8.93	4.09	2.182 X
T3	100 - 80	H1-3 (2.18 CR) - 72 15/16	20.00	0.99	101.6 K=2.00	14.345	0.6903	-13.55	9.90	1.368 X
T4	80 - 60	H1-3 (1.37 CR) - 141 1 1/4	20.00	0.99	76.2 K=2.00	19.768	1.2272	-18.41	24.26	0.759 ✓
T5	60 - 40	1 7/16	20.00	0.99	66.2 K=2.00	21.626	1.6229	-23.42	35.10	0.667 ✓
T6	40 - 20	ROHN 2 STD	20.03	4.01	61.1 K=1.00	22.531	1.0745	-21.88	24.21	0.904 ✓
T7	20 - 0	ROHN 2 STD	20.03	4.01	61.1 K=1.00	22.531	1.0745	-18.36	24.21	0.758 ✓

### Diagonal Design Data (Compression)

Section No.	Elevation	Size	L	L <sub>u</sub>	Kl/r	F <sub>a</sub>	A	Actual P	Allow. P <sub>a</sub>	Ratio P/P <sub>a</sub>
	ft		ft	ft		ksi	in <sup>2</sup>	K	K	
T1	140 - 120	3/8	1.53	1.47	131.7 K=0.70	8.612	0.1104	-0.97	0.95	1.016 ✓
T2	120 - 100	3/8	1.79	1.72	153.7 K=0.70	6.324	0.1104	-0.77	0.70	1.102 ✓
T3	100 - 80	7/16	2.07	1.98	152.4 K=0.70	6.432	0.1503	-0.69	0.97	0.717 ✓
T4	80 - 60	5/8	2.37	2.26	121.5 K=0.70	10.072	0.3068	-0.69	3.09	0.222 ✓
T5	60 - 40	5/8	2.67	2.54	136.3 K=0.70	8.032	0.3068	-0.67	2.46	0.270 ✓
T6	40 - 20	L1 1/2x1 1/2x1/8	4.83	2.35	101.3 K=1.07	12.817	0.3594	-1.15	4.61	0.250 ✓
T7	20 - 0	L1 1/2x1 1/2x1/8	7.17	3.48	140.9 K=1.00	7.526	0.3594	-0.37	2.70	0.137 ✓

### Top Girt Design Data (Compression)

Section No.	Elevation	Size	L	L <sub>u</sub>	Kl/r	F <sub>a</sub>	A	Actual P	Allow. P <sub>a</sub>	Ratio P/P <sub>a</sub>
	ft		ft	ft		ksi	in <sup>2</sup>	K	K	
T1	140 - 120	3/8	1.17	1.12	100.3 K=0.70	12.935	0.1104	-0.06	1.43	0.042 ✓
T2	120 - 100	3/8	1.17	1.11	99.1 K=0.70	13.096	0.1104	-0.51	1.45	0.354 ✓
T3	100 - 80	7/16	1.50	1.42	109.3 K=0.70	11.765	0.1503	-0.37	1.77	0.211 ✓
T4	80 - 60	5/8	1.83	1.73	92.9	13.862	0.3068	-0.25	4.25	0.059 ✓

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Section No.	Elevation	Size	L	L <sub>u</sub>	Kl/r	F <sub>a</sub>	A	Actual P	Allow. P <sub>a</sub>	Ratio P / P <sub>a</sub>
	ft		ft	ft		ksi	in <sup>2</sup>	K	K	
T5	60 - 40	5/8	2.17	2.05	K=0.70 K=0.70	110.1 K=0.70	11.656	0.3068	-0.18	3.58 0.049

### Bottom Girt Design Data (Compression)

Section No.	Elevation	Size	L	L <sub>u</sub>	Kl/r	F <sub>a</sub>	A	Actual P	Allow. P <sub>a</sub>	Ratio P / P <sub>a</sub>
	ft		ft	ft		ksi	in <sup>2</sup>	K	K	
T1	140 - 120	3/8	1.17	1.12	100.3 K=0.70	12.935	0.1104	-0.41	1.43	0.289
T2	120 - 100	3/8	1.50	1.44	128.7 K=0.70	9.019	0.1104	-0.28	1.00	0.280
T3	100 - 80	7/16	1.83	1.75	134.4 K=0.70	8.262	0.1503	-0.20	1.24	0.162
T4	80 - 60	5/8	2.17	2.06	110.8 K=0.70	11.563	0.3068	-0.17	3.55	0.047
T5	60 - 40	5/8	2.50	2.38	127.9 K=0.70	9.131	0.3068	-0.33	2.80	0.119

### Tension Checks

### Leg Design Data (Tension)

Section No.	Elevation	Size	L	L <sub>u</sub>	Kl/r	F <sub>a</sub>	A	Actual P	Allow. P <sub>a</sub>	Ratio P / P <sub>a</sub>
	ft		ft	ft		ksi	in <sup>2</sup>	K	K	
T1	140 - 120	9/16	20.00	0.99	84.6	30.000	0.2485	4.07	7.46	0.545
T2	120 - 100	3/4	20.00	0.99	63.5	30.000	0.4418	8.09	13.25	0.610
T3	100 - 80	H1-3 (1.83 CR) - 73 15/16	20.00	0.99	50.8	30.000	0.6903	12.42	20.71	0.600
T4	80 - 60	1 1/4	20.00	0.99	38.1	30.000	1.2272	16.85	36.82	0.458
T5	60 - 40	1 7/16	20.00	0.99	33.1	30.000	1.6229	21.37	48.69	0.439
T6	40 - 20	ROHN 2 STD	20.03	4.01	61.1	30.000	1.0745	20.08	32.24	0.623
T7	20 - 0	ROHN 2 STD	20.03	4.01	61.1	30.000	1.0745	15.62	32.24	0.484

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### Diagonal Design Data (Tension)

Section No.	Elevation	Size	L	L <sub>u</sub>	Kl/r	F <sub>a</sub>	A	Actual P K	Allow. P <sub>a</sub> K	Ratio P P <sub>a</sub>
	ft		ft	ft		ksi	in <sup>2</sup>			
T1	140 - 120	3/8	1.53	1.47	188.1	21.600	0.1104	0.98	2.39	0.409
T2	120 - 100	3/8	1.54	1.46	187.3	21.600	0.1104	1.03	2.39	0.431
T3	100 - 80	7/16	1.81	1.72	188.4	21.600	0.1503	0.81	3.25	0.248
T4	80 - 60	5/8	2.09	1.98	151.7	21.600	0.3068	0.73	6.63	0.110
T5	60 - 40	5/8	2.39	2.26	173.8	21.600	0.3068	0.68	6.63	0.103
T6	40 - 20	L1 1/2x1 1/2x1/8	4.83	2.35	63.5	29.000	0.2109	1.03	6.12	0.168
T7	20 - 0	L1 1/2x1 1/2x1/8	6.19	3.00	80.3	29.000	0.2109	0.38	6.12	0.062

### Top Girt Design Data (Tension)

Section No.	Elevation	Size	L	L <sub>u</sub>	Kl/r	F <sub>a</sub>	A	Actual P K	Allow. P <sub>a</sub> K	Ratio P P <sub>a</sub>
	ft		ft	ft		ksi	in <sup>2</sup>			
T1	140 - 120	3/8	1.17	1.12	143.3	21.600	0.1104	0.44	2.39	0.184*
T2	120 - 100	3/8	1.17	1.11	141.5	21.600	0.1104	0.43	2.39	0.181
T3	100 - 80	7/16	1.50	1.42	156.2	21.600	0.1503	0.29	3.25	0.091
T4	80 - 60	5/8	1.83	1.73	132.7	21.600	0.3068	0.21	6.63	0.032
T5	60 - 40	5/8	2.17	2.05	157.3	21.600	0.3068	0.15	6.63	0.023

\* DL controls

### Bottom Girt Design Data (Tension)

Section No.	Elevation	Size	L	L <sub>u</sub>	Kl/r	F <sub>a</sub>	A	Actual P K	Allow. P <sub>a</sub> K	Ratio P P <sub>a</sub>
	ft		ft	ft		ksi	in <sup>2</sup>			
T1	140 - 120	3/8	1.17	1.12	143.3	21.600	0.1104	0.47	2.39	0.196
T2	120 - 100	3/8	1.50	1.44	183.8	21.600	0.1104	0.35	2.39	0.147
T3	100 - 80	7/16	1.83	1.75	192.1	21.600	0.1503	0.23	3.25	0.072

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Section No.	Elevation	Size	L	L <sub>u</sub>	Kl/r	F <sub>a</sub>	A	Actual P	Allow. P <sub>a</sub>	Ratio P/P <sub>a</sub>
	ft		ft	ft		ksi	in <sup>2</sup>	K	K	
T4	80 - 60	5/8	2.17	2.06	158.3	21.600	0.3068	0.19	6.63	0.028
T5	60 - 40	5/8	2.50	2.38	182.7	21.600	0.3068	0.36	6.63	0.054 ✓

### Section Capacity Table

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	SF*P <sub>allow</sub> K	% Capacity	Pass Fail	
T1	140 - 120	Leg	9/16	3	-4.68	1.73	271.1	Fail X	
T2	120 - 100	Leg	3/4	72	-8.93	5.46	163.7	Fail X	
T3	100 - 80	Leg	15/16	141	-13.55	13.20	102.6	Fail X	
T4	80 - 60	Leg	1 1/4	210	-18.41	32.34	56.9	Pass	
T5	60 - 40	Leg	1 7/16	279	-23.42	46.79	50.1	Pass	
T6	40 - 20	Leg	ROHN 2 STD	348	-21.88	32.27	67.8	Pass	
T7	20 - 0	Leg	ROHN 2 STD	381	-18.36	32.27	56.9	Pass	
T1	140 - 120	Diagonal	3/8	12	-0.97	1.27	76.3	Pass	
T2	120 - 100	Diagonal	3/8	80	-0.77	0.93	82.7	Pass	
T3	100 - 80	Diagonal	7/16	149	-0.69	1.29	53.8	Pass	
T4	80 - 60	Diagonal	5/8	218	-0.69	4.12	16.7	Pass	
T5	60 - 40	Diagonal	5/8	291	-0.67	3.28	20.3	Pass	
T6	40 - 20	Diagonal	L1 1/2x1 1/2x1/8	378	-1.15	6.14	18.7	Pass	
T7	20 - 0	Diagonal	L1 1/2x1 1/2x1/8	394	-0.37	3.61	10.3	Pass	
T1	140 - 120	Top Girt	3/8	5	0.44	2.39	18.4	Pass	
T2	120 - 100	Top Girt	3/8	74	-0.51	1.93	26.5	Pass	
T3	100 - 80	Top Girt	7/16	143	-0.37	2.36	15.8	Pass	
T4	80 - 60	Top Girt	5/8	212	-0.25	5.67	4.4	Pass	
T5	60 - 40	Top Girt	5/8	281	-0.18	4.77	3.7	Pass	
T1	140 - 120	Bottom Girt	3/8	9	-0.41	1.90	21.7	Pass	
T2	120 - 100	Bottom Girt	3/8	77	-0.28	1.33	21.0	Pass	
T3	100 - 80	Bottom Girt	7/16	146	-0.20	1.66	12.1	Pass	
T4	80 - 60	Bottom Girt	5/8	215	-0.17	4.73	3.5	Pass	
T5	60 - 40	Bottom Girt	5/8	284	-0.33	3.73	8.9	Pass	
							Summary		
							Leg (T1)	271.1	Fail X
							Diagonal (T2)	82.7	Pass
							Top Girt (T2)	26.5	Pass
							Bottom Girt (T1)	21.7	Pass
							Bolt Checks	30.5	Pass
							RATING =	271.1	Fail X



JWB Tower Services, LLC  
148 Governor Street  
New Britain, CT 06053  
(800) 819-3084  
(860) 256-8175 fax

## Self-Support Lattice Tower Mapping and Inventory General Information

<b>Site Name:</b>	S Woodstock	
<b>Site Number:</b>	6290	
<b>FCC Number:</b>	1044251	
<b>Manufacturer ID #</b>	Rohn SSV	
<b>Street Address:</b>	87 West Quassett Road	
<b>City/State/Zip Code:</b>	Woodstock, CT	
<b>County:</b>		
<b>Lat:</b>	N/S	41° 55' 43.6"
<b>Long:</b>	E/W	71° 59' 13.3"
<b>Performed By:</b>	JWB	
<b>Date:</b>	8/19/2011	

## Manufacture: (Circle One)

Rohn       Summit       EEI       Pirod       Sabre       Fort Worth       Valmont       Nudd       Other

### Foundation:

Reveal: 0 Uphill and 12" Downhill  
Grout: 1" (No Grout)  
Size/Circumference: 10'x10'

### Anchor Bolts:

Base Plate Grouted: Yes  No   
Number of Anchor Bolts: 4/Leg      Diameter of Anchor Bolts: 5/8"  
Anchor Bolt Spacing: Equal

### Safety Climb:

Start Elevation (AGL) N/A      End Elevation (AGL) N/A  
Location N/A

### Climbing Components: Climbing Access is via Diagonals

Step Bolts	Climbing Ladder	Internal	External
<u>N/A</u> Leg Start Elevation: (AGL)	<u>N/A</u> End Elevation: (AGL)	<u>N/A</u>	
<u> </u> Leg Start Elevation: (AGL)	<u> </u> End Elevation: (AGL)	<u> </u>	
<u> </u> Leg Start Elevation: (AGL)	<u> </u> End Elevation: (AGL)	<u> </u>	
<u> </u> Leg Start Elevation: (AGL)	<u> </u> End Elevation: (AGL)	<u> </u>	

### Lighting System Information:

1st OB: <u>N/A</u>	1st Beacon: <u>N/A</u>
2nd OB: <u> </u>	2nd Beacon: <u> </u>
3rd OB: <u> </u>	3rd Beacon: <u> </u>
4th OB: <u> </u>	4th Beacon: <u> </u>

Top of Tower Steel (Top of Concrete) 142'-9"

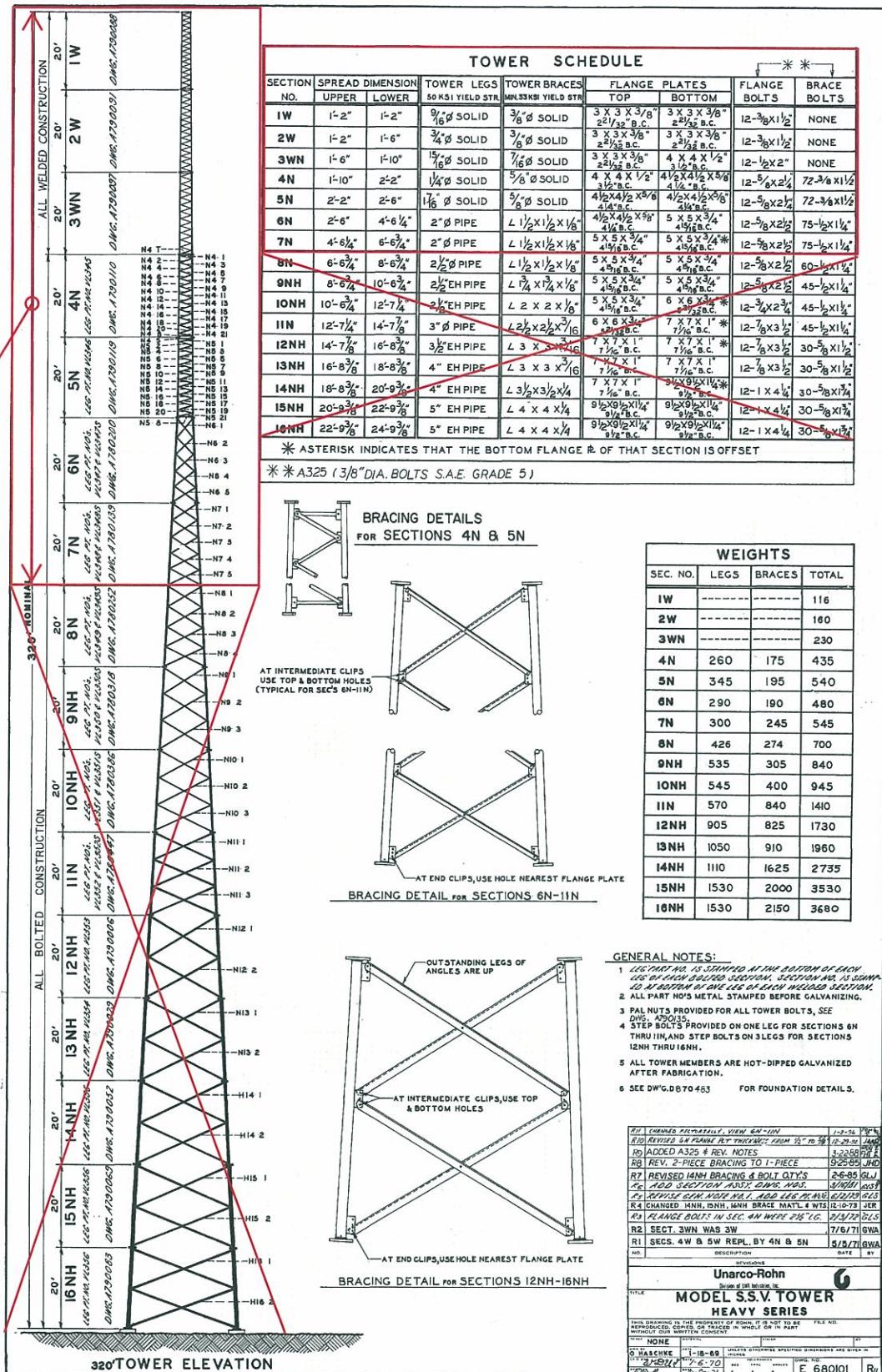
## Antenna Information:

CARRIER		Verizon		PIC #	5
<b>MOUNT</b>					
Type:	<b>Standoff</b>	Manf.:	<b>Custom</b>		
Elev. C/L:		Bottom:	<b>132'</b>	Top:	<b>137'-4"</b>
Face Width:	<b>3"</b>	Height:	<b>5'-4"</b>	Projection:	<b>6'</b>
<b>Leg:</b> _____					
<b>Azimuth/s:</b> _____					
<b>ANTENNA 1</b>					
Type:	<b>Omni</b>	Manf.:	<b>Celwave?</b>	Model:	<b>Unknown</b>
Elev. C/L:		Bottom:	<b>137'-4"</b>	Top:	<b>148'-4"</b>
Quantity:	<b>1</b>	Dim: (HxWxD)	<b>11'x3" + 11'x0.5"</b>		
<b>Leg:</b> <b>E</b>					
<b>Azimuth/s:</b> _____					
<b>ANTENNA 2</b>					
Type:	<b>Omni</b>	Manf.:	<b>Celwave?</b>	Model:	<b>Unknown</b>
Elev. C/L:		Bottom:	<b>132'</b>	Top:	<b>121'</b>
Quantity:	<b>1</b>	Dim: (HxWxD)	<b>11'x3" + 11'x0.5"</b>		
<b>Leg:</b> <b>E</b>					
<b>Azimuth/s:</b> _____					
<b>TMA'S</b>					
Quantity:	<b>N/A</b>	Manf.:			
<b>COAX</b> <b>Taped to E Leg - 12' - 136'</b>					
Quantity:	<b>2</b>	Size:	<b>7/8"</b>	Jumper:	<b>1/2"</b>
Color: <b>N/A</b>					

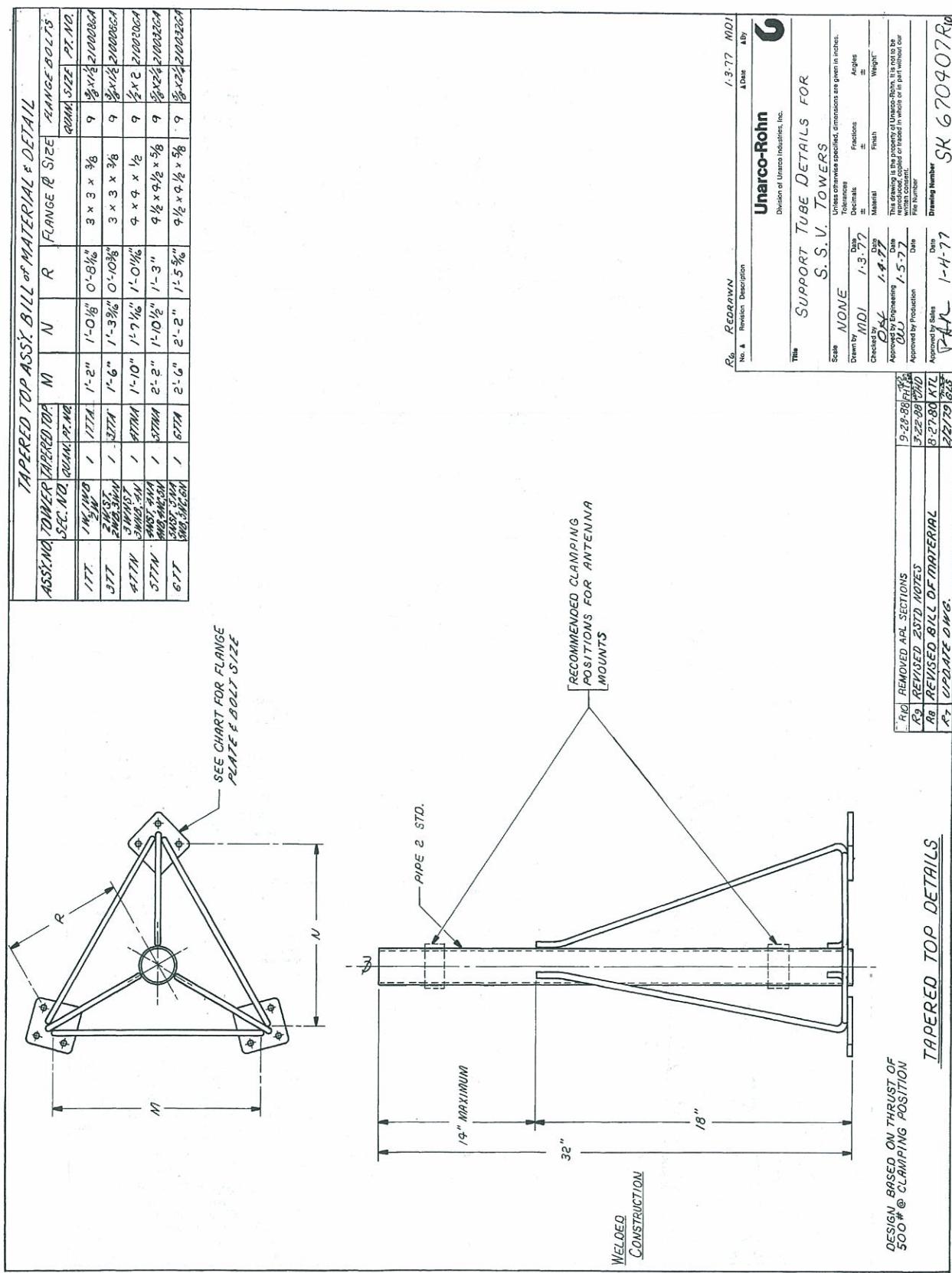
# Self-Supporting Towers



140' + 32"  
Tapered  
Top Section



# Self-Supporting Towers







1.0 Elevation



2.0 Base

### 3.1 Bent Members

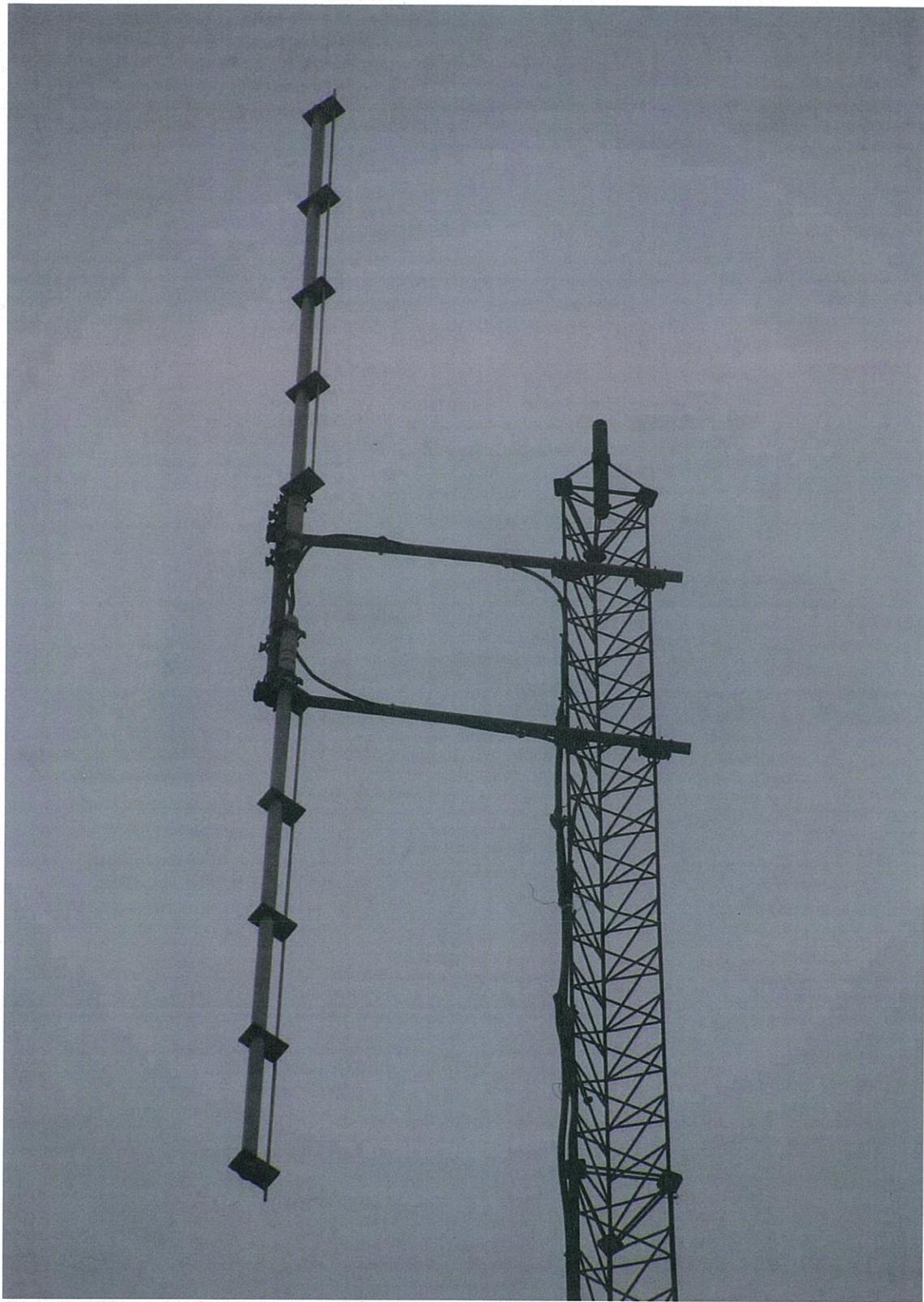


### 3.2 Bent Members

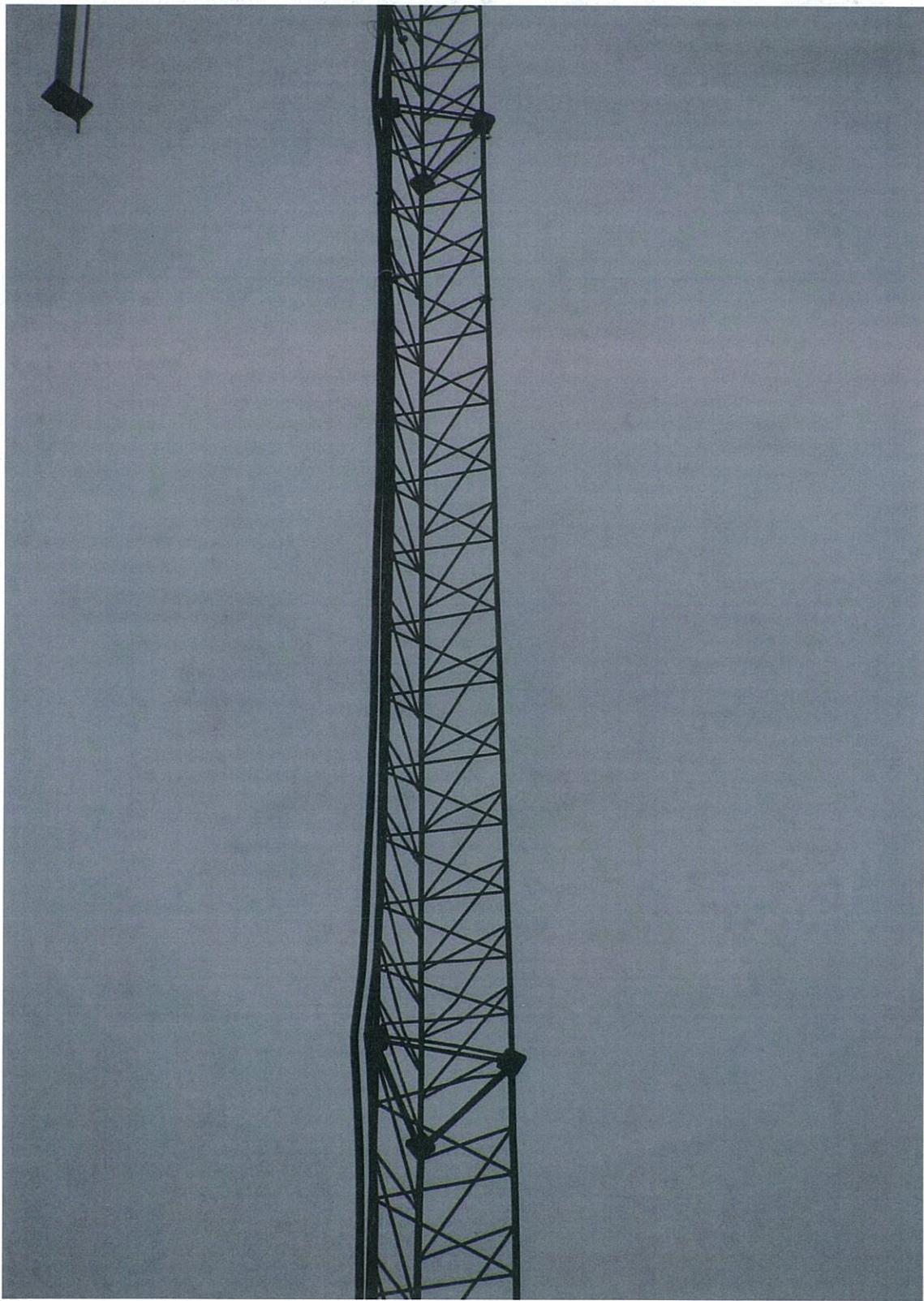




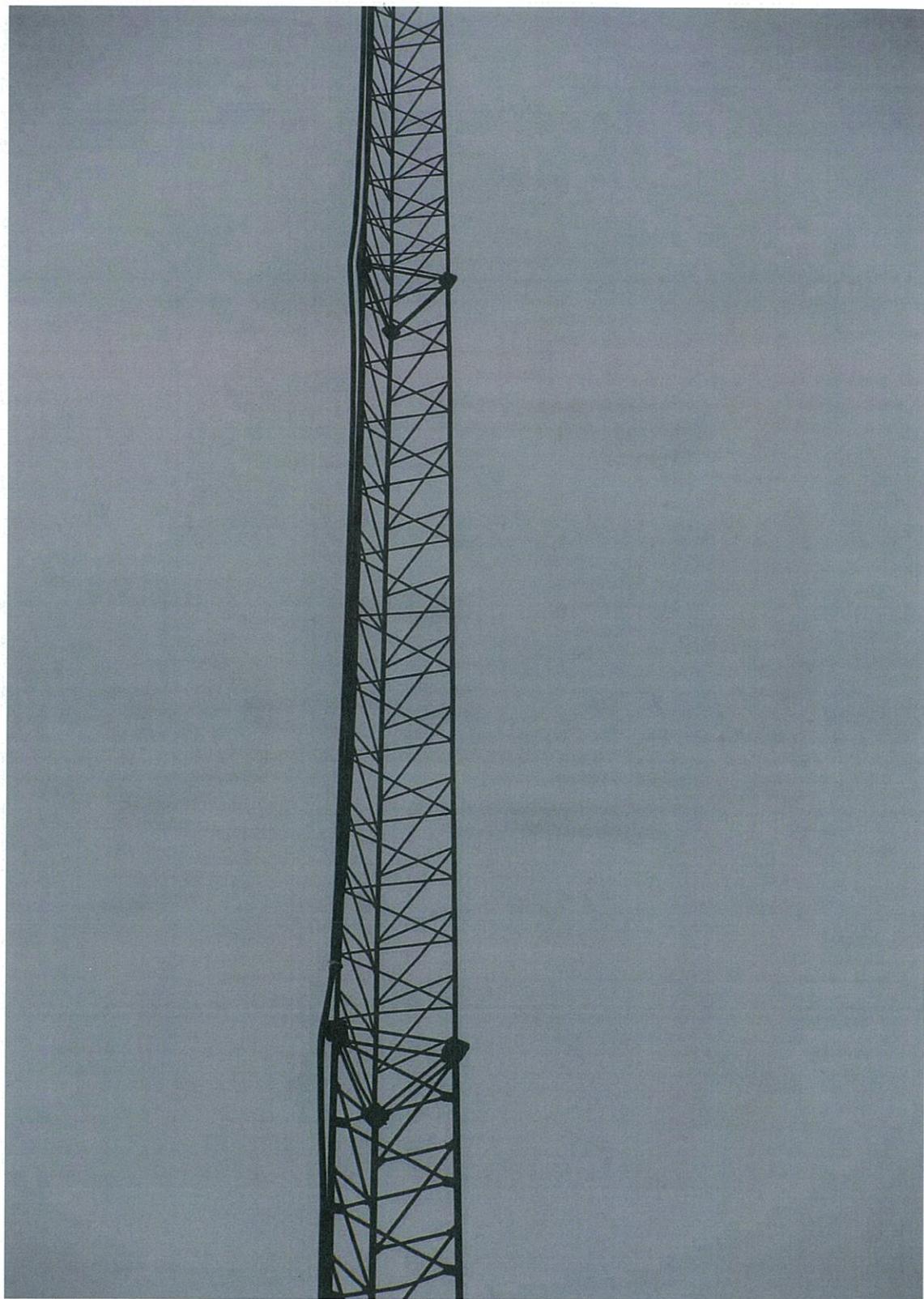
4.0 Verizon Coax



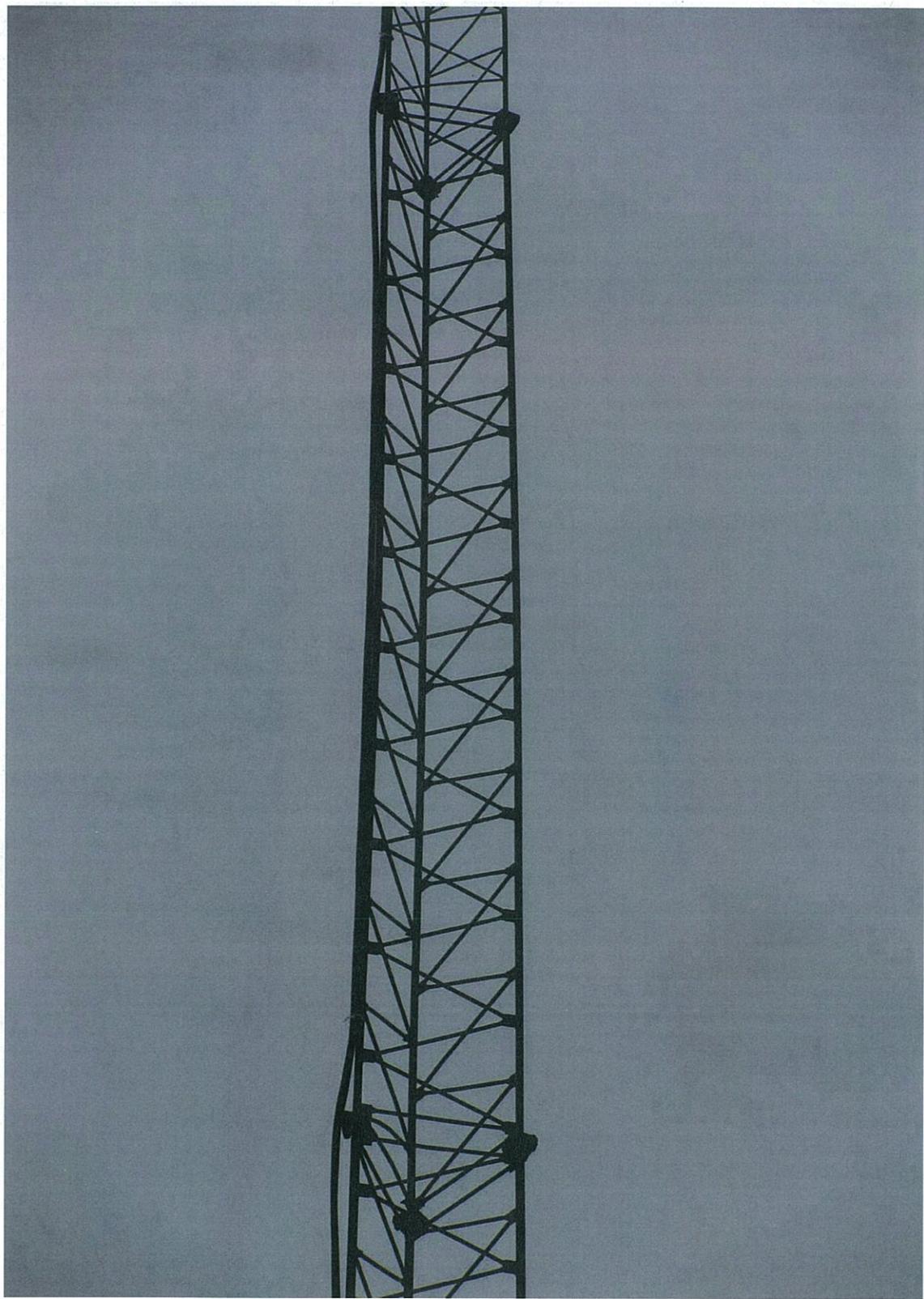
5.0



6.0



7.0

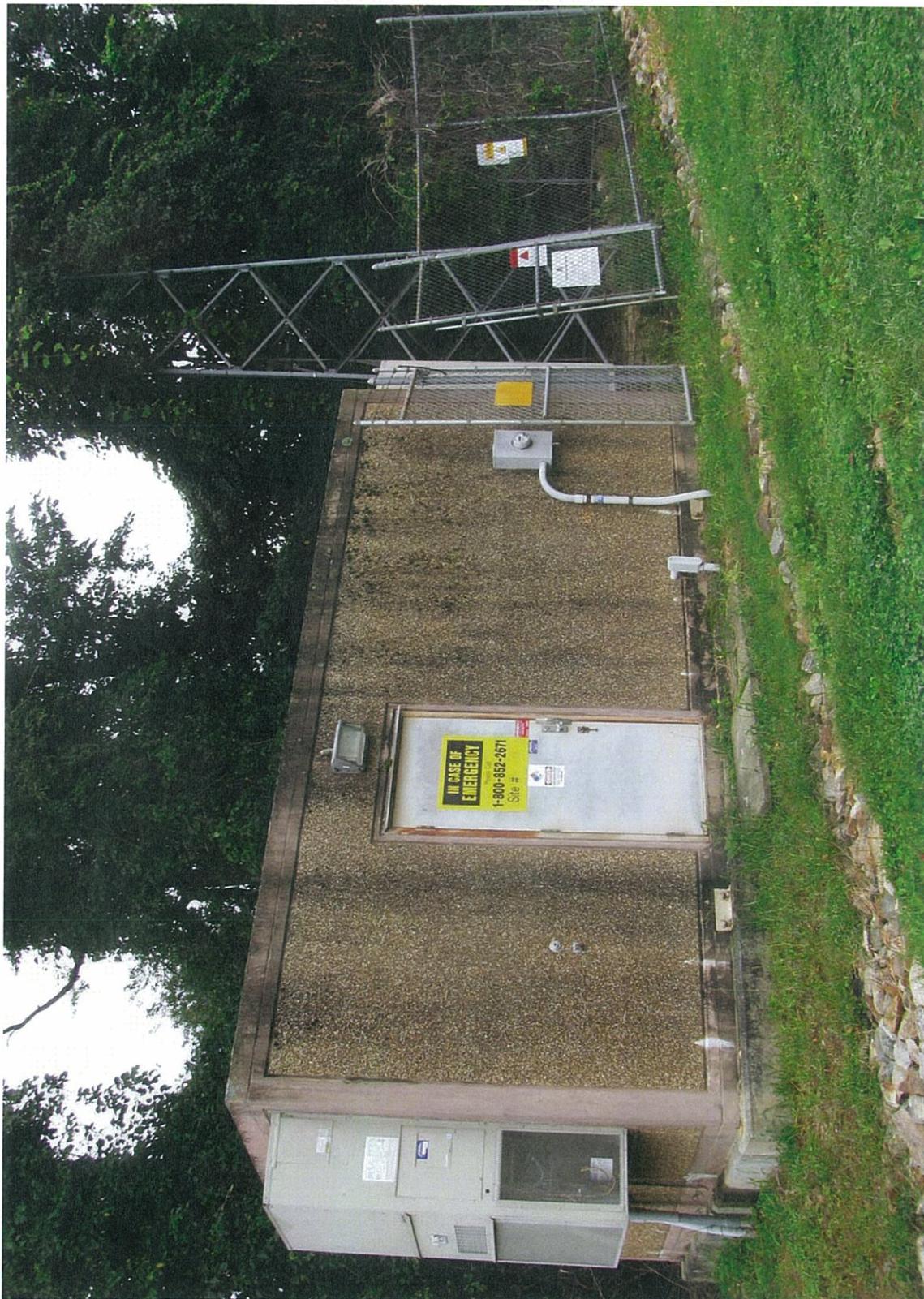


8.0





10.0



11.0 Compound

